STORMWATER MANAGEMENT REPORT

Harmony Village

218-220 Main Street Medway, Massachusetts

Prepared for:

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November 12, 2020





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* Checklist for Stormwater Report

REPORT SUMMARY:

Calculation Objectives:

The objective of these calculations is to demonstrate design compliance of the proposed development at 218-220 Main Street in Medway, Massachusetts for water quantity and water quality objectives of the DEP's Stormwater Management Regulations, the Massachusetts Stormwater Handbook, and Medway's Stormwater Management and Land Disturbance Bylaw. Portions of the Project can be considered as redevelopment. The proposed development will fully comply with the ten (10) standards of the MADEP Stormwater Regulations as well as Medway's Stormwater Management and Land Disturbance Bylaw.

Subcatchment Area Plans have been incorporated into this report to depict existing and proposed watershed areas.

Calculation Methods:

- TR55/TR20 methodology utilizing HydroCAD software by Applied Microcomputer Systems.
- MADEP Stormwater Management Handbook for Water Quality Calculations / TSS Removal.

Sources of Data:

- Technical Report No. 20 & No. 55
- Technical Paper No. 40
- NOAA Atlas 14, September 2015
- Existing Conditions Field Survey by Meridian Associates, Inc. in July 2019
- Web Soil Survey of Norfolk County Massachusetts by the USDA Natural Resources Conservation Service (NRCS)
- Soil Testing performed by Janice Weldon, SE of Meridian Associates, Inc. on April 27, 2020
- "Stormwater Management Stormwater Policy Handbook and Stormwater Technical Handbook" by the Massachusetts DEP – February 2008

Soll Descriptions:

Existing soil conditions have been characterized by the Norfolk County Soil Survey Report. The soils have been assigned a Hydrologic Soil Grouping (HSG) by NRCS. According to NRCS, the site consists of the following soils:

Hydrologic Soil Group (HSG) Rating	NRCS Soil Map Unit Name
В	Charlton-Hollis-Rock outcrop complex, 8-15% slopes
В	Canton fine sandy loam, 0-8% slopes, extremely stony

As required by Volume 3: Documenting Compliance with the Massachusetts Stormwater Management Standards, an on-site soil evaluation was undertaken on April 27, 2020 to confirm the NRCS soil survey by Janice Weldon, a licensed soil evaluator with MAI.

The observed soil type was documented, mapped and is included in this report. The observed soils were found to be primarily sand and loamy sand, with an Estimated Seasonal High Groundwater elevation varying from 226.0 to 233.5. This variation is likely due to the presence of ledge.

Due to the soil type, design of the infiltration chambers, as well as dewatering and mounding calculations are based on a loamy sand Rawls Infiltration rate of 2.41 in/hr, as the chambers will be draining into this layer. The detention basin was modelled with a more conservative Rawls Infiltration rate of 1.02 in/hr since the basin will dewater into the sandy loam. Mounding and dewatering calculations were also performed with this lower Rawls Rate.

Selection of Storm Events:

The storm events have been compiled from the National Oceanic and Atmospheric Administration (NOAA)'s Atlas 14. The 2-year, 10-year, and 100-year storm events have been utilized for hydrology calculations. The rainfall data for the Type III, 24-hour storm events follow:

Frequency (Years)	Rainfall (Inches/Hour)
2	3.37
10	5.26
100	8.26

Existing Conditions Overview:

The Site is a 1.22 acre parcel located on Main Street in southern Medway. There are currently two single family homes on the site as well as a shed and a pool. Stormwater on the site drains naturally to the abutting property to the west or overland to the municipal storm drain system on Main Street. Some of the runoff which drains to Main Street is captured in a manmade pond and/or a natural depression, however there are no true stormwater management devices on the property.

Existing conditions on the site have been modelled using four subcatchment areas. A summary of existing subcatchments and natural drainage devices can be found below.

<u>Description</u>	Comments
SC-E1 (DP-1)	Developed area of site, flows directly overland to Main Street
SC-E2 (DP-1)	Existing pervious area, flows to man-made pond
SC-E3 (DP-1)	Overland flow to existing depression
SC-E4 (DP-2)	Overland flow to western abutters
EP-1	Man-made lined pond, no exfiltration
EP-2	Existing depression in southwest corner of site
DP-1	Main Street municipal storm drain system
DP-2	224 Main Street (Western abutters)

Proposed Conditions Overview:

New Generation Custom Homes is proposing to construct four additional residential units in the form of one quadplex. The driveway will be extended to service the new building. The existing pool and shed will be demolished. Development will add approximately 11,100 sf of new impervious to the site in the form of driveways and the building.

Increases in stormwater runoff rates and volumes will be mitigated through the installation of two subsurface infiltration systems which will serve as drywells for all three buildings on site. The drywells have been sized to contain the 100-year storm event, and roof drains on all buildings will be fitted with overflows to allow for bypass in larger storm events. Stormwater from driveways and yards will be directed to a detention basin via deep sump catch basins and a CDS treatment unit.

The following is a summary of post-development subcatchment watershed areas from the site:

<u>Description</u>	Comments
SC P-1 (DP-2)	Overland flow to 244 Main Street
SC P-2 (DP-1)	Proposed development driveways and central yard area to PP-1
SC P-3 (DP-1)	Overland flow directly to PP-1
SC P-4 (DP-1)	Overland flow to Main Street
P-Ex	Existing buildings
P-D	Proposed four-unit development
PP-1	Proposed Detention Basin
DW-1	Proposed drywell to serve existing buildings
DW-2	Proposed drywell to serve proposed building
DP-1	Main Street municipal storm drain system
DP-2	224 Main Street (Western Abutters)

Summary of Flows at Design Point 1

	Existing Co	nditions (Pre)	Proposed Co	onditions (Post)
Storm Event	Peak Flow (CFS)	Runoff Volume (CF)	Peak Flow (CFS)	Runoff Volume (CF)
2-Year (3.37 in./hr.)	0.47	2,52 9	0.11	509
10-Year (5.26 in./hr.)	1.28	6,196	0.35	1,328
100-Year (8.26 in./hr.)	2.78	13,201	0.88	5,709

Summary of Flows at Design Point 2

	Existing Co	nditions (Pre)	Proposed C	onditions (Post)
Storm Event	Peak Flow (CFS)	Runoff Volume (CF)	Peak Flow (CFS)	Runoff Volume (CF)
2-Year (3.37 in./hr.)	0.24	1,890	0.24	1,381
10-Year (5.26 in./hr.)	0.97	5,722	0.97	4,093
100-Year (8.26 in./hr.)	2.53	13,996	2.50	9,762

Erosion Control Discussion:

The project is subject to the NPDES Construction General Permit requirements, so a comprehensive Stormwater Pollution Prevention Plan (SWPPP) will be required prior to construction. Erosion control measures have been depicted on the plans and are further outlined in the Operation and Maintenance Plan found In this Report. Inlet protection shall be provided on all catch basins and storm drain inlets within the limit of work. In addition, the Project area will be surrounded by a compost sock or sediment control barrier for the duration of construction. An Operation and Maintenance Exhibit is also included as part of this submission.

Conclusion:

The calculations performed for all design storm events indicate that neither peak flow rates nor volumes will exceed those of existing conditions with implementation of the stormwater management system as proposed for the 2, 10 and 100-year storm events.

An Operation and Maintenance Plan for stormwater systems is included herein.

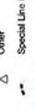
With Implementation of the stormwater management system as designed, full compliance with the MADEP Stormwater Management regulations as well as the Town of Medway Stormwater Management and Land Disturbance Bylaw.

SOILS INFORMATION	

MAP LEGEND

	Area of Interest (AOI)	œ	Spoil Area
	Area of Interest (AOI)	0	Story Spot
solls	Soil Man Linit Polymone	8	Very Stony Spot
1	Soil Map Unit Lines	D	Wet Spot
1	Soil Man Unit Points	٥	Other
Special	Special Point Features		Special Line Feat

Other	Special Line F
٥	



eatures







Closed Depression

Borrow Pit

Blowout

Clay Spot

Interstate Highways



Major Roads

Gravelly Spot

Gravel Pit



Aerial Photography Background

Marsh or swamp

Lava Flow

_andfill

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot Sandy Spot

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25,000.

Warning: Soil Map may not be valid at this scale.

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause line placement. The maps do not show the small areas of

Please rely on the bar scale on each map sheet for map measurements.

Coordinate System: Web Mercator (EPSG:3857) Web Soil Survey URL:

Source of Map: Natural Resources Conservation Service

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Version 14, Sep 12, 2018 Survey Area Data:

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) serial images were photographed: May 14, 2010—Apr

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Severely Eroded Spot

Slide or Slip

Sinkhole

Sodic Spot

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
103C	Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes	0.8	65.7%
422B	Canton fine sandy loam, 0 to 8 percent slopes, extremely stony	0.4	34.3%
Totals for Area of Interest		1.2	100.0%



April 27, 2020

Soil Testing Summary
New Generation Homes Multifamily
Development
218-220 Main Street, Medway, MA

The following test pits were evaluated on this date by Soil Evaluator Janice Weldon

TP-1

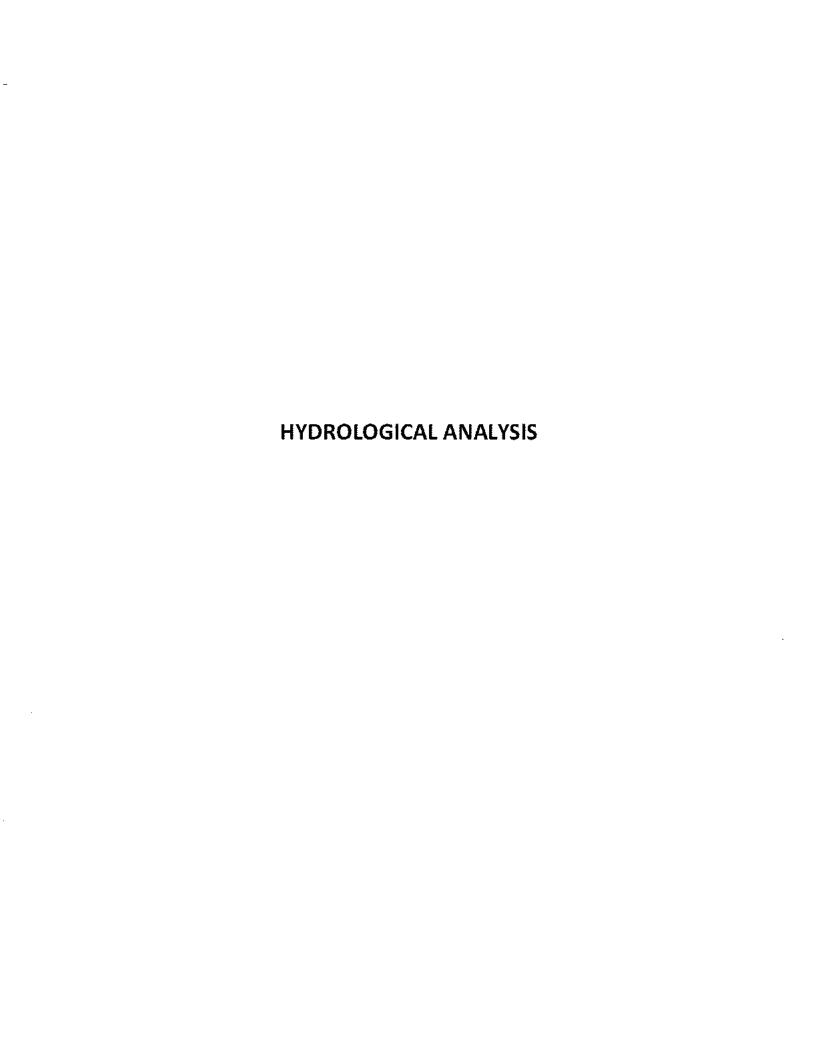
Surface elevation (existing)=228.5
0-10" Ap Sandy Loam
10"-24" Bw Fine Sandy Loam
24"-41" C1 Stony Fine Loamy Sand
41"-90"+ C2 Extremely Stony Loamy Sand
Roots to 36"
ESHGW Elev. 226.0
Refusal at Elev. 221.0

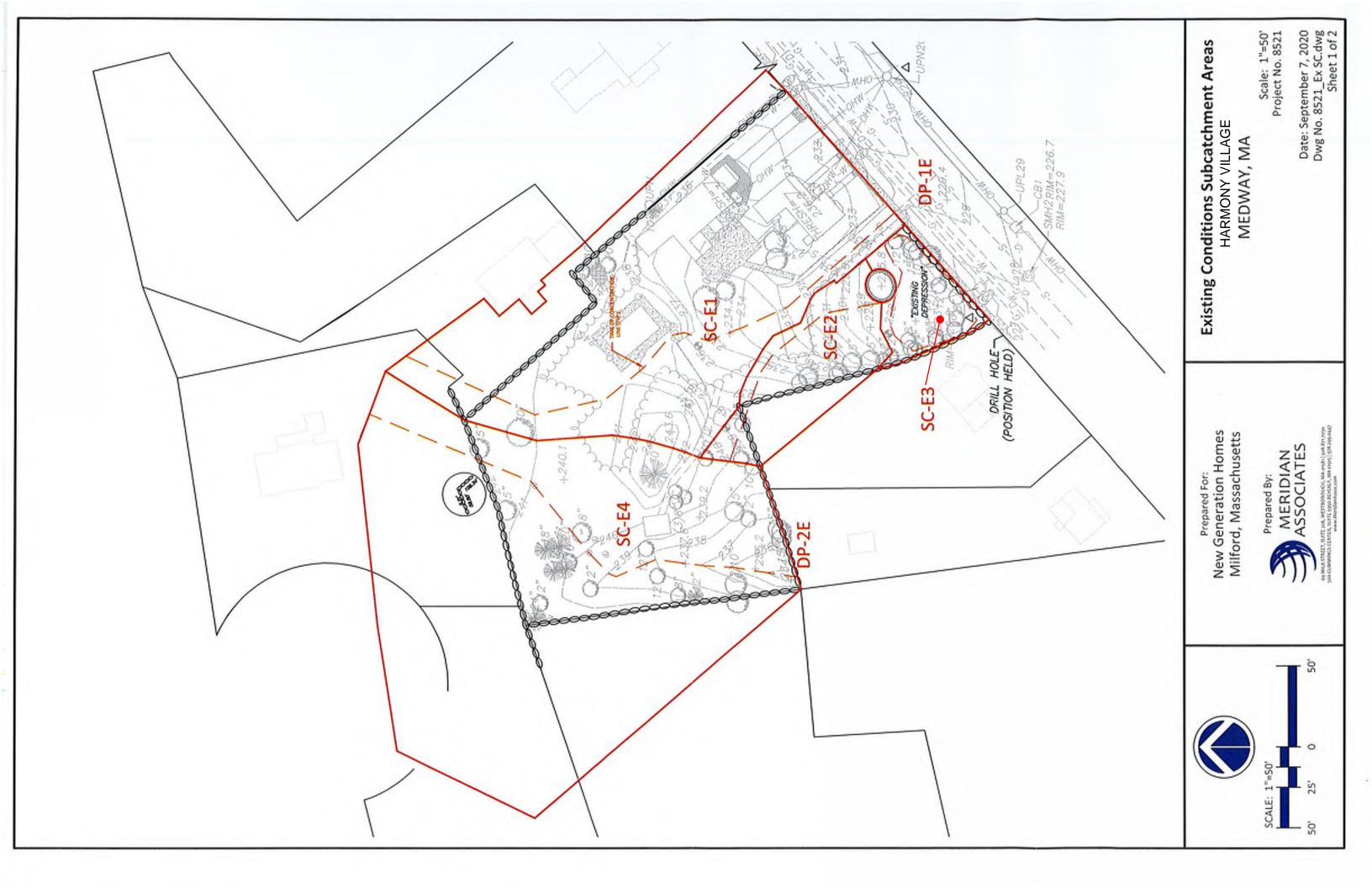
TP-2

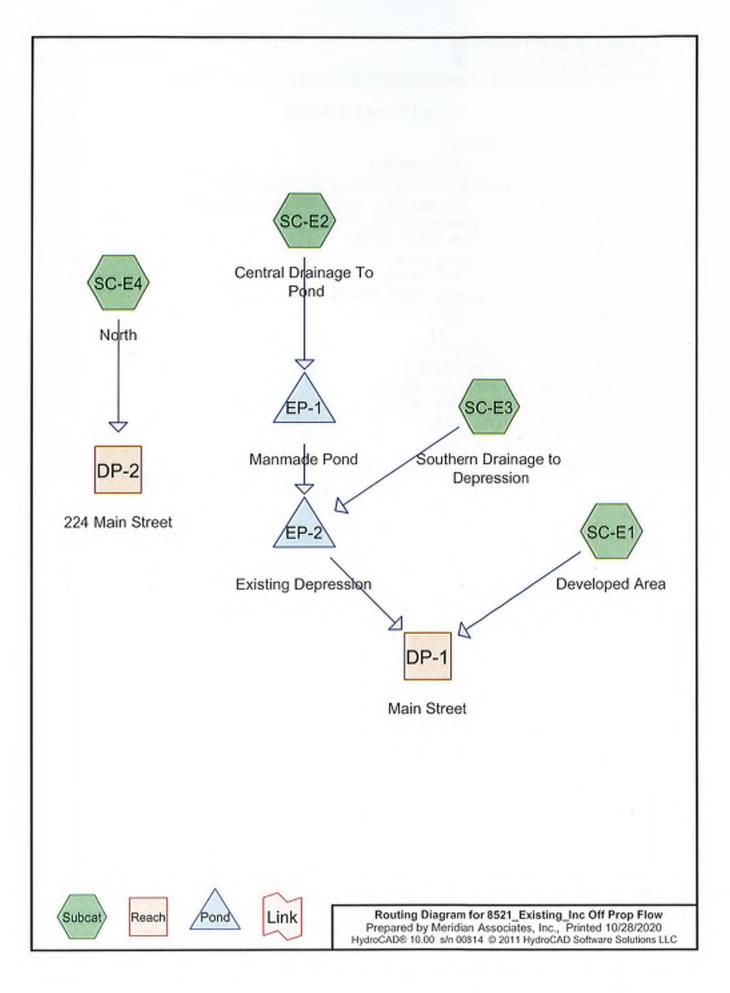
Surface Elevation (existing) = 235.5 0-10" Ap, Fine Sandy Loam 10"-14" Bw1, Stony Fine Sandy Loam 14"-31" Bw2, Stony Fine Loamy Sand 31"-46" C1, Stony Fine Sand 46"-81" C2, Extremely Stony Sand ESHGW Elev. 232.7 Refusal at Elev. 228.75

TP-3

Surface elevation (existing) = 239.0
0-10" Ap, Fine Sandy Loam
10"-27" Fill (10"-48" on south pit face)
27"-57" Bw Stony Fine Sandy Loam
57"-93"+ C, Fine Loamy Sand
Cobbles beginning at 10"
Large rocks and boulders at 57"
Roots to 60"
ESHGW Elev. 233.5
Refusal at Elev. 231.3







8521_Existing_Inc Off Prop Flow
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Area Listing (all nodes)

A	\rea (CN	Description
(s	q-ft)		(subcatchment-numbers)
65,	007	60	Woods, Fair, HSG B (SC-E1, SC-E2, SC-E3, SC-E4)
18,	456	61	>75% Grass cover, Good, HSG B (SC-E1, SC-E3, SC-E4)
	119	79	<50% Grass cover, Poor, HSG B (SC-E2)
	366	82	Gravel path (SC-E1, SC-E4)
1,	671	98	218 and patio (SC-E1)
1,	126	98	220 and patio (SC-E1)
	347	98	Paved parking, HSG B (SC-E2)
1,	165	98	Pool (SC-E1)
	196	98	Shed (SC-E4)
1,	774	98	concrete (SC-E1)
1,	499	98	pavement (SC-E1)
	298	98	retaining walls (SC-E1)
	27	98	stone walkway (SC-E1)
92,	051	64	TOTAL AREA

Page 3

Soil Listing (all nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
0	HSG A	
83,929	HSG B	SC-E1, SC-E2, SC-E3, SC-E4
0	HSG C	
0	HSG D	
8,122	Other	SC-E1, SC-E4
92,051		TOTAL AREA

8521_Existing_Inc Off Prop Flow
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Ground Covers (all nodes)

H\$G-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover
0	0	0	0	1,671	1,671	218 and patio
0	0	0	0	1,126	1,126	220 and patio
0	0	0	0	366	366	Gravel path
0	0	0	0	1,165	1,165	Pool
0	0	0	0	196	196	Shed
0	0	0	0	1,774	1,774	concrete
0	0	0	0	1,499	1,499	pavement
0	0	0	0	298	298	retaining walls
0	0	0	0	27	27	stone walkway
0	119	0	0	0	119	<50% Grass
						cover, Poor
0	18,456	0	0	0	18,456	>75% Grass
						cover, Good
0	347	0	0	0	347	Paved parking
0	65,007	0	0	0	65,007	Woods, Fair
0	83,929	0	0	8,122	92,051	TOTAL AREA
	(sq-ft) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(sq-ft) (sq-ft) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(sq-ft) (sq-ft) (sq-ft) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 119 0 0 347 0 0 65,007 0	(sq-ft) (sq-ft) (sq-ft) (sq-ft) 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 119 0 0 0 347 0 0 0 65,007 0 0	(sq-ft) (sq-ft) (sq-ft) (sq-ft) 0 0 0 0 1,671 0 0 0 0 1,126 0 0 0 0 366 0 0 0 0 1,165 0 0 0 0 196 0 0 0 0 1,774 0 0 0 0 1,499 0 0 0 0 298 0 0 0 0 27 0 119 0 0 0 0 347 0 0 0 0 65,007 0 0 0	(sq-ft) (sq-ft) (sq-ft) (sq-ft) (sq-ft) 0 0 0 1,671 1,671 0 0 0 0 1,126 1,126 0 0 0 0 366 366 0 0 0 0 1,165 1,165 0 0 0 0 196 196 0 0 0 0 1,774 1,774 0 0 0 0 1,499 1,499 0 0 0 0 298 298 0 0 0 0 119 0 119 0 0 0 119 0 18,456 0 0 0 347 0 65,007 0 0 0 65,007

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment SC-E1: Developed Area

Runoff Area=34,607 sf 21.85% Impervious Runoff Depth=0.88" Flow Length=936' Tc=21.5 min CN=69 Runoff=0.47 cfs 2,529 cf

Subcatchment SC-E2: Central Drainage To

Runoff Area=6,523 sf 5.32% Impervious Runoff Depth=0.56" Flow Length=109' Tc=6.9 min CN=62 Runoff=0.07 cfs 302 cf

SubcatchmentSC-E3: Southern Drainage to Runoff Area=3,338 sf 0.00% Impervious Runoff Depth=0.52" Tc=6.0 min CN=61 Runoff=0.03 cfs 143 cf

Subcatchment SC-E4: North

Runoff Area=47,583 sf 0.41% Impervious Runoff Depth=0.48" Flow Length=932' Tc=29.6 min CN=60 Runoff=0.24 cfs 1,890 cf

Reach DP-1: Main Street

Inflow=0.47 cfs 2.529 cf Outflow=0.47 cfs 2,529 cf

Reach DP-2: 224 Main Street

Inflow=0.24 cfs 1,890 cf Outflow=0.24 cfs 1,890 cf

Pond EP-1: Manmade Pond

Peak Elev=228.25' Storage=302 cf Inflow=0.07 cfs 302 cf

Outflow=0.00 cfs 0 cf

Pond EP-2: Existing Depression

Peak Elev=227.02' Storage=14 cf Inflow=0.03 cfs 143 cf

Discarded=0.02 cfs 143 cf Primary=0.00 cfs 0 cf Outflow=0.02 cfs 143 cf

Total Runoff Area = 92,051 sf Runoff Volume = 4,865 cf Average Runoff Depth = 0.63" 91.20% Pervious = 83,948 sf 8.80% Impervious = 8,103 sf

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Summary for Subcatchment SC-E1: Developed Area

Runoff

=

0.47 cfs @ 12.34 hrs, Volume=

2,529 cf, Depth= 0.88"

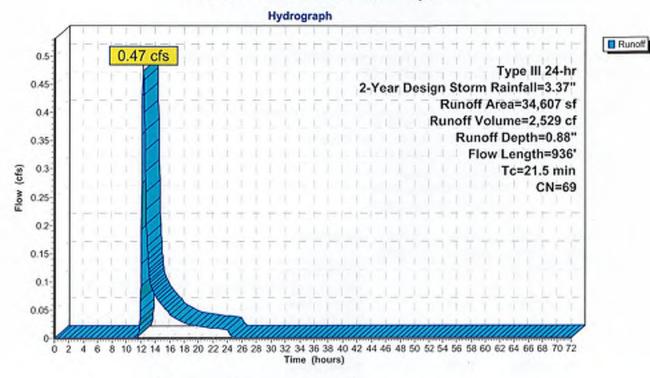
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

	F	Area (sf)	CN	Description							
*		1,165		98 Pool							
*		1,671		218 and patio							
*		1,126		220 and patio							
*		1,774		concrete	·						
*		27			otone walkway						
*		298		retaining wa	•						
*		1,499		pavement							
		10,828		Woods, Fai	r. HSG B						
*		197		Gravel path							
		16,022	61	>75% Grass	s cover, Go	ood, HSG B					
		34,607	69	Weighted A	verage	_					
		27,047		78.15% Per							
		7,560		21.85% lmp	pervious Are	ea					
				·							
	Tc	Length	Slope		Capacity	Description					
_	<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)						
_	(min) 9.0		(ft/ft) 0.0460		(cfs)	Sheet Flow,					
_	9.0	50	0.0460	0.09	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10"					
_		50		0.09	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow,					
	9.0 9.6	50 625	0.0460 0.0470	0.09	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps					
_	9.0	50	0.0460	0.09	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow,					
_	9.0 9.6 0.8	50 625 31	0.0460 0.0470 0.0150	0.09 0.08 0.61	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps					
_	9.0 9.6	50 625	0.0460 0.0470	0.09 0.08 0.61	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow,					
	9.0 9.6 0.8 1.1	50 625 31 66	0.0460 0.0470 0.0150 0.0200	0.09 1.08 0.61 0.99	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					
	9.0 9.6 0.8	50 625 31	0.0460 0.0470 0.0150	0.09 1.08 0.61 0.99	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,					
	9.0 9.6 0.8 1.1	50 625 31 66 10	0.0460 0.0470 0.0150 0.0200 0.3100	0.09 1.08 0.61 0.99 0.3.90	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					
	9.0 9.6 0.8 1.1	50 625 31 66	0.0460 0.0470 0.0150 0.0200	0.09 1.08 0.61 0.99 0.3.90	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,					
	9.0 9.6 0.8 1.1 0.0 0.6	50 625 31 66 10 59	0.0460 0.0470 0.0150 0.0200 0.3100 0.0500	0.09 1.08 0.61 0.99 0.3.90 1.57	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					
	9.0 9.6 0.8 1.1	50 625 31 66 10	0.0460 0.0470 0.0150 0.0200 0.3100	0.09 1.08 0.61 0.99 0.3.90 1.57	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,					
	9.0 9.6 0.8 1.1 0.0 0.6	50 625 31 66 10 59	0.0460 0.0470 0.0150 0.0200 0.3100 0.0500	0.09 1.08 0.61 0.99 0.3.90 1.57	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					

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Subcatchment SC-E1: Developed Area



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Summary for Subcatchment SC-E2: Central Drainage To Pond

Runoff

₩

0.07 cfs @ 12.13 hrs, Volume=

302 cf, Depth= 0.56"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

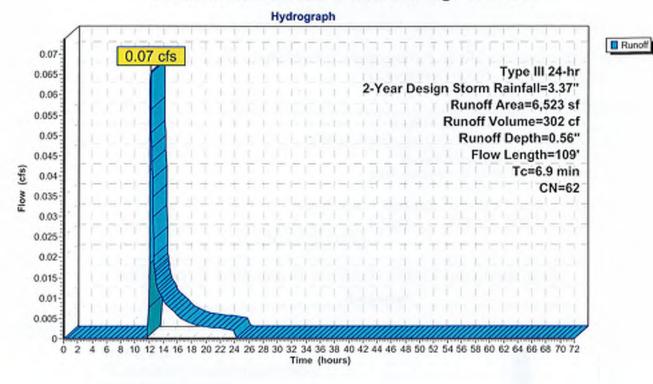
A	rea (sf)	CN_D	escription)						
	347 119			ing, HSG B					
	6,057		· ·						
	6,523		Veighted A	verage vious Area					
	6,176 347			ervious Area					
To	Length	Slope	Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
3.3	20	0.0900	0.10		Sheet Flow,				
1.7	9	0.1000	0.09		Woods: Light underbrush n= 0.400 P2= 3.10" Sheet Flow,				
1.7	J	0.1000	0.00		Woods: Light underbrush n= 0.400 P2= 3.10"				
0.3	4	0.1400	0.19		Sheet Flow,				
	_				Grass: Short n= 0.150 P2= 3.10"				
1.0	9	0.0500	0.15		Sheet Flow,				
0.1	7	0.0540	1.18		Grass: Short n= 0.150 P2= 3.10" Sheet Flow,				
V. ;	,	0.0040	1.10		Smooth surfaces n= 0.011 P2= 3.10"				
0.0	12	0.0700	5.37		Shallow Concentrated Flow,				
	_				Paved Kv= 20.3 fps				
0.0	3	0.0800	1.98		Shallow Concentrated Flow,				
0.5	45	0.0800	1.41		Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,				
			······································	***************************************	Woodland Kv= 5.0 fps				
6.9	109	Total							

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Subcatchment SC-E2: Central Drainage To Pond



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Summary for Subcatchment SC-E3: Southern Drainage to Depression

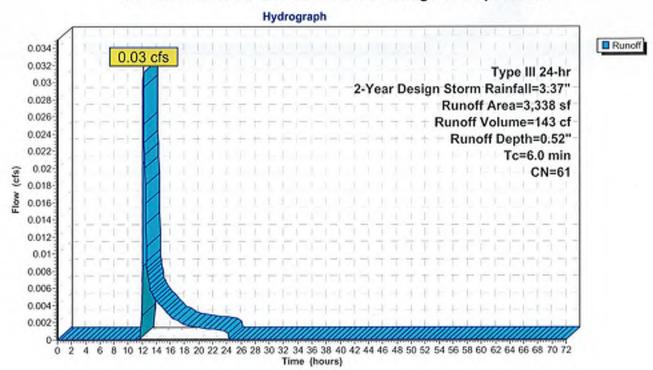
Runoff = 0.03 cfs @ 12.12 hrs, Volume=

143 cf, Depth= 0.52"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

Α	rea (sf)	CN	Description						
	1,000	60	Woods, Fair, HSG B						
	2,338	61	>75% Grass cover, Good, HSG B						
	3,338	61	Weighted A	verage					
	3,338		100.00% Pe	ervious Are	a				
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description				
6.0					Direct Entry, Min Tc				

Subcatchment SC-E3: Southern Drainage to Depression



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Summary for Subcatchment SC-E4: North

Runoff

0.24 cfs @ 12.55 hrs, Volume=

1,890 cf, Depth= 0.48"

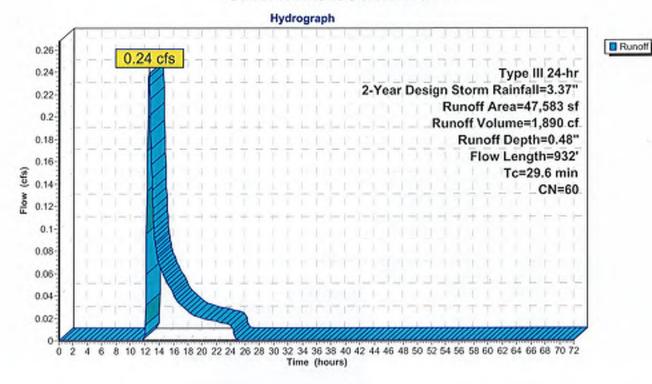
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

_	A	rea (sf)	CN D	escription							
*		196	98 S	Shed							
		96	61 >	>75% Grass cover, Good, HSG B							
*		169	82 G	Gravel path							
_		47,122	60 V	Woods, Fair, HSG B							
		47,583	,583 60 Weighted Average								
		47,387	9	9.59% Per	vious Area						
		196	0	.41% Impe	ervious Area	3					
				1.4.1. 1.							
	Tc	Length	Slope	Velocity	Capacity	Description					
*****	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	16.5	50	0.0100	0.05		Sheet Flow,					
		0.07	0.0500	4.40		Woods: Light underbrush n= 0.400 P2= 3.10"					
	10.2	687	0.0500	1.12		Shallow Concentrated Flow,					
	ο	00	0.0000	0.74		Woodland Kv= 5.0 fps					
	0.5	22	0.0200	0.71		Shallow Concentrated Flow,					
	1.0	53	0.0300	0.87		Woodland Kv= 5.0 fps					
	1.0	33	0.0500	0.07		Shallow Concentrated Flow, Woodland Kv= 5.0 fps					
	0.4	61	0.3200	2.83		Shallow Concentrated Flow,					
	U. -1	01	0.3200	2.00		Woodland Kv= 5.0 fps					
	1.0	59	0.0400	1.00		Shallow Concentrated Flow,					
		50	5.5.50			Woodland Kv= 5.0 fps					
	29.6	932	Total								

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Subcatchment SC-E4: North



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Summary for Reach DP-1: Main Street

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

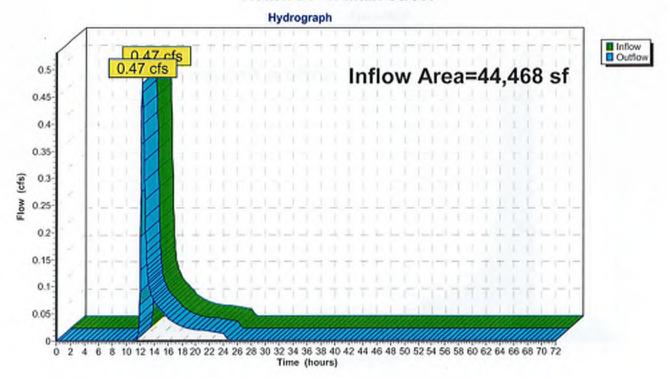
44,468 sf, 17.78% Impervious, Inflow Depth = 0.68" for 2-Year Design Storm event

Inflow 0.47 cfs @ 12.34 hrs, Volume= 2,529 cf

Outflow 0.47 cfs @ 12.34 hrs, Volume= 2,529 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-1: Main Street



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Summary for Reach DP-2: 224 Main Street

[40] Hint: Not Described (Outflow=Inflow)

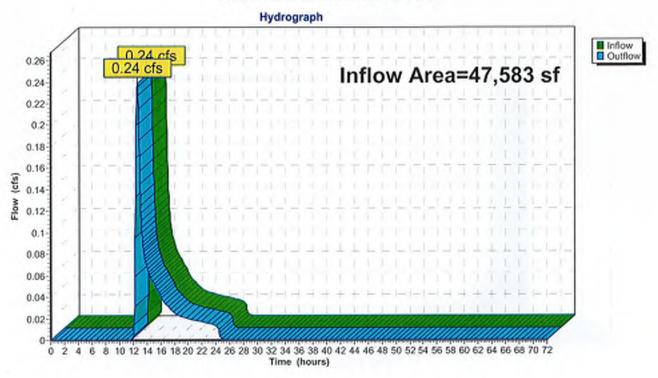
Inflow Area = 47,583 sf, 0.41% Impervious, Inflow Depth = 0.48" for 2-Year Design Storm event

Inflow = 0.24 cfs @ 12.55 hrs, Volume= 1,890 cf

Outflow = 0.24 cfs @ 12.55 hrs, Volume= 1,890 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-2: 224 Main Street



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Summary for Pond EP-1: Manmade Pond

Inflow Area = 6,523 sf, 5.32% Impervious, Inflow Depth = 0.56" for 2-Year Design Storm event

Inflow = 0.07 cfs @ 12.13 hrs, Volume= 302 cf

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2

Starting Elev= 127.00' Surf.Area= 0 sf Storage= 0 cf

Peak Elev= 228.25' @ 24.45 hrs Surf.Area= 290 sf Storage= 302 cf

Flood Elev= 228.50' Surf.Area= 311 sf Storage= 379 cf

Plug-Flow detention time= (not calculated: initial storage excedes outflow)

Center-of-Mass det. time= (not calculated: no outflow)

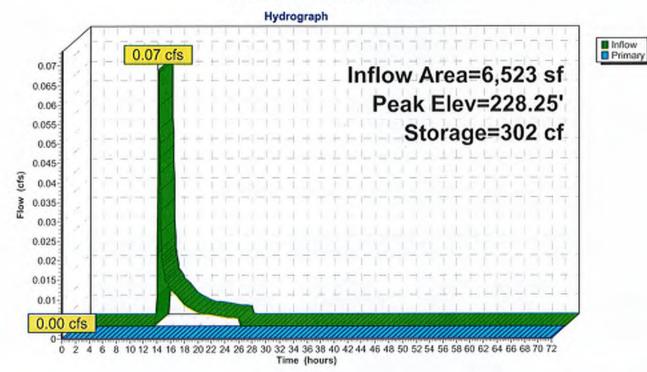
Volume	In√	ert Avail	Storage 3	Storage Description	า		
#1	227.	00'	379 cf	Custom Stage Dat	ta (Irregular)Listed	below (Recalc)	
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
227.0 228.5		198 311	50.1 62.7	0 379	0 379	198 339	
Device	Rouling	lnv	ert Outlet	Devices			
#1	Primary	228.	Head	ing x 18.8' breadt (feet) 0.20 0.40 0 (English) 2.68 2.7	0.60 0.80 1.00 1.2	20 1.40 1.60	

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=227.00' (Free Discharge)
1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond EP-1: Manmade Pond



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Summary for Pond EP-2: Existing Depression

[58] Hint: Peaked 99.02' above defined flood level

 Inflow Area =
 9,861 sf, 3.52% Impervious, Inflow Depth = 0.17" for 2-Year Design Storm event

 Inflow =
 0.03 cfs @ 12.12 hrs, Volume=
 143 cf

 Outflow =
 0.02 cfs @ 12.45 hrs, Volume=
 143 cf, Atten= 49%, Lag= 19.5 min

 Discarded =
 0.02 cfs @ 12.45 hrs, Volume=
 143 cf

 Primary =
 0.00 cfs @ 0.00 hrs, Volume=
 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 227.02' @ 12.45 hrs Surf.Area= 681 sf Storage= 14 cf Flood Elev= 128.00' Surf.Area= 0 sf Storage= 0 cf

Plug-Flow detention time= 8.4 min calculated for 143 cf (100% of inflow)

Center-of-Mass det. time= 8.4 min (916.8 - 908.4)

Volume	Inve	ert Avail.	.Storage	Storage Description	n	
#1	227.0	00'	1,285 cf	Custom Stage Da	ta (Irregular)Listed	below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
227.0	00	659	112.5	0	0	659
228.0	00	2,038	207.9	1,285	1,285	3,097
Device	Routing	Inv	ert Outle	et Devices		
#1	Primary	227.		long x 2.7' breadt		
						20 1.40 1.60 1.80 2.00
				3.00 3.50 4.00 4.		
						2.65 2.66 2.72 2.72
				2.86 3.00 3.10 3.		
#2	Discarde	d 227.0		in/hr Exfiltration		
			Cond	ductivity to Groundw	rater Elevation $= 0.0$	00,

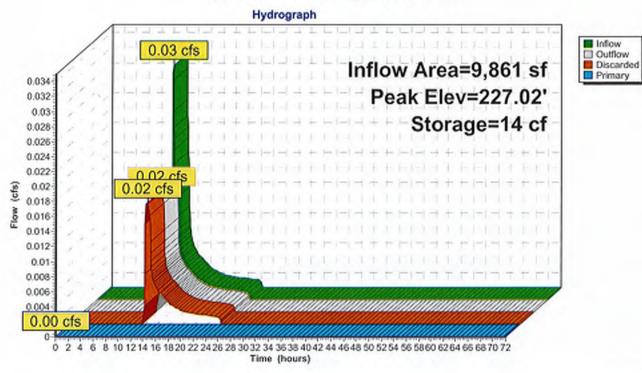
Discarded OutFlow Max=0.02 cfs @ 12.45 hrs HW=227.02' (Free Discharge) = 2=Exfiltration (Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=227.00' (Free Discharge) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond EP-2: Existing Depression



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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment SC-E1: Developed Area

Runoff Area=34,607 sf 21.85% Impervious Runoff Depth=2.15" Flow Length=936' Tc=21.5 min CN=69 Runoff=1.28 cfs 6,196 cf

Subcatchment SC-E2: Central Drainage To

Runoff Area=6,523 sf 5.32% Impervious Runoff Depth=1.60" Flow Length=109' Tc=6.9 min CN=62 Runoff=0.25 cfs 870 cf

SubcatchmentSC-E3: Southern Drainage to Runoff Area=3,338 sf 0.00% Impervious Runoff Depth=1.53" Tc=6.0 min CN=61 Runoff=0.12 cfs 425 cf

Subcatchment SC-E4: North

Runoff Area=47,583 sf 0.41% Impervious Runoff Depth=1.46" Flow Length=932' Tc=29.6 min CN=60 Runoff=0.97 cfs 5,771 cf

Reach DP-1: Main Street

Inflow=1.28 cfs 6.196 cf Outflow=1.28 cfs 6.196 cf

Reach DP-2: 224 Main Street

Inflow=0.97 cfs 5,771 cf Outflow=0.97 cfs 5,771 cf

Pond EP-1: Manmade Pond

Peak Elev=228.54' Storage=379 cf Inflow=0.25 cfs 870 cf

Outflow=0.08 cfs 695 cf

Pond EP-2: Existing Depression

Peak Elev=227.45' Storage=413 cf Inflow=0.12 cfs 1,120 cf Discarded=0.03 cfs 1,120 cf Primary=0.00 cfs 0 cf Outflow=0.03 cfs 1,120 cf

Total Runoff Area = 92,051 sf Runoff Volume = 13,263 cf Average Runoff Depth = 1.73" 91.20% Pervious = 83,948 sf 8.80% Impervious = 8,103 sf

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Summary for Subcatchment SC-E1: Developed Area

Runoff

1.28 cfs @ 12.31 hrs, Volume=

6,196 cf, Depth= 2.15"

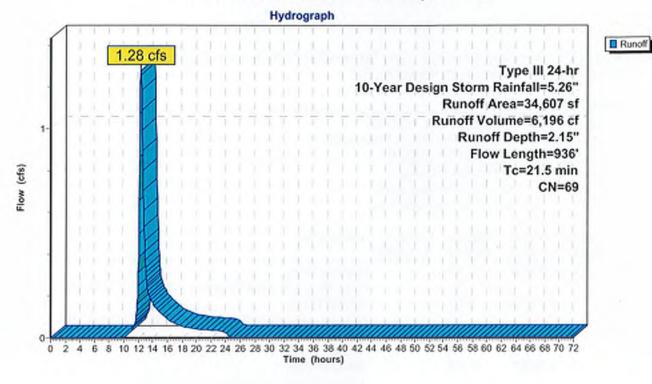
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

	Α	rea (sf)	CN [Description						
*		1,165	98 F	98 Pool						
*		1,671	98 2	18 and pat	tio					
*		1,126		20 and pat						
*		1,774		oncrete on the second s						
*		27	98 s	tone walkway						
*		298		etaining walls						
*		1,499	98 p	avement						
		10,828	60 V	Voods, Fail	r, HSG B					
*		197	82 (3ravel path						
		16,022	61 >	·75% Grass	s cover, Go	ood, HSG B				
		34,607	69 V	Veighted A	verage					
		27,047	7	'8.15% Per	vious Area					
		7,560	2	1.85% lmp	ervious Are	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	9.0	50	0.0460	0.09		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.10"				
	9.6	625								
		02.0	0.0470	1.08		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	0.8	31	0.0470	1.08 0.61		Woodland Kv= 5.0 fps Shallow Concentrated Flow,				
		31	0.0150	0.61		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps				
	0.8	31				Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow,				
	1.1	31 66	0.0150 0.0200	0.61 0.99		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				
		31	0.0150	0.61		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,				
	1.1 0.0	31 66 10	0.0150 0.0200 0.3100	0.61 0.99 3.90		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				
	1.1	31 66	0.0150 0.0200	0.61 0.99		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,				
	1.1 0.0 0.6	31 66 10 59	0.0150 0.0200 0.3100 0.0500	0.61 0.99 3.90 1.57		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				
	1.1 0.0	31 66 10	0.0150 0.0200 0.3100	0.61 0.99 3.90		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,				
***************************************	1.1 0.0 0.6	31 66 10 59	0.0150 0.0200 0.3100 0.0500	0.61 0.99 3.90 1.57		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				

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Subcatchment SC-E1: Developed Area



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Summary for Subcatchment SC-E2: Central Drainage To Pond

Runoff :

0.25 cfs @ 12.11 hrs, Volume=

870 cf, Depth= 1.60"

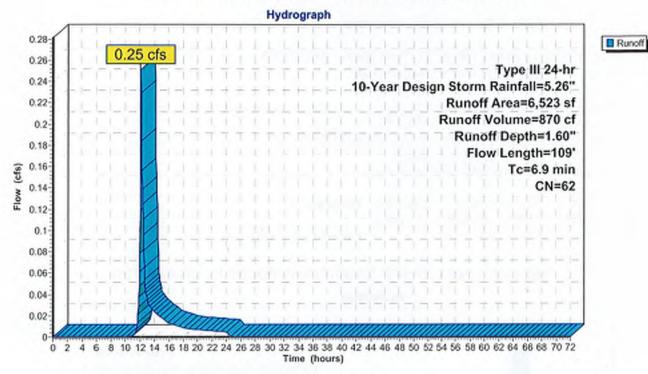
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

Д	rea (sf)	CN I	Description		
	347 98 Paved parking, H 119 79 <50% Grass cove				
	6,057		Noods, Fai	·	
	6,523	62 \	Neighted A	verage	
	6,176	ξ	94.68% Per	vious Area	
	347	ŧ	5.32% Impe	ervious Area	a
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.3	20	0.0900	0.10		Sheet Flow,
	_				Woods: Light underbrush n= 0.400 P2= 3.10"
1.7	9	0.1000	0.09		Sheet Flow,
Λ 2	,	0.1400	0.40		Woods: Light underbrush n= 0.400 P2= 3.10"
0.3	4	0.1400	0.19		Sheet Flow, Grass: Short n= 0.150 P2= 3.10"
1.0	9	0.0500	0.15		Sheet Flow,
1.0	•	0.0000	0.10		Grass: Short n= 0.150 P2= 3.10"
0.1	7	0.0540	1.18		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.10"
0.0	12	0.0700	5.37		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.0	3	0.0800	1.98		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.5	45	0.0800	1.41		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
6.9	109	Total			

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Subcatchment SC-E2: Central Drainage To Pond



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Summary for Subcatchment SC-E3: Southern Drainage to Depression

Runoff

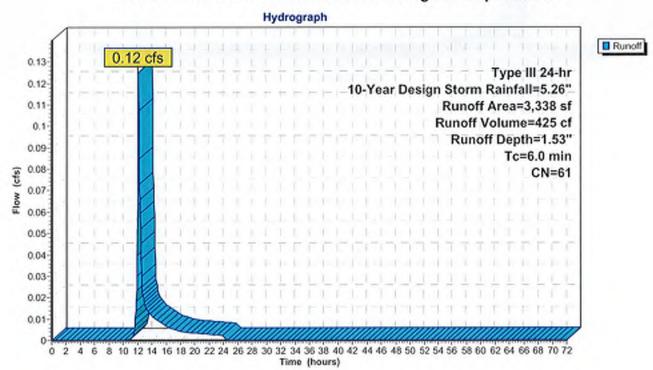
0.12 cfs @ 12.10 hrs, Volume=

425 cf, Depth= 1.53"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

Α	rea (sf)	CN	Description						
	1,000	60	Woods, Fai	/oods, Fair, HSG B					
	2,338	61	75% Grass cover, Good, HSG B						
	3,338 3,338	61	Weighted A 100.00% Pe		ea				
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description				
6.0					Direct Entry, Min Tc				

Subcatchment SC-E3: Southern Drainage to Depression



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Summary for Subcatchment SC-E4: North

Runoff 0.97 cfs @ 12.46 hrs, Volume=

5,771 cf, Depth= 1.46"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

	А	rea (sf)	CN D	escription						
*		196	98 S	ihed						
		96	61 >	61 >75% Grass cover, Good, HSG B						
*		169	82 G	Fravel path						
_		47,122	60 V	Voods, Fai	r, HSG B					
		47,583	60 V	Veighted A	verage					
		47,387	9	9.59% Per	vious Area					
		196	0	.41% Impe	ervious Area	a				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	16.5	50	0.0100	0.05		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.10"				
	10.2	687	0.0500	1.12		Shallow Concentrated Flow,				
	0.5	-00	0.0000	0.54		Woodland Kv= 5.0 fps				
	0.5	22	0.0200	0.71		Shallow Concentrated Flow,				
	4.0	# 2	0.0000	0.07		Woodland Kv= 5.0 fps				
	1.0	53	0.0300	0.87		Shallow Concentrated Flow,				
	0.4	61	0.3200	2.83		Woodland Kv= 5.0 fps Shallow Concentrated Flow,				
	U.~	O r	0.5200	2.00		Woodland Kv= 5.0 fps				
	1.0	59	0.0400	1.00		Shallow Concentrated Flow,				
		00	010 400	1.00		Woodland Kv= 5.0 fps				
	29.6	932	Total							

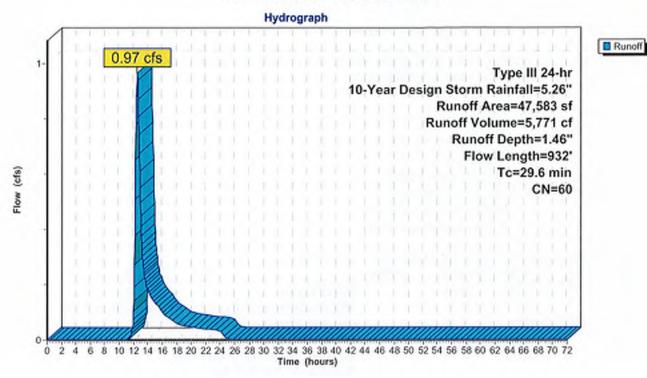
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Subcatchment SC-E4: North



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Summary for Reach DP-1: Main Street

[40] Hint: Not Described (Outflow=Inflow)

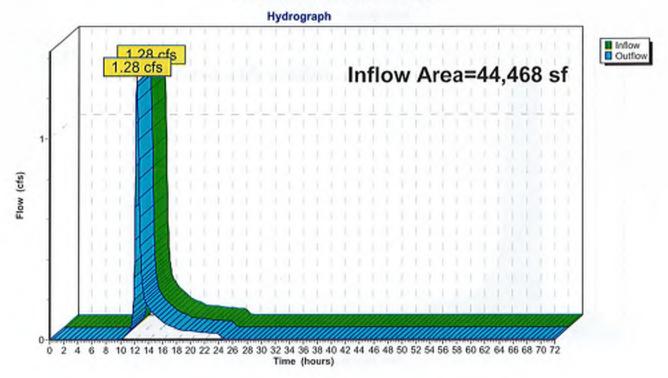
Inflow Area = 44,468 sf, 17.78% Impervious, Inflow Depth = 1.67" for 10-Year Design Storm event

Inflow = 1.28 cfs @ 12.31 hrs, Volume= 6,196 cf

Outflow = 1.28 cfs @ 12.31 hrs, Volume= 6,196 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-1: Main Street



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Summary for Reach DP-2: 224 Main Street

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

47,583 sf, 0.41% Impervious, Inflow Depth = 1.46" for 10-Year Design Storm event

Inflow

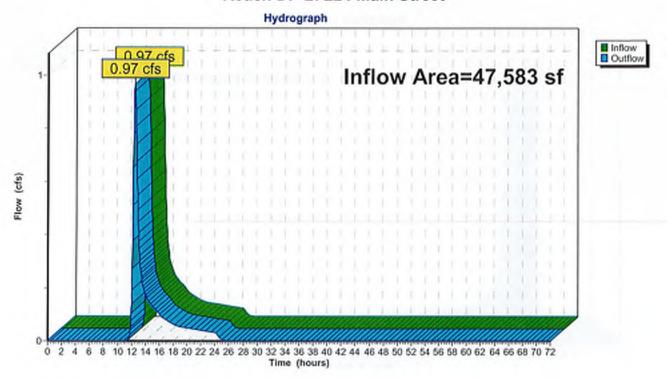
Outflow

0.97 cfs @ 12.46 hrs, Volume= 0.97 cfs @ 12.46 hrs, Volume= 5,771 cf

5,771 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-2: 224 Main Street



8521_Existing_Inc Off Prop Flow

Type III 24-hr 10-Year Design Storm Rainfall=5.26"

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Summary for Pond EP-1: Manmade Pond

[93] Warning: Storage range exceeded by 0.04' [58] Hint: Peaked 0.04' above defined flood level

Inflow Area = 6,523 sf, 5.32% Impervious, Inflow Depth = 1.60" for 10-Year Design Storm event

Inflow = 0.25 cfs @ 12.11 hrs, Volume= 870 cf

Outflow = 0.08 cfs @ 12.62 hrs, Volume= 695 cf, Atten= 67%, Lag= 30.6 min

Primary = 0.08 cfs @ 12.62 hrs, Volume= 695 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2

Starting Elev= 127.00' Surf.Area= 0 sf Storage= 0 cf

Peak Elev= 228.54' @ 12.60 hrs Surf.Area= 311 sf Storage= 379 cf

Flood Elev= 228.50' Surf.Area= 311 sf Storage= 379 cf

Plug-Flow detention time= 156.9 min calculated for 695 cf (80% of inflow)

Center-of-Mass det. time= 73.8 min (940.5 - 866.8)

Volume	Inv	ert Avail	.Storage 🧐	Storage Description	າ		
#1	227.0	00'	379 cf	Custom Stage Dat	ta (Irregular)Listed	below (Recalc)	
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
227.0 228.5		198 311	50.1 62.7	0 379	0 379	198 339	
Device	Routing	lnv	ert Outlet	Devices			<u>-</u>
#1	Primary	228.	Head	(feet) 0.20 0.40 (h Broad-Crested F 0.60 0.80 1.00 1.2 70 2.70 2.64 2.63	20 1.40 1.60	

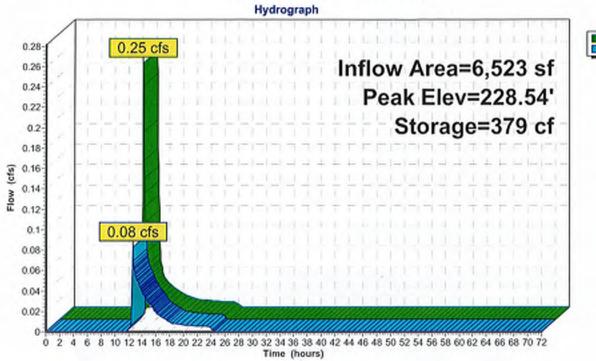
Primary OutFlow Max=0.07 cfs @ 12.62 hrs HW=228.54' (Free Discharge)
1=Broad-Crested Rectangular Weir (Weir Controls 0.07 cfs @ 0.58 fps)

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Pond EP-1: Manmade Pond





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Summary for Pond EP-2: Existing Depression

[58] Hint: Peaked 99.45' above defined flood level

9,861 sf, 3.52% Impervious, Inflow Depth = 1.36" for 10-Year Design Storm event Inflow Area = Inflow 0.12 cfs @ 12.10 hrs, Volume= 1,120 cf 0.03 cfs @ 15.71 hrs, Volume= 0.03 cfs @ 15.71 hrs, Volume= 1,120 cf, Atten= 77%, Lag= 216.5 min Outflow

Discarded = 1,120 cf 0.00 cfs @ 0.00 hrs. Volume= 0 cf Primary

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 227.45' @ 15.71 hrs Surf.Area= 1,190 sf Storage= 413 cf Flood Elev= 128.00' Surf.Area= 0 sf Storage= 0 cf

Plug-Flow detention time= 172.5 min calculated for 1,119 cf (100% of inflow)

Center-of-Mass det. time= 172.4 min (1,085.7 - 913.3)

Volume	Inver	t Avail.St	orage	Storage Description	n		
#1	227.00	1,2	285 cf	Custom Stage Da	ta (Irregular)Liste	d below (Recalc)	
Elevatio		urf.Area l (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
227.0 228.0	-	659 2,038	112.5 207.9	0 1,285	0 1,285	659 3,097	
Device	Routing	Invert	Outle	et Devices			
#1	Primary	227.90'	Head 2.50 Coef	83.7' long x 2.7' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 Coef. (English) 2.46 2.59 2.63 2.63 2.64 2.65 2.66 2.72 2.72 2.74 2.86 3.00 3.10 3.22 3.32			
#2	Discarded	227.00'	1.02	2.86 3.00 3.10 3. 0 In/hr Exfiltration ductivity to Groundw	over Surface area		

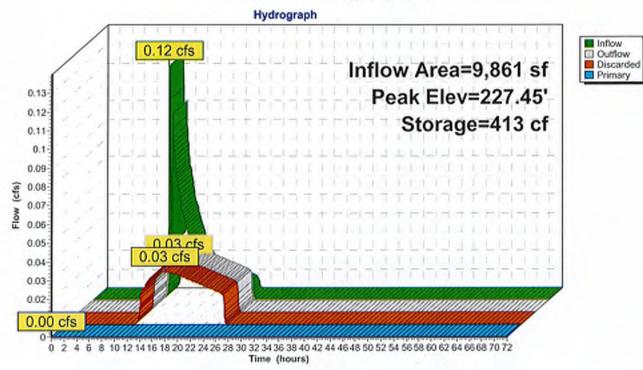
Discarded OutFlow Max=0.03 cfs @ 15.71 hrs HW=227.45' (Free Discharge) T-2=Exfiltration (Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=227.00' (Free Discharge) -1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond EP-2: Existing Depression



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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment SC-E1: Developed Area

Runoff Area=34,607 sf 21.85% Impervious Runoff Depth=4.57"

Flow Length=936' Tc=21.5 min CN=69 Runoff=2.78 cfs 13,184 cf

Subcatchment SC-E2: Central Drainage To Runoff Area=6,523 sf 5.32% Impervious Runoff Depth=3.76" Flow Length=109' Tc=6.9 min CN=62 Runoff=0.63 cfs 2,043 cf

Subcatchment SC-E3: Southern Drainage to Runoff Area=3,338 sf 0.00% Impervious Runoff Depth=3.64" Tc=6.0 min CN=61 Runoff=0.32 cfs 1,014 cf

Subcatchment SC-E4: North

Runoff Area=47,583 sf 0.41% Impervious Runoff Depth=3.53"
Flow Length=932' Tc=29.6 min CN=60 Runoff=2.53 cfs 13,996 cf

 Reach DP-1: Main Street
 Inflow=2.78 cfs
 13,201 cf

 Outflow=2.78 cfs
 13,201 cf

Reach DP-2: 224 Main StreetInflow=2.53 cfs 13,996 cf
Outflow=2.53 cfs 13,996 cf

Pond EP-1: Manmade Pond Peak Elev=228.68' Storage=379 cf Inflow=0.63 cfs 2,043 cf Outflow=0.59 cfs 1,048 cf

Pond EP-2: Existing Depression Peak Elev=227.90' Storage=1,092 cf Inflow=0.91 cfs 2,062 cf Discarded=0.04 cfs 2,045 cf Primary=0.02 cfs 17 cf Outflow=0.06 cfs 2,062 cf

Total Runoff Area = 92,051 sf Runoff Volume = 30,236 cf Average Runoff Depth = 3.94" 91.20% Pervious = 83,948 sf 8.80% Impervious = 8,103 sf

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Summary for Subcatchment SC-E1: Developed Area

Runoff

2.78 cfs @ 12.30 hrs, Volume=

13,184 cf, Depth= 4.57"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

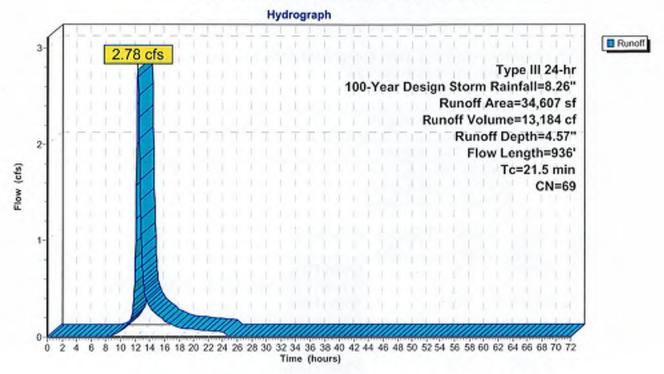
	A	Area (sf)	CN [Description					
*		1,165	98 F	Pool					
*		1,671	98 2	98 218 and patio					
*		1,126		·					
*		1,774		concrete					
*		27	98 8	stone walky	vav				
*		298		etaining wa	•				
*		1,499		pavement					
		10,828		Noods, Fair	r, HSG B				
*		197		Gravel path					
		16,022		•		ood, HSG B			
		34,607	69 \	Veighted A	verage				
		27,047			vious Area				
		7,560	2	21.85% lmp	ervious Ar	ea			
		•							
	Tc	Length	Slope	Velocity	Capacity	Description			
			10,00	44.1					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
_	(min) 9.0		(ft/ft) 0.0460	(ft/sec) 0.09	(cfs)	Sheet Flow,			
_	9.0	50	0.0460	0.09	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10"			
		50			(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow,			
_	9.0 9.6	50 625	0.0460 0.0470	0.09 1.08	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
_	9.0	50 625	0.0460	0.09	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow,			
_	9.0 9.6 0.8	50 625 31	0.0460 0.0470 0.0150	0.09 1.08 0.61	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
	9.0 9.6	50 625	0.0460 0.0470	0.09 1.08	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow,			
	9.0 9.6 0.8 1.1	50 625 31 66	0.0460 0.0470 0.0150 0.0200	0.09 1.08 0.61 0.99	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps			
	9.0 9.6 0.8	50 625 31 66	0.0460 0.0470 0.0150	0.09 1.08 0.61	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,			
	9.0 9.6 0.8 1.1 0.0	50 625 31 66 10	0.0460 0.0470 0.0150 0.0200 0.3100	0.09 1,08 0.61 0.99 3.90	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps			
	9.0 9.6 0.8 1.1	50 625 31 66 10	0.0460 0.0470 0.0150 0.0200	0.09 1.08 0.61 0.99	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,			
	9.0 9.6 0.8 1.1 0.0	50 625 31 66 10	0.0460 0.0470 0.0150 0.0200 0.3100 0.0500	0.09 1.08 0.61 0.99 3.90 1.57	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps			
	9.0 9.6 0.8 1.1 0.0	50 625 31 66 10	0.0460 0.0470 0.0150 0.0200 0.3100	0.09 1,08 0.61 0.99 3.90	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,			
	9.0 9.6 0.8 1.1 0.0	50 625 31 66 10 59	0.0460 0.0470 0.0150 0.0200 0.3100 0.0500	0.09 1.08 0.61 0.99 3.90 1.57	(cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps			

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Subcatchment SC-E1: Developed Area



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Summary for Subcatchment SC-E2: Central Drainage To Pond

Runoff

0.63 cfs @ 12.11 hrs, Volume=

2,043 cf, Depth= 3.76"

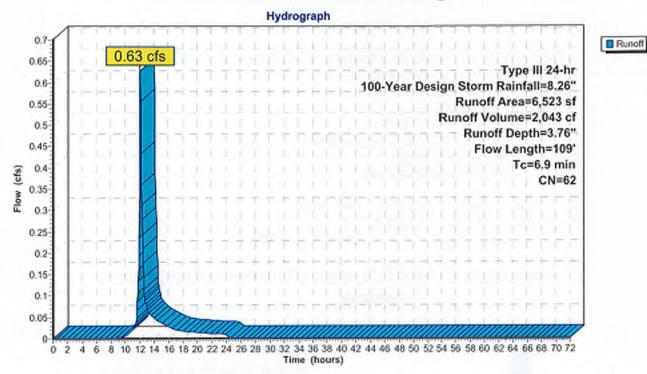
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

	Α	rea (sf)	CN E	Description		
		347	98 F	Paved park	ing, HSG B	3
		119			s cover, Po	or, HSGB
		6,057	60 V	<u> Voods, Fai</u>	r, HSG B	
		6,523	62 V	Neighted A	verage	
		6,176	ç	94.68% Pe	rvious Area	
		347	8	5.32% Impe	ervious Area	a
	Tc	Length	Slope	Velocity		Description
<u>(n</u>	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	3.3	20	0.0900	0.10		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.10"
	1.7	9	0.1000	0.09		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.10"
	0.3	4	0.1400	0.19		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.10"
	1.0	9	0.0500	0.15		Sheet Flow,
						Grass: Short n= 0,150 P2= 3,10"
	0.1	7	0.0540	1.18		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.10"
	0.0	12	0.0700	5.37		Shallow Concentrated Flow,
		_				Paved Kv= 20.3 fps
	0.0	3	0.0800	1.98		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.5	45	0.0800	1.41		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	6.9	109	Total			

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Subcatchment SC-E2: Central Drainage To Pond



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Summary for Subcatchment SC-E3: Southern Drainage to Depression

Runoff

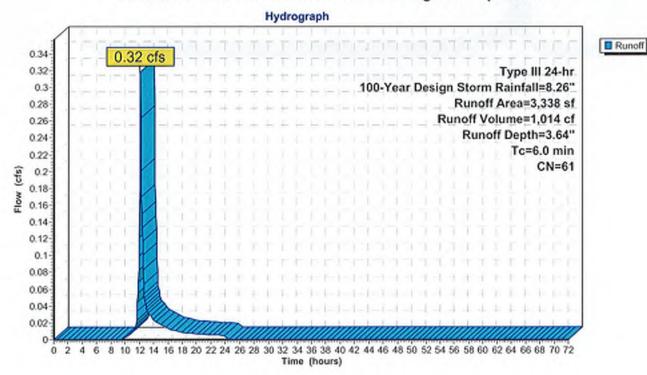
0.32 cfs @ 12.10 hrs, Volume=

1,014 cf, Depth= 3.64"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

A	rea (sf)	CN	Description						
	1,000	60	Woods, Fai	Voods, Fair, HSG B					
	2,338	61	>75% Gras	75% Grass cover, Good, HSG B					
	3,338 3,338	61	Weighted Average 100.00% Pervious Area						
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description	1.0			
6.0					Direct Entry, Min Tc				

Subcatchment SC-E3: Southern Drainage to Depression



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Summary for Subcatchment SC-E4: North

Runoff = 2.53 cfs @ 12.43 hrs, Volume=

13,996 cf, Depth= 3.53"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

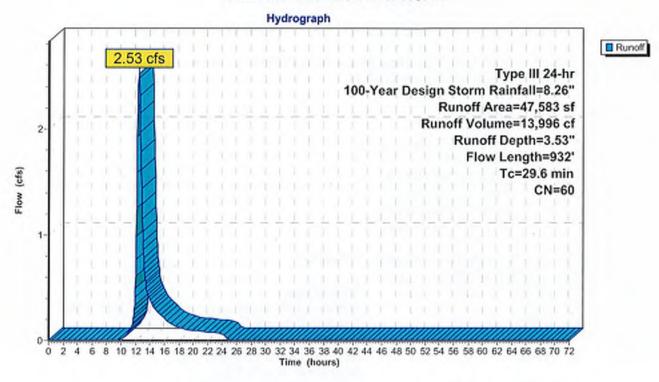
	Δ	rea (sf)	CN E	escription						
*		196	98 S	Shed						
		96	61 >	>75% Grass cover, Good, HSG B						
*		169		aravel path	-					
		47,122	60 V	Voods, Fai	r, HSG B					
		47,583	60 V	Veighted A	verage					
		47,387			vious Area					
		196	0	.41% Impe	ervious Area	3				
				•						
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	16.5	50	0.0100	0.05		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.10"				
	10.2	687	0.0500	1.12		Shailow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	0.5	22	0.0200	0.71		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	1.0	53	0.0300	0.87		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	0.4	61	0.3200	2.83		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	1.0	59	0.0400	1.00		Shallow Concentrated Flow,				
_						Woodland Kv= 5.0 fps				
	29.6	932	Total							

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Subcatchment SC-E4: North



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Summary for Reach DP-1: Main Street

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =

44,468 sf, 17.78% Impervious, Inflow Depth = 3.56" for 100-Year Design Storm event

Inflow

2.78 cfs @ 12.30 hrs, Volume=

13,201 cf

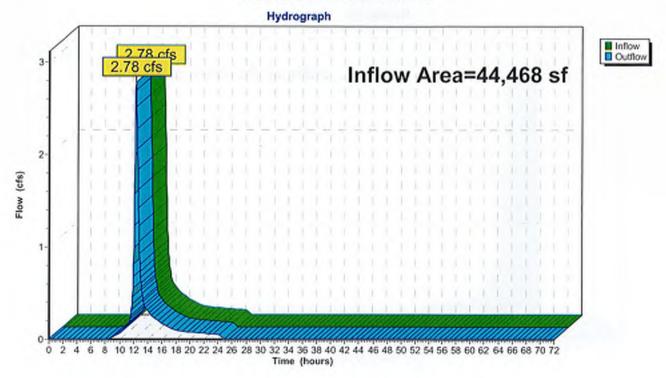
Outflow

2.78 cfs @ 12.30 hrs, Volume=

13,201 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-1: Main Street



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Summary for Reach DP-2: 224 Main Street

[40] Hint: Not Described (Outflow=Inflow)

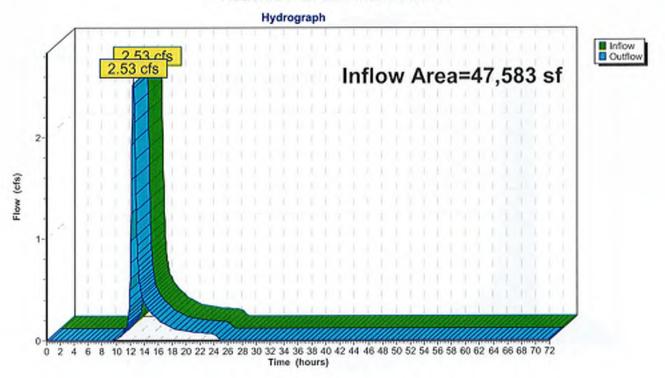
Inflow Area = 47,583 sf, 0.41% Impervious, Inflow Depth = 3.53" for 100-Year Design Storm event

Inflow = 2.53 cfs @ 12.43 hrs, Volume= 13,996 cf

Outflow = 2.53 cfs @ 12.43 hrs, Volume= 13,996 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-2: 224 Main Street



8521_Existing_Inc Off Prop Flow

Type III 24-hr 100-Year Design Storm Rainfall=8.26"

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Summary for Pond EP-1: Manmade Pond

[93] Warning: Storage range exceeded by 0.18' [58] Hint: Peaked 0.18' above defined flood level

Inflow Area = 6,523 sf, 5.32% Impervious, Inflow Depth = 3.76" for 100-Year Design Storm event

0.63 cfs @ 12.11 hrs, Volume= 0.59 cfs @ 12.11 hrs, Volume= 2.043 cf

1,048 cf, Atten= 6%, Lag= 0.0 min

Inflow =
Outflow =
Primary = 0.59 cfs @ 12.11 hrs, Volume= 1,048 cf

Routing by Stor-Ind method, Time Span= 0.00-72,00 hrs, dt= 0.05 hrs / 2

Starting Elev= 127.00' Surf.Area= 0 sf Storage= 0 cf

Peak Elev= 228.68' @ 12.11 hrs Surf.Area= 311 sf Storage= 379 cf

Flood Elev= 228.50' Surf.Area= 311 sf Storage= 379 cf

Plug-Flow detention time= 125.0 min calculated for 1,047 cf (51% of inflow)

Center-of-Mass det. time= 5.5 min (846.5 - 841.0)

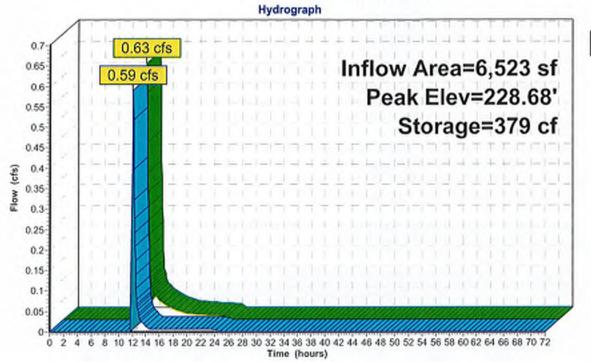
Volume	Inv	ert Avail	.Storage	Storage Description	on		
#1	227.	00'	379 cf	Custom Stage D	ata (Irregular)Liste	ed below (Recalc)	
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
227.0 228.5		198 311	50.1 62.7	0 379	0 379	198 339	
Device	Routing	Inv	ert Outle	et Devices			
#1	Primary	228.	Hea	d (feet) 0.20 0.40	0.60 0.80 1.00 1	d Rectangular Weir 1.20 1.40 1.60 33 2.64 2.64 2.63	

Primary OutFlow Max=0.58 cfs @ 12.11 hrs HW=228.68' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 0.58 cfs @ 1.16 fps)

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Pond EP-1: Manmade Pond





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Summary for Pond EP-2: Existing Depression

[58] Hint: Peaked 99.90' above defined flood level

Inflow Area = 9,861 sf, 3.52% Impervious, Inflow Depth = 2.51" for 100-Year Design Storm event

Inflow = 0.91 cfs @ 12.10 hrs, Volume= 2,062 cf

Outflow = 0.06 cfs @ 13.16 hrs, Volume= 2,062 cf, Atten= 93%, Lag= 63.8 min

Discarded = 0.04 cfs @ 13.16 hrs, Volume= 2,045 cf
Primary = 0.02 cfs @ 13.16 hrs, Volume= 17 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 227.90' @ 13.16 hrs Surf.Area= 1,867 sf Storage= 1,092 cf

Flood Elev= 128.00' Surf.Area= 0 sf Storage= 0 cf

Plug-Flow detention time= 294.3 min calculated for 2,060 cf (100% of inflow)

Center-of-Mass det. time= 294.3 min (1,138.7 - 844.4)

Volume	Inver	t Avail.S	torage	Storage Description				
#1	227.00) ' 1,	,285 cf	Custom Stage Dat	a (Irregular)Listed	below (Recalc)		
Elevation (fee	-	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)		
227.0		659	112.5	0	0	659		
228.0	00	2,038	207.9	1,285	1,285	3,097		
Device	Routing	Inver	t Outle	et Devices				
#1	Primary	227.90	Head 2.50 Coef	3.00 3.50 4.00 4.5 English) 2.46 2.5 (English)	.60 0.80 1.00 1.2 50 9 2.63 2.63 2.64	Rectangular Weir 20 1.40 1.60 1.80 2.00 2.65 2.66 2.72 2.72		
#2	Discarded	227.00) 1.020	2.86 3.00 3.10 3.2 Din/hr Exfiltration of ductivity to Groundwa	ver Surface area	90,		

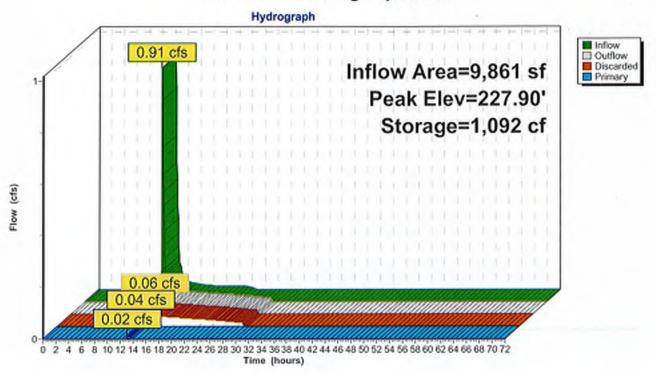
Discarded OutFlow Max=0.04 cfs @ 13.16 hrs HW=227.90' (Free Discharge) = 2=Exfiltration (Controls 0.04 cfs)

Primary OutFlow Max=0.00 cfs @ 13.16 hrs HW=227.90' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 0.00 cfs @ 0.07 fps)

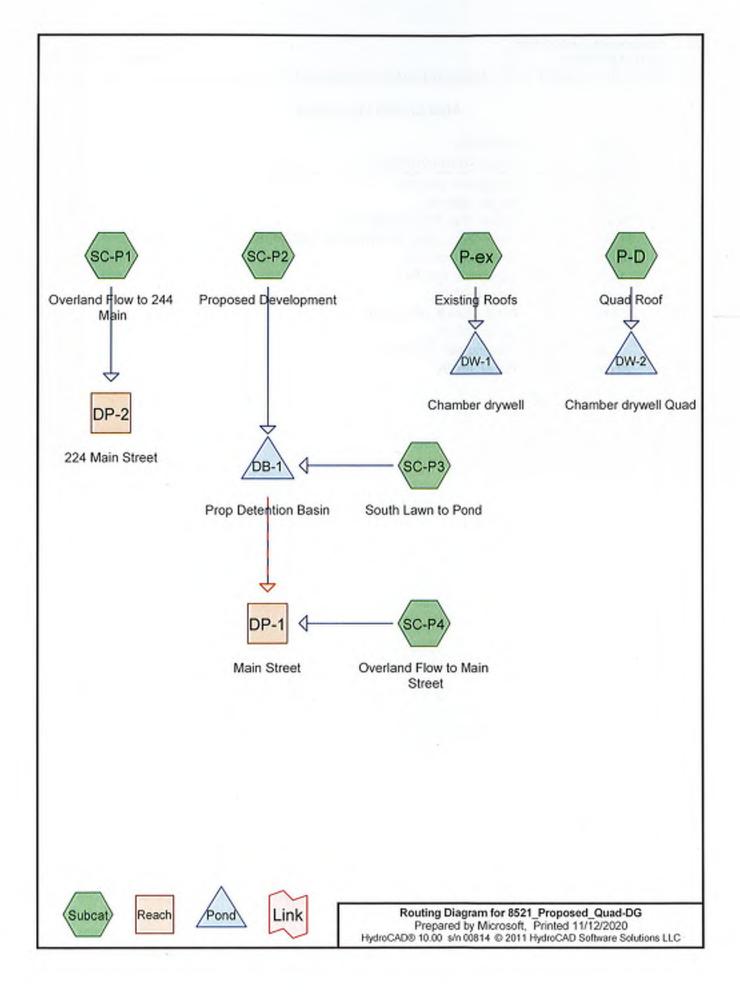
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Pond EP-2: Existing Depression







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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
10,692	60	Woodlands (SC-P2)
2,054	60	Woods (SC-P4)
24,311	60	Woods, Fair, HSG B (SC-P1) .
34,598	61	>75% Grass cover, Good, HSG B (SC-P1, SC-P2, SC-P3, SC-P4)
8,886	98	Driveways (SC-P2)
1,195	98	Impervious (SC-P4)
210	98	Patio (SC-P2)
9,065	98	Roofs, HSG B (P-D, P-ex)
979	98	patios (SC-P1)
61	98	retaining wall (SC-P2)
92,051	69	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
0	HSG A	
67,974	HSG B	P-D, P-ex, SC-P1, SC-P2, SC-P3, SC-P4
0	HSG C	
0	HSG D	
24,077	Other	SC-P1, SC-P2, SC-P4
92,051		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover
0	34,598	0	0	0	34,598	>75% Grass cover, Good
0	0	0	0	8,886	8,886	Driveways
0	0	0	0	1,195	1,195	Impervious
0	0	0	0	210	210	Patio
0	9,065	0	0	0	9,065	Roofs
0	0	0	0	10,692	10,692	Woodlands
0	0	0	0	2,054	2,054	Woods
0	24,311	0	0	0	24,311	Woods, Fair
0	0	0	0	979	979	patios
0	0	0	0	61	61	retaining wall
0	67,974	. 0	0	24,077	92,051	TOTAL AREA

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P-D: Quad Roof

Runoff Area=6,891 sf 100.00% Impervious Runoff Depth=3.14"

Tc=6.0 min CN=98 Runoff=0.51 cfs 1,801 cf

Subcatchment P-ex: Existing Roofs

Runoff Area=2,174 sf 100.00% Impervious Runoff Depth=3.14"

Tc=6.0 min CN=98 Runoff=0.16 cfs 568 cf

Subcatchment SC-P1: Overland Flow to 244 Runoff Area=32,145 sf 3.05% Impervious Runoff Depth=0.52"

Flow Length=310' Tc=12.4 min CN=61 Runoff=0.24 cfs 1,381 cf

Subcatchment SC-P2: Proposed

Runoff Area=32,876 sf 27.85% Impervious Runoff Depth=0.98"

Flow Length=280' Tc=10.7 min CN=71 Runoff=0.68 cfs 2,690 cf

Subcatchment SC-P3: South Lawn to Pond Runoff Area=9,610 sf 0.00% Impervious Runoff Depth=0.52"

Tc=6.0 min CN=61 Runoff=0.09 cfs 413 cf

Subcatchment SC-P4: Overland Flow to

Runoff Area=8,355 sf 14.30% Impervious Runoff Depth=0.73"

Flow Length=250' Tc=11.2 min CN=66 Runoff=0.11 cfs 509 cf

Reach DP-1: Main Street

Inflow=0.11 cfs 509 cf

Outflow=0.11 cfs 509 cf

Reach DP-2: 224 Main Street

Inflow=0.24 cfs 1,381 cf

Outflow=0.24 cfs 1,381 cf

Pond DB-1: Prop Detention Basin

Peak Elev=228.56' Storage=1,030 cf Inflow=0.76 cfs 3,103 cf

Discarded=0.11 cfs 3,103 cf Primary=0.00 cfs 0 cf Secondary=0.00 cfs 0 cf Outflow=0.11 cfs 3,103 cf

Pond DW-1: Chamber drywell

Peak Elev=229.82' Storage=162 cf Inflow=0.16 cfs 568 cf

Outflow=0.02 cfs 568 cf

Pond DW-2: Chamber drywell Quad

Peak Elev=235.31' Storage=463 cf Inflow=0.51 cfs 1,801 cf

Outflow=0.09 cfs 1,801 cf

Total Runoff Area = 92,051 sf Runoff Volume = 7,362 cf Average Runoff Depth = 0.96" 77.84% Pervious = 71,655 sf 22.16% Impervious = 20,396 sf

Summary for Subcatchment P-D: Quad Roof

Runoff

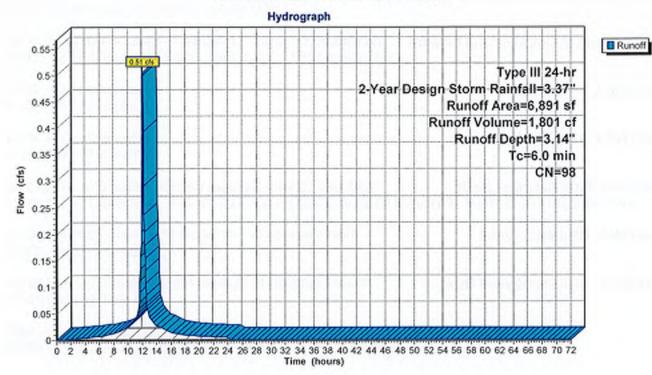
0.51 cfs @ 12.09 hrs, Volume=

1,801 cf, Depth= 3.14"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

A	rea (sf)	CN [Description		
	6,891	98 F	Roofs, HSG	B	
	6,891	1	100.00% Im	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0				9	Direct Entry, direct

Subcatchment P-D: Quad Roof



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Summary for Subcatchment P-ex: Existing Roofs

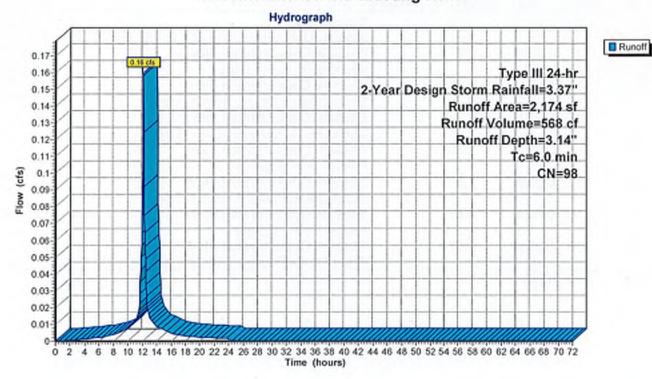
Runoff

0.16 cfs @ 12.09 hrs, Volume= 568 cf, Depth= 3.14"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

A	rea (sf)	CN I	Description		
	2,174	98 I	Roofs, HSC	BB	
	2,174		100.00% In	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, direct

Subcatchment P-ex: Existing Roofs



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Summary for Subcatchment SC-P1: Overland Flow to 244 Main

Runoff

=

0.24 cfs @ 12.23 hrs, Volume=

1,381 cf, Depth= 0.52"

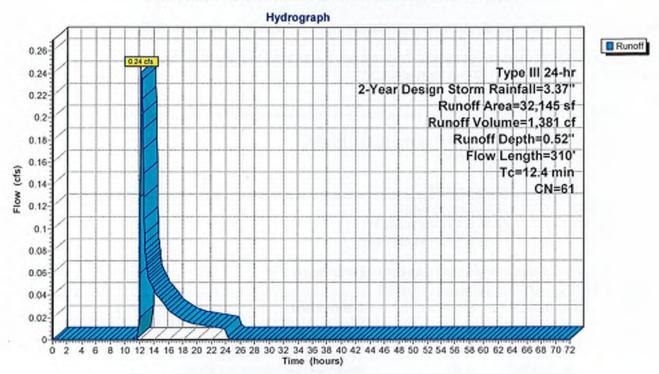
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

А	rea (sf)	CN E	Description		
*	6,855 24,311 979	60 V	≻75% Gras Voods, Fai oatios		ood, HSG B
	32,145 31,166 979	9		verage rvious Area ervious Are	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
8.6	50	0.0460			Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.37"
8.0	36	0.0200	0.71		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.7	50	0.0300	1.21		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
1.4	81	0.0200	0.99		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
0.1	15	0.0360	3.85		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.3	25	0.0360	1.33		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
0.1	15	0.0500	4.54		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.4	38	0.0500	1.57		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
12.4	310	Total	***************************************		

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Subcatchment SC-P1: Overland Flow to 244 Main



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Summary for Subcatchment SC-P2: Proposed Development

Runoff

0.68 cfs @ 12.17 hrs, Volume=

2,690 cf, Depth= 0.98"

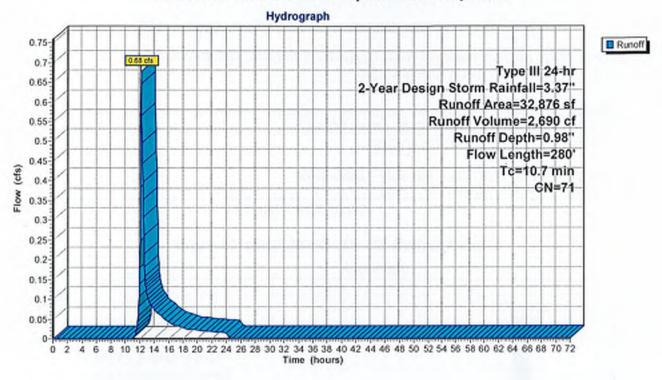
Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

	A	rea (sf)	CN D	Description						
*		8,886	98 [) Priveways	-					
		13,027	61 >	1 >75% Grass cover, Good, HSG B						
*		10,692	60 V	Woodlands						
*		210	98 F	Patio						
*		61	98 r							
		32,876	71 V	Veighted A	verage					
		23,719	7	'2.15% Per	vious Area					
		9,157	2	7.85% lmp	ervious Ar	e a				
	_		.			5				
	Tc	Length	Slope	Velocity		Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	8.2	50	0.0520	0.10		Sheet Flow,				
				4.46		Woods: Light underbrush n= 0.400 P2= 3.37"				
	8.0	50	0.0480	1.10		Shallow Concentrated Flow,				
		40	0 0000	4.00		Woodland Kv= 5.0 fps				
	0.1	13	0.0800	1.98		Shallow Concentrated Flow,				
	4.0	74	0.0000	4.04		Short Grass Pasture Kv= 7.0 fps				
	1.0	71	0.0300	1.21		Shallow Concentrated Flow,				
	0.4	40	0.4000	2.00		Short Grass Pasture Kv= 7.0 fps				
	0.1	19	0.1600	2.80		Shallow Concentrated Flow,				
	0.0	15	0.0400	1.40		Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,				
	0.2	15	0.0400	1.40		Short Grass Pasture Kv= 7.0 fps				
	0.3	62	0.0400	4.06		Shallow Concentrated Flow,				
	0.3	QZ	0.0400	4.00		Paved Kv= 20.3 fps				
_	40.7	200	Takal			1 a 2 Gu 1/4 - 20.0 1 pa				
	10.7	280	Total							

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Subcatchment SC-P2: Proposed Development



Summary for Subcatchment SC-P3: South Lawn to Pond

Runoff

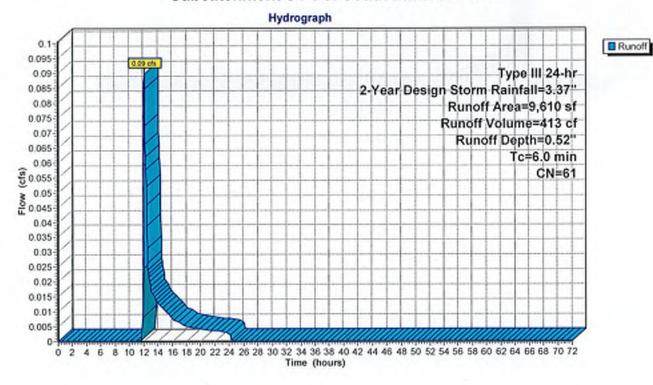
0.09 cfs @ 12.12 hrs, Volume=

413 cf, Depth= 0.52"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

A	rea (sf)	CN [Description			
	9,610	10 61 >75% Grass cover, Good, HSG B				
	9,610	1	100.00% Pe	ervious Are	ea	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
6.0					Direct Entry, Min Tc	

Subcatchment SC-P3: South Lawn to Pond



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Summary for Subcatchment SC-P4: Overland Flow to Main Street

Runoff

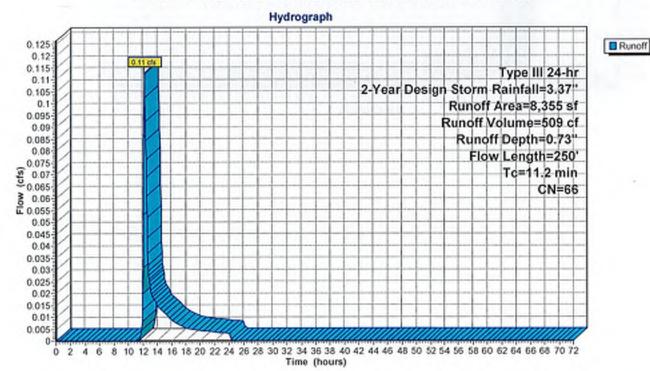
0.11 cfs @ 12.19 hrs, Volume=

509 cf, Depth= 0.73"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Design Storm Rainfall=3.37"

A	rea (sf)	CN E	escription							
	1,195	98 I	mpervious	npervious						
	5,106	61 >	75% Gras	s cover, Go	ood, HSG B					
	2,054	60 V	Voods		7.77					
	8,355	66 V	Veighted A	verage						
	7,160	8	5.70% Per	vious Area						
	1,195	1	4.30% Imp	ervious Ar	ea					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
8.3	50	0.0500	0.10		Sheet Flow,					
		3			Woods: Light underbrush n= 0.400 P2= 3.37"					
2.9	200	0.0530	1.15		Shallow Concentrated Flow, Woodland Kv= 5.0 fps					
11.2	250	Total								

Subcatchment SC-P4: Overland Flow to Main Street



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Summary for Reach DP-1: Main Street

Inflow Area =

50,841 sf, 20.36% Impervious, Inflow Depth = 0.12" for 2-Year Design Storm event

Inflow =

0.11 cfs @ 12.19 hrs, Volume=

509 cf

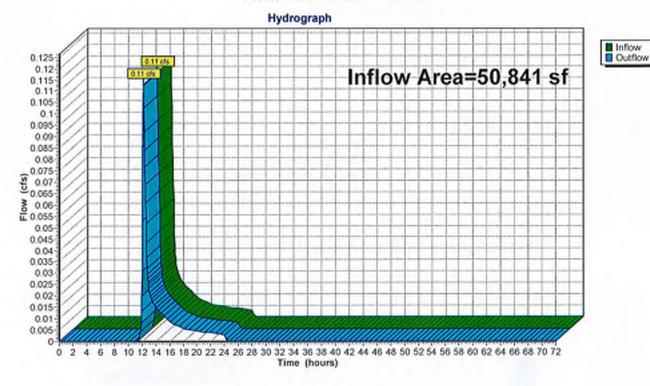
Outflow =

0.11 cfs @ 12.19 hrs, Volume=

509 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-1: Main Street



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Summary for Reach DP-2: 224 Main Street

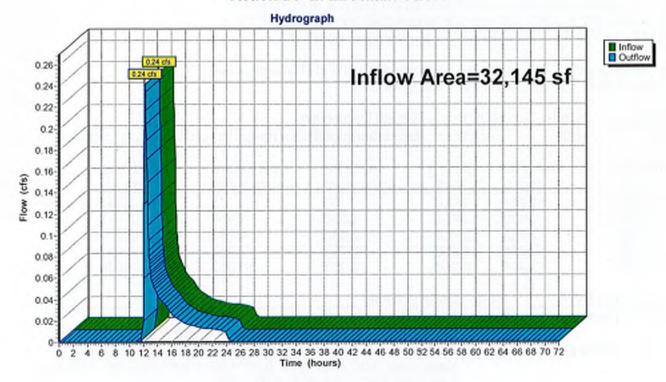
Inflow Area = 32,145 sf, 3.05% Impervious, Inflow Depth = 0.52" for 2-Year Design Storm event

Inflow = 0.24 cfs @ 12.23 hrs, Volume= 1,381 cf

Outflow = 0.24 cfs @ 12.23 hrs, Volume= 1,381 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-2: 224 Main Street



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Summary for Pond DB-1: Prop Detention Basin

Inflow Area = 42,486 sf. 21.55% Impervious, Inflow Depth = 0.88" for 2-Year Design Storm event 0.76 cfs @ 12.16 hrs, Volume= 3,103 cf Inflow = Outflow = 0.11 cfs @ 13.24 hrs, Volume= 3,103 cf, Atten= 86%, Lag= 64.7 min 0.11 cfs @ 13.24 hrs, Volume= Discarded = 3,103 cf 0.00 cfs @ 0.00 hrs, Volume= 0 cf Primary = 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 228.56' @ 13.24 hrs Surf.Area= 1,957 sf Storage= 1,030 cf Flood Elev= 232.00' Surf.Area= 3,494 sf Storage= 10,313 cf

Plug-Flow detention time= 90.3 min calculated for 3,101 cf (100% of inflow) Center-of-Mass det. time= 90.2 min (967.9 - 877.6)

Volume	Invert	Avail.St	orage	Storage Description	າ					
#1	#1 228.00' 10,313 cf		Main Infiltration Ba	Main Infiltration Basin (Irregular) Listed below (Recalc)						
Elevatio		rf.Area ((sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)				
228.0	00	1,744	183.8	0	0	1,744				
229.0	00	2,135	201.4	1,936	1,936	2,317				
230.0	00	2,558	218.0	2,343	4,280	2,909				
231.0	00	3,014	233.8	2,783	7,062	3,521				
232.0	00	3,494 246		3,251 10,3		4,059				
Device	Routing	Invert	Outle	et Devices						
#1	Discarded	228.00	2.41	110 in/hr Exfiitration over Surface area						
			Con	ductivity to Groundw	ater Elevation = 0.0	00'				
#2	Primary	231.00		l' long ix 8.0' breadth Broad-Crested Rectangular Weir						
				Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00						
				3.00 3.50 4.00 4.						
						2.68 2.66 2.64 2.64				
				2.65 2.65 2.66 2.	·					
#3	Secondary	231.20	24.0	" x 48.0" Horiz. Orifi	ice/Grate C= 0.66	00				
			Limi	ted to weir flow at lov	w heads					

Discarded OutFlow Max=0.11 cfs @ 13.24 hrs HW=228.56' (Free Discharge) 1=Exfiltration (Controls 0.11 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.00' (Free Discharge) —2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

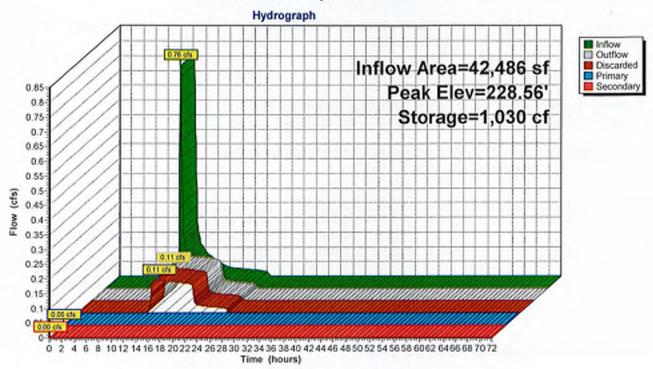
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.00' (Free Discharge) =3=Orifice/Grate (Controls 0.00 cfs)

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Pond DB-1: Prop Detention Basin



8521 Proposed Quad-DG

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Summary for Pond DW-1: Chamber drywell

2,174 sf,100.00% Impervious, Inflow Depth = 3.14" for 2-Year Design Storm event Inflow Area =

Inflow = 0.16 cfs @ 12.09 hrs, Volume= 568 cf

0.02 cfs @ 11.70 hrs, Volume= Outflow = 568 cf, Atten= 85%, Lag= 0.0 min

0.02 cfs @ 11.70 hrs, Volume= Discarded = 568 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 229.82' @ 12.58 hrs Surf.Area= 430 sf Storage= 162 cf

Plug-Flow detention time= 40.4 min calculated for 568 cf (100% of inflow)

Center-of-Mass det. time= 40.4 min (795.7 - 755.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	229.10'	391 cf	11.17'W x 38.50'L x 3.54'H Field A
			1,523 cf Overall - 544 cf Embedded = 979 cf x 40.0% Voids
#2A	229.60	544 cf	Cultec R-330XL x 10 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		935 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	229.10'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.02 cfs @ 11.70 hrs HW=229.14' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.02 cfs)

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Pond DW-1: Chamber drywell - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length

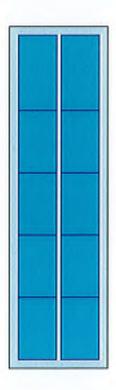
2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

10 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 543.9 cf Chamber Storage

1,522.6 cf Field - 543.9 cf Chambers = 978.7 cf Stone x 40.0% Voids = 391.5 cf Stone Storage

Stone + Chamber Storage = 935.4 cf = 0.021 af Overall Storage Efficiency = 61.4%

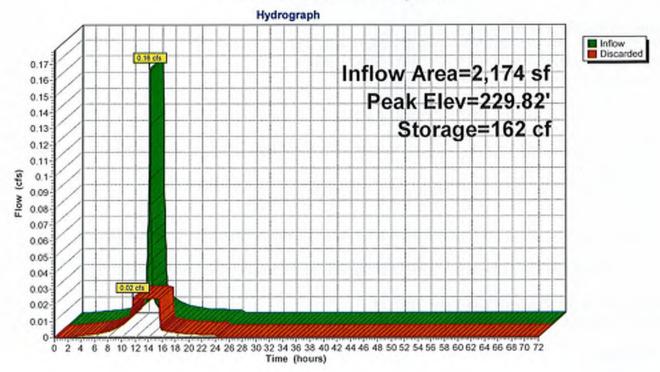
10 Chambers 56.4 cy Field 36.2 cy Stone





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Pond DW-1: Chamber drywell



8521_Proposed_Quad-DG

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Summary for Pond DW-2: Chamber drywell Quad

Inflow Area = 6,891 sf,100.00% Impervious, Inflow Depth = 3.14" for 2-Year Design Storm event

Inflow = 0.51 cfs @ 12.09 hrs, Volume= 1,801 cf

Outflow = 0.09 cfs @ 11.70 hrs, Volume= 1,801 cf, Atten= 82%, Lag= 0.0 min

Discarded = 0.09 cfs @ 11.70 hrs, Volume= 1,801 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 235.31' @ 12.54 hrs Surf.Area= 1,600 sf Storage= 463 cf

Plug-Flow detention time= 28.6 min calculated for 1,800 cf (100% of inflow)

Center-of-Mass det. time= 28.6 min (783.9 - 755.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	234.70	995 cf	40.00'W x 40.00'L x 2.04'H Field A
			3,267 cf Overall - 778 cf Embedded = 2,489 cf x 40.0% Voids
#2A	235.20'	778 cf	- m.,
			Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf
			Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap
			Row Length Adjustment= +0.50' x 1.86 sf x 11 rows

1,774 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	234.70'	2.410 in/hr Exfiltration over Surface area	

Discarded OutFlow Max=0.09 cfs @ 11.70 hrs HW=234.72' (Free Discharge)
1=Exfiltration (Exfiltration Controls 0.09 cfs)

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Pond DW-2: Chamber drywell Quad - Chamber Wizard Field A

Chamber Model = Cultec C-100

Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap Row Length Adjustment= +0.50' x 1.86 sf x 11 rows

36.0" Wide + 6.0" Spacing = 42.0" C-C Row Spacing

5 Chambers/Row x 7.50' Long +0.50' Row Adjustment = 38.00' Row Length +12.0" End Stone x 2 = 40.00' Base Length

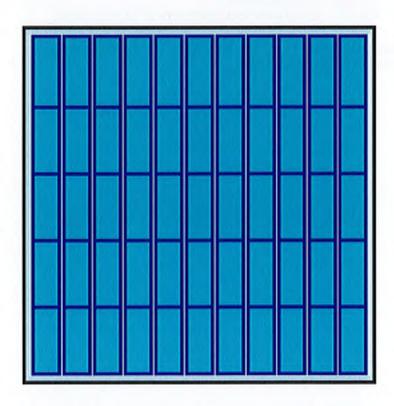
11 Rows x 36.0" Wide + 6.0" Spacing x 10 + 12.0" Side Stone x 2 = 40.00' Base Width 6.0" Base + 12.5" Chamber Height + 6.0" Cover = 2.04' Field Height

55 Chambers x 14.0 cf +0.50' Row Adjustment x 1.86 sf x 11 Rows = 778.1 cf Chamber Storage

3,266.7 cf Field - 778.1 cf Chambers = 2,488.6 cf Stone x 40.0% Voids = 995.4 cf Stone Storage

Stone + Chamber Storage = 1,773.5 cf = 0.041 af Overall Storage Efficiency = 54.3%

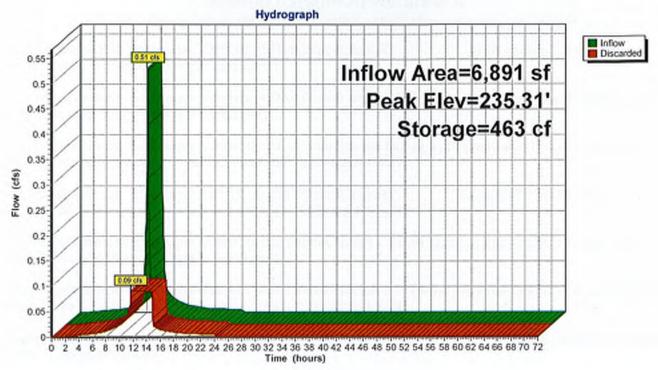
55 Chambers 121.0 cy Field 92.2 cy Stone





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Pond DW-2: Chamber drywell Quad



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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P-D: Quad Roof

Runoff Area=6,891 sf 100.00% Impervious Runoff Depth=5.02"

Tc=6.0 min CN=98 Runoff=0.80 cfs 2,884 cf

Subcatchment P-ex: Existing Roofs

Runoff Area=2,174 sf 100.00% Impervious Runoff Depth=5.02"

Tc=6.0 min CN=98 Runoff=0.25 cfs 910 cf

Subcatchment SC-P1: Overland Flow to 244 Runoff Area=32,145 sf 3.05% Impervious Runoff Depth=1.53"

Flow Length=310' Tc=12.4 min CN=61 Runoff=0.97 cfs 4,093 cf

Subcatchment SC-P2: Proposed

Runoff Area=32,876 sf 27.85% Impervious Runoff Depth=2.31"

Flow Length=280' Tc=10.7 min CN=71 Runoff=1.72 cfs 6,342 cf

Subcatchment SC-P3: South Lawn to Pond Runoff Area=9,610 sf 0.00% Impervious Runoff Depth=1.53"

Tc=6.0 min CN=61 Runoff=0.36 cfs 1,224 cf

Subcatchment SC-P4: Overland Flow to

Runoff Area=8,355 sf 14,30% Impervious Runoff Depth=1.91"

Flow Length=250' Tc=11.2 min CN=66 Runoff=0.35 cfs 1,328 cf

Reach DP-1: Main Street

Inflow=0.35 cfs 1,328 cf

Outflow=0.35 cfs 1,328 cf

Reach DP-2: 224 Main Street

Inflow=0.97 cfs 4,093 cf

Outflow=0.97 cfs 4,093 cf

Pond DB-1: Prop Detention Basin

Peak Elev=229.79' Storage=3.746 cf Inflow=2.02 cfs 7,566 cf

Discarded=0.14 cfs 7,566 cf Primary=0.00 cfs 0 cf Secondary=0.00 cfs 0 cf Outflow=0.14 cfs 7,566 cf

Pond DW-1: Chamber drywell

Peak Elev=230.25' Storage=310 cf Inflow=0.25 cfs 910 cf

Outflow=0.02 cfs 910 cf

Pond DW-2: Chamber drywell Quad

Peak Elev=235.67' Storage=908 cf Inflow=0.80 cfs 2,884 cf

Outflow=0.09 cfs 2,884 cf

Total Runoff Area = 92,051 sf Runoff Volume = 16,781 cf Average Runoff Depth = 2.19" 77.84% Pervious = 71.655 sf 22.16% Impervious = 20,396 sf

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Summary for Subcatchment P-D: Quad Roof

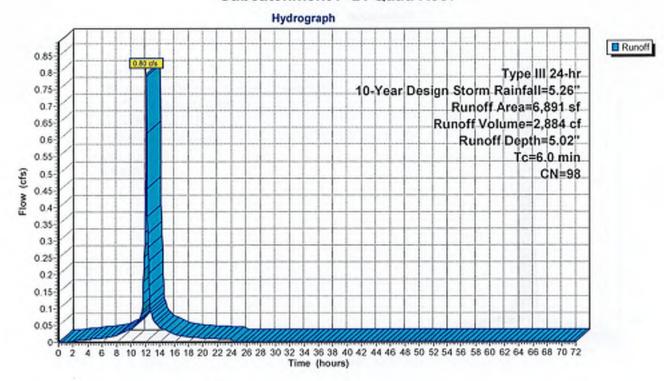
Runoff

0.80 cfs @ 12.09 hrs, Volume= 2,884 cf, Depth= 5.02"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

A	rea (sf)	CN I	Description			
	6,891	98 I	Roofs, HSG	B B		
	6,891		100.00% In	pervious A	rea	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
6.0					Direct Entry, direct	

Subcatchment P-D: Quad Roof



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Summary for Subcatchment P-ex: Existing Roofs

Runoff

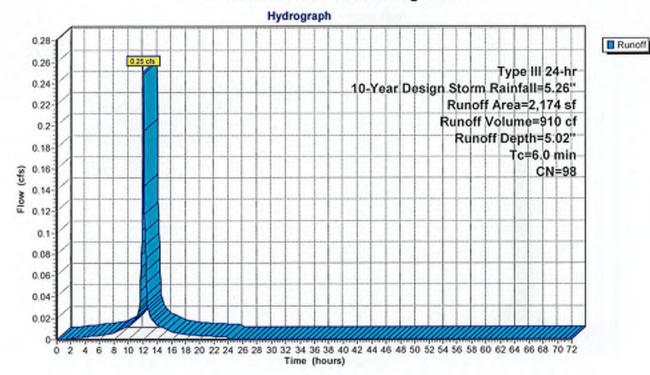
0.25 cfs @ 12.09 hrs, Volume=

910 cf, Depth= 5.02"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

A	rea (sf)	CN I	Description		
	2,174	98	Roofs, HSG	B	
	2,174		100.00% Im	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
6.0					Direct Entry, direct

Subcatchment P-ex: Existing Roofs



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Summary for Subcatchment SC-P1: Overland Flow to 244 Main

Runoff

0.97 cfs @ 12.19 hrs, Volume=

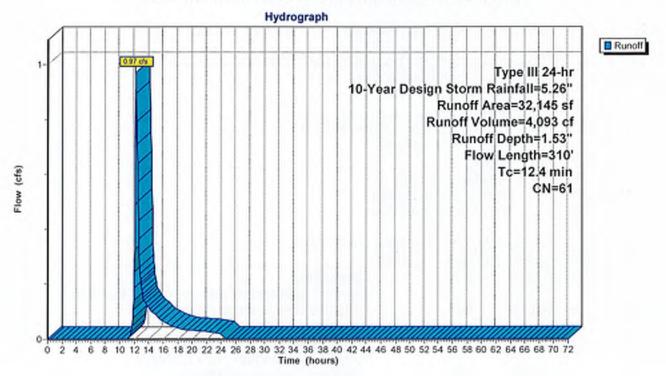
4,093 cf, Depth= 1.53"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

	Α	rea (sf)	CN E	escription							
		6,855 24,311		· · · · · · · · · · · · · · · · · · ·							
*	979 98 patios										
		32,145 31,166 979	9		verage vious Area ervious Are						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
_	8.6	50	0.0460	0.10		Sheet Flow,					
				~ ***		Woods: Light underbrush n= 0.400 P2= 3.37"					
	8.0	36	0.0200	0.71		Shallow Concentrated Flow, Woodland Kv= 5.0 fps					
	0.7	50	0.0300	1.21		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					
	1.4	81	0.0200	0.99		Shallow Concentrated Flow,					
	0.1	15	0.0360	3.85		Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,					
	0.3	25	0.0360	1.33		Paved Kv= 20.3 fps Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					
	0.1	15	0.0500	4.54		Shallow Concentrated Flow, Paved Kv= 20.3 fps					
	0.4	38	0.0500	1.57		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					
_	12.4	310	Total								

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Subcatchment SC-P1: Overland Flow to 244 Main



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Summary for Subcatchment SC-P2: Proposed Development

Runoff

1.72 cfs @ 12.16 hrs, Volume=

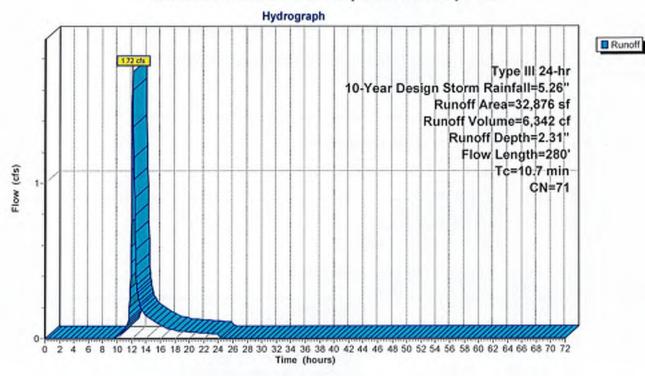
6,342 cf, Depth= 2.31"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

	Α	rea (sf)	CN E	Description								
*		8,886	98 E	,								
		13,027	61 >	75% Grass cover, Good, HSG B								
*		10,692	60 V	Voodlands								
*		210	98 F	atio								
*		61	98 r	etaining wa	all							
		32,876	71 V	Veighted A	verage							
		23,719			vious Area							
		9,157	2	7.85% lmp	ervious Ar	ea						
	Тс	•	Slope	•	Capacity	Description						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	8.2	50	0.0520	0.10		Sheet Flow,						
						Woods: Light underbrush n= 0.400 P2= 3.37"						
	8.0	50	0.0480	1.10		Shallow Concentrated Flow,						
						Woodland Kv= 5.0 fps						
	0.1	13	0.0800	1.98		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						
	1.0	71	0.0300	1.21		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						
	0.1	19	0.1600	2.80		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						
	0.2	15	0.0400	1.40		Shallow Concentrated Flow,						
						Short Grass Pasture Kv= 7.0 fps						
	0.3	62	0.0400	4.06		Shallow Concentrated Flow,						
_						Paved Kv= 20.3 fps						
_	10.7	280	Total									

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Subcatchment SC-P2: Proposed Development



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Summary for Subcatchment SC-P3: South Lawn to Pond

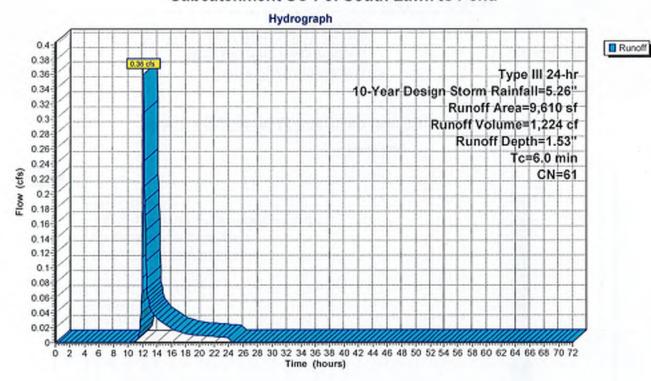
Runoff

0.36 cfs @ 12.10 hrs, Volume= 1,224 cf, Depth= 1.53"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

A	rea (sf)	CN	Description					
	9,610	61	>75% Grass cover, Good, HSG B					
	9,610		100.00% Pe	ervious Are	a		1.50	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	2.	-	
6.0					Direct Entry,	Min Tc		

Subcatchment SC-P3: South Lawn to Pond



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Summary for Subcatchment SC-P4: Overland Flow to Main Street

Runoff =

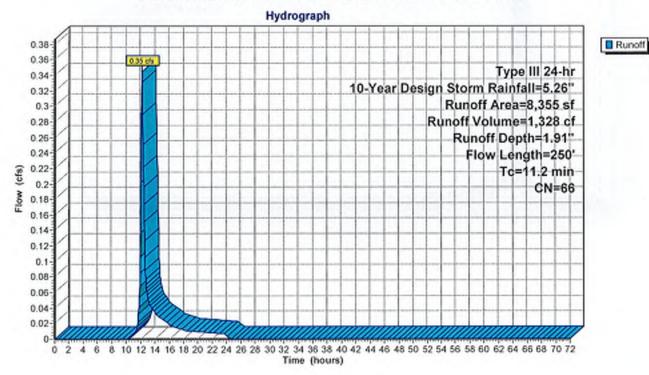
0.35 cfs @ 12.17 hrs, Volume=

1,328 cf, Depth= 1.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Design Storm Rainfall=5.26"

A	rea (sf)	CN I	Description		4				
	1,195	98 1	mpervious						
	5,106	61 >	75% Gras	s cover, Go	ood, HSG B				
	2,054		Voods						
	8,355	66 V	Neighted A	verage					
	7,160		85.70% Pervious Area						
	1,195		14.30% Impervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
8.3	50	0.0500	0.10	, , ,	Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.37"				
2.9	200	0.0530	1.15		Shallow Concentrated Flow, Woodland Kv= 5.0 fps				
11.2	250	Total							

Subcatchment SC-P4: Overland Flow to Main Street



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Summary for Reach DP-1: Main Street

Inflow Area =

50,841 sf, 20.36% Impervious, Inflow Depth = 0.31" for 10-Year Design Storm event

Inflow

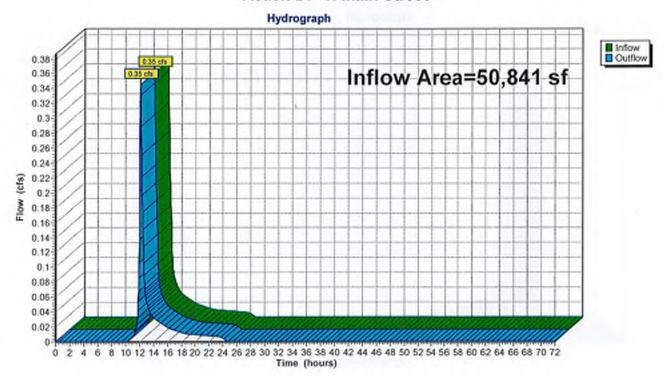
0.35 cfs @ 12.17 hrs, Volume= 1,328 cf

Outflow

0.35 cfs @ 12.17 hrs, Volume= 1,328 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-1: Main Street



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Summary for Reach DP-2: 224 Main Street

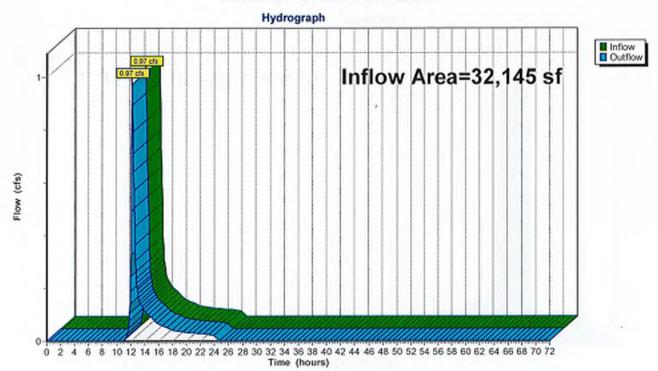
Inflow Area = 32,145 sf, 3.05% Impervious, Inflow Depth = 1.53" for 10-Year Design Storm event

Inflow = 0.97 cfs @ 12.19 hrs, Volume= 4,093 cf

Outflow = 0.97 cfs @ 12.19 hrs, Volume= 4,093 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-2: 224 Main Street



Invert

3.014

3,494

Volume

231.00

232.00

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Summary for Pond DB-1: Prop Detention Basin

Inflow Area =	42,486 sf, 21.55% Impervious,	Inflow Depth = 2.14" for 10-Year Design Storm event
Inflow =	2.02 cfs @ 12.15 hrs, Volume=	7,566 cf
Outflow =	0.14 cfs @ 15.01 hrs, Volume=	7,566 cf, Atten= 93%, Lag= 171.6 min
Discarded =	0.14 cfs @ 15.01 hrs, Volume=	7,566 cf
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	O cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 229.79' @ 15.01 hrs Surf.Area= 2,465 sf Storage= 3,746 cf Flood Elev= 232.00' Surf.Area= 3,494 sf Storage= 10,313 cf

Plug-Flow detention time= 304.6 min calculated for 7,566 cf (100% of inflow) Center-of-Mass det. time= 304.5 min (1,154.9 - 850.4)

233.8

246.4

Avail.Storage Storage Description

#1	228.00'	10,313 cf	Main Infiltration Ba	asin (Irregular) List	ted below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
228.00	1,744	183.8	0	0	1,744
229.00	2,135	201.4	1,936	1,936	2,317
230.00	2,558	218.0	2,343	4,280	2,909

Device	Routing	Invert	Outlet Devices
#1	Discarded	228.00'	2.410 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 0.00'
#2	Primary	231.00	8.0' long x 8.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.43 2.54 2.70 2.69 2.68 2.68 2.66 2.64 2.64
			2.64 2.65 2.65 2.66 2.66 2.68 2.70 2.74
#3	Secondary	231.20'	24.0" x 48.0" Horiz. Orifice/Grate

Limited to weir flow at low heads

2,783

3,251

7,062

10,313

3,521

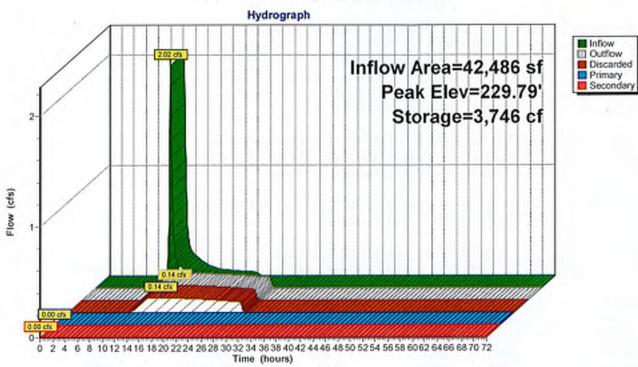
4,059

Discarded OutFlow Max=0.14 cfs @ 15.01 hrs HW=229.79' (Free Discharge) 1=Exfiltration (Controls 0.14 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond DB-1: Prop Detention Basin



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Summary for Pond DW-1: Chamber drywell

Inflow Area = 2,174 sf,100.00% Impervious, Inflow Depth = 5.02" for 10-Year Design Storm event

Inflow = 0.25 cfs @ 12.09 hrs, Volume= 910 cf

Outflow = 0.02 cfs @ 11.40 hrs, Volume= 910 cf, Atten= 90%, Lag= 0.0 min

Discarded = 0.02 cfs @ 11.40 hrs, Volume= 910 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 230.25' @ 12.90 hrs Surf.Area= 430 sf Storage= 310 cf

Plug-Flow detention time= 88.2 min calculated for 909 cf (100% of inflow) Center-of-Mass det. time= 88.1 min (835.3 - 747.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	229.10'	391 cf	11.17'W x 38.50'L x 3.54'H Field A
			1,523 cf Overall - 544 cf Embedded = 979 cf x 40.0% Voids
#2A	229.601	544 cf	Cultec R-330XL x 10 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		935 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	229.10	2.410 in/hr Exfiltration over Surface area	

Discarded OutFlow Max=0.02 cfs @ 11.40 hrs HW=229.14' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.02 cfs)

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Pond DW-1: Chamber drywell - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length

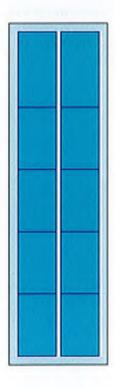
2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

10 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 543.9 cf Chamber Storage

1,522.6 cf Field - 543.9 cf Chambers = 978.7 cf Stone x 40.0% Voids = 391.5 cf Stone Storage

Stone + Chamber Storage = 935.4 cf = 0.021 af Overall Storage Efficiency = 61.4%

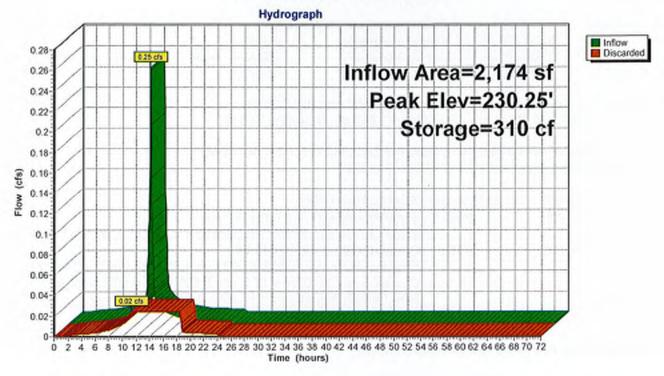
10 Chambers 56.4 cy Field 36.2 cy Stone





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Pond DW-1: Chamber drywell



8521 Proposed Quad-DG

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Summary for Pond DW-2: Chamber drywell Quad

6,891 sf,100.00% Impervious, Inflow Depth = 5.02" for 10-Year Design Storm event Inflow Area =

Inflow = 0.80 cfs @ 12.09 hrs, Volume= 2,884 cf

0.09 cfs @ 11.55 hrs, Volume= 2,884 cf, Atten= 89%, Lag= 0.0 min Outflow =

0.09 cfs @ 11.55 hrs, Volume= 2,884 cf Discarded =

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 235.67' @ 12.73 hrs Surf. Area= 1,600 sf Storage= 908 cf

Plug-Flow detention time= 64.9 min calculated for 2,882 cf (100% of inflow) Center-of-Mass det. time= 64.8 min (812.0 - 747.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	234.70'	995 cf	40.00'W x 40.00'L x 2.04'H Field A
			3,267 cf Overall - 778 cf Embedded = 2,489 cf x 40.0% Voids
#2A	235.20'	778 cf	Cultec C-100 x 55 Inside #1
			Eftective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf
			Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap
			Row Length Adjustment= +0.50' x 1.86 sf x 11 rows
		1 774 of	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	234.70'	2.410 in/hr Exfiltration over Surface area	

Discarded OutFlow Max=0.09 cfs @ 11.55 hrs HW=234.72' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.09 cfs)

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Pond DW-2: Chamber drywell Quad - Chamber Wizard Field A

Chamber Model = Cultec C-100

Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap Row Length Adjustment= +0.50' x 1.86 sf x 11 rows

36.0" Wide + 6.0" Spacing = 42.0" C-C Row Spacing

5 Chambers/Row x 7.50' Long +0.50' Row Adjustment = 38.00' Row Length +12.0" End Stone x 2 = 40.00' Base Length

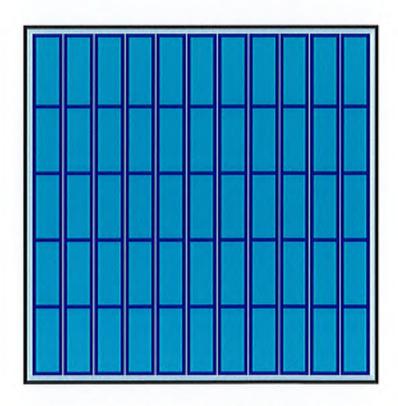
11 Rows x 36.0" Wide + 6.0" Spacing x 10 + 12.0" Side Stone x 2 = 40.00' Base Width 6.0" Base + 12.5" Chamber Height + 6.0" Cover = 2.04' Field Height

55 Chambers x 14.0 cf +0.50' Row Adjustment x 1.86 sf x 11 Rows = 778.1 cf Chamber Storage

3,266.7 cf Field - 778.1 cf Chambers = 2,488.6 cf Stone x 40.0% Voids = 995.4 cf Stone Storage

Stone + Chamber Storage = 1,773.5 cf = 0.041 af Overall Storage Efficiency = 54.3%

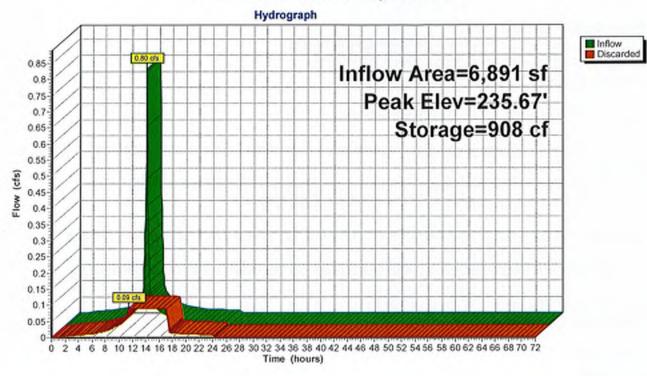
55 Chambers 121.0 cy Field 92.2 cy Stone





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Pond DW-2: Chamber drywell Quad



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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P-D: Quad Roof

Runoff Area=6,891 sf 100.00% Impervious Runoff Depth=8.02"

Tc=6.0 min CN=98 Runoff=1.25 cfs 4,606 cf

Subcatchment P-ex: Existing Roofs

Runoff Area=2,174 sf 100.00% Impervious Runoff Depth=8.02"

Tc=6.0 min CN=98 Runoff=0.40 cfs 1,453 cf

Subcatchment SC-P1: Dverland Flow to 244 Runoff Area=32,145 sf 3.05% Impervious Runoff Depth=3.64"

Flow Length=310' Tc=12.4 min CN=61 Runoff=2.50 cfs 9,762 cf

Subcatchment SC-P2: Proposed

Runoff Area=32,876 sf 27.85% Impervious Runoff Depth=4.81"

Flow Length=280' Tc=10.7 min CN=71 Runoff=3.60 cfs 13,166 cf

Subcatchment SC-P3: South Lawn to Pond Runoff Area=9,610 sf 0.00% Impervious Runoff Depth=3.64"

Tc=6.0 min CN=61 Runoff=0.92 cfs 2,918 cf

Subcatchment SC-P4: Dverland Flow to

Runoff Area=8,355 sf 14.30% Impervious Runoff Depth=4.22"

Flow Length=250' Tc=11.2 min CN=66 Runoff=0.79 cfs 2,939 cf

Reach DP-1: Main Street

Inflow=0.88 cfs 5,709 cf

Outflow=0.88 cfs 5,709 cf

Reach DP-2: 224 Main Street

Inflow=2.50 cfs 9,762 cf

Outflow=2.50 cfs 9,762 cf

Pond DB-1: Prop Detention Basin

Peak Elev=231.11' Storage=7,394 cf Inflow=4.37 cfs 16,085 cf

Discarded=0.17 cfs 13,314 cf Primary=0.71 cfs 2,770 cf Secondary=0.00 cfs 0 cf Outflow=0.88 cfs 16,084 cf

Pond DW-1: Chamber drywell

Peak Elev=231.13' Storage=593 cf Inflow=0.40 cfs 1,453 cf

Outflow=0.02 cfs 1,453 cf

Pond DW-2: Chamber drywell Quad

Peak Elev=236.69' Storage=1,739 cf Inflow=1.25 cfs 4,606 cf

Outflow=0.09 cfs 4,606 cf

Total Runoff Area = 92,051 sf Runoff Volume = 34,844 cf Average Runoff Depth = 4.54" 77.84% Pervious = 71,655 sf 22.16% Impervious = 20,396 sf

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Summary for Subcatchment P-D: Quad Roof

Runoff

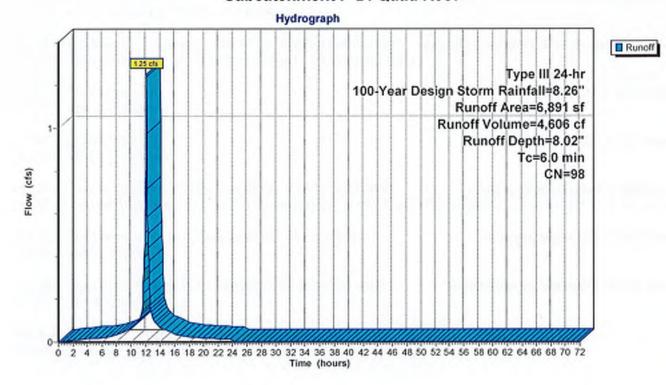
1.25 cfs @ 12.09 hrs, Volume=

4,606 cf, Depth= 8.02"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

A	rea (sf)	CN I	Description		
	6,891	98	Roofs, HSG	B	
	6,891		100.00% In	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, direct

Subcatchment P-D: Quad Roof



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Summary for Subcatchment P-ex: Existing Roofs

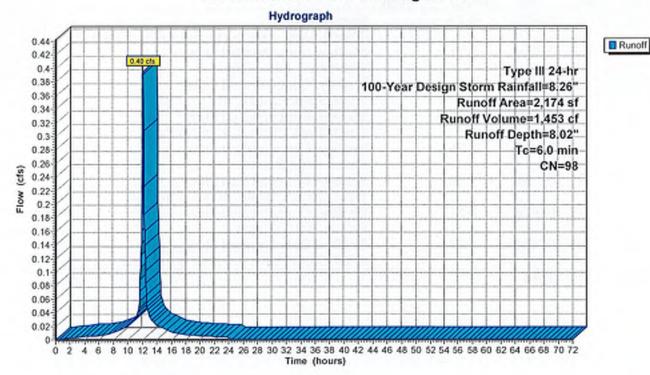
Runoff

0.40 cfs @ 12.09 hrs, Volume= 1,453 cf, Depth= 8.02"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

A	rea (sf)	CN	Description		I o	
	2,174	98	Roofs, HSG B			
	2,174		100.00% Im	pervious A	Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description	
6.0					Direct Entry, direct	

Subcatchment P-ex: Existing Roofs



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Summary for Subcatchment SC-P1: Overland Flow to 244 Main

Runoff

=

2.50 cfs @ 12.18 hrs, Volume=

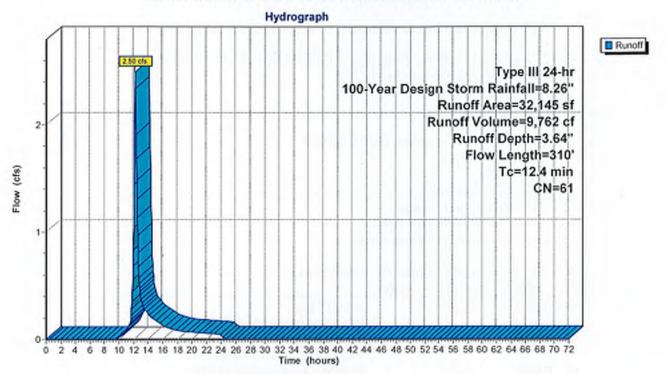
9,762 cf, Depth= 3.64"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

 Α	rea (sf)	CN D	escription	·····	
	6,855				ood, HSG B
	24,311		Voods, Fai	r, HSG B	
 	979		atios		
	32,145		Veighted A		
	31,166			vious Area	
	979	3	.05% Impe	ervious Area	a
Tc	Length	Slope	Velocity	Capacity	Description
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
 8.6	50	0.0460	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.37"
8.0	36	0.0200	0.71		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.7	50	0.0300	1.21		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.4	81	0.0200	0.99		Shallow Concentrated Flow,
	•				Short Grass Pasture Kv= 7.0 fps
0.1	15	0.0360	3.85		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.3	25	0.0360	1.33		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.1	15	0.0500	4.54		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.4	38	0.0500	1.57		Shallow Concentrated Flow,
 					Short Grass Pasture Kv= 7.0 fps
12.4	310	Total			

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Subcatchment SC-P1: Overland Flow to 244 Main



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Summary for Subcatchment SC-P2: Proposed Development

Runoff

3.60 cfs @ 12.15 hrs, Volume=

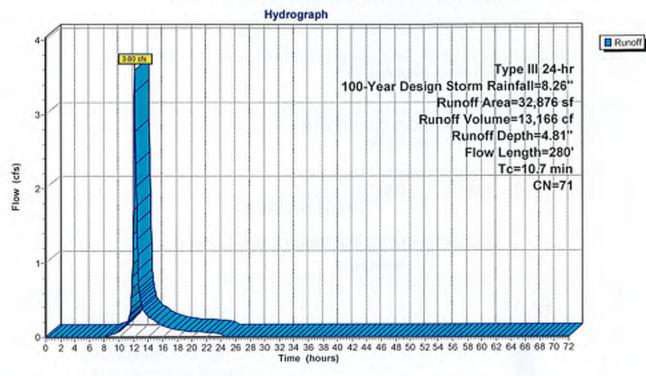
13,166 cf, Depth= 4.81"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

		/aÐ	ON 5)						
	A	rea (sf)	***************************************	Description						
*		8,886)riveways	_					
		13,027				ood, HSG B				
*		10,692		Woodlands						
*		210								
*		61_	98 r	etaining wa	all					
		32,876	71 V	Veighted A	verage					
		23,719	7	2.15% Per	vious Area	l				
		9,157	2	7.85% Imp	pervious Ar	ea				
				,						
	Tc	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	8.2	50	0.0520	0.10		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.37"				
	0.8	50	0.0480	1.10		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	0.1	13	0.0800	1.98		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	1.0	71	0.0300	1.21		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.1	19	0.1600	2.80		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.2	15	0.0400	1,40		Shallow Concentrated Flow,				
				•••		Short Grass Pasture Kv= 7.0 fps				
	0.3	62	0.0400	4.06		Shallow Concentrated Flow,				
		- 				Paved Kv= 20.3 fps				
•	10.7	280	Total							

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Subcatchment SC-P2: Proposed Development



Summary for Subcatchment SC-P3: South Lawn to Pond

Runoff

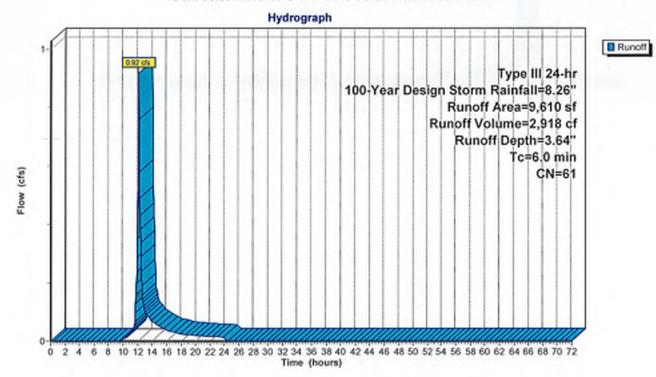
0.92 cfs @ 12.10 hrs, Volume=

2,918 cf, Depth= 3.64"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

Α	rea (sf)	CN I	Description		
	9,610	61 :	75% Gras	s cover, Go	ood, HSG B
	9,610		100.00% P	ervious Are	ea
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, Min To

Subcatchment SC-P3: South Lawn to Pond



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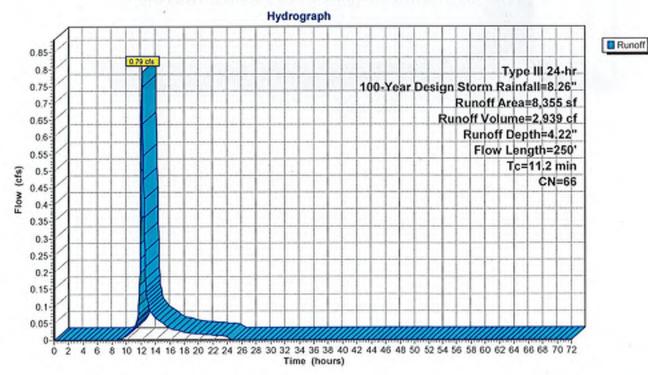
Summary for Subcatchment SC-P4: Overland Flow to Main Street

0.79 cfs @ 12.16 hrs, Volume= 2,939 cf, Depth= 4.22" Runoff

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Design Storm Rainfall=8.26"

A	rea (sf)	CN	Description			
*	1,195	98	Impervious		C. C. C. C. C.	
	5,106	61	>75% Gras	s cover, Go	ood, HSG B	
*	2,054	60	Woods			
	8,355	66	Weighted A	verage		
	7,160		85.70% Per			
	1,195		14.30% Imp	pervious Ar	ea	
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description	
8.3	50	0.050	0.10		Sheet Flow, Woods: Light underbrush n= 0.400	P2= 3.37"
2.9	200	0.053	1.15		Shallow Concentrated Flow, Woodland Kv= 5.0 fps	
11.2	250	Total				

Subcatchment SC-P4: Overland Flow to Main Street



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Summary for Reach DP-1: Main Street

Inflow Area =

50,841 sf, 20.36% Impervious, Inflow Depth = 1.35" for 100-Year Design Storm event

Inflow =

0.88 cfs @ 12.65 hrs, Volume=

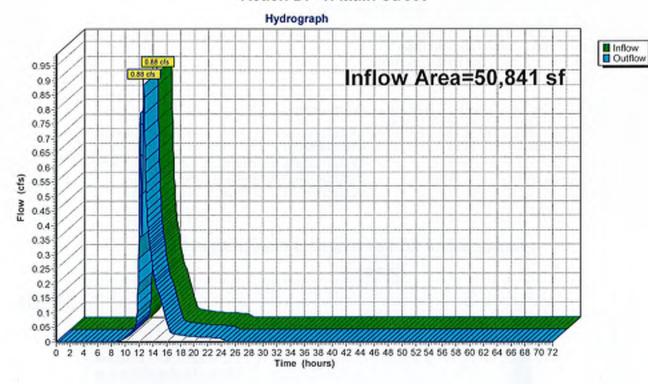
5,709 cf

Outflow

0.88 cfs @ 12.65 hrs, Volume= 5,709 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-1: Main Street



8521 Proposed Quad-DG

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Summary for Reach DP-2: 224 Main Street

Inflow Area =

32,145 sf, 3.05% Impervious, Inflow Depth = 3.64" for 100-Year Design Storm event

Inflow

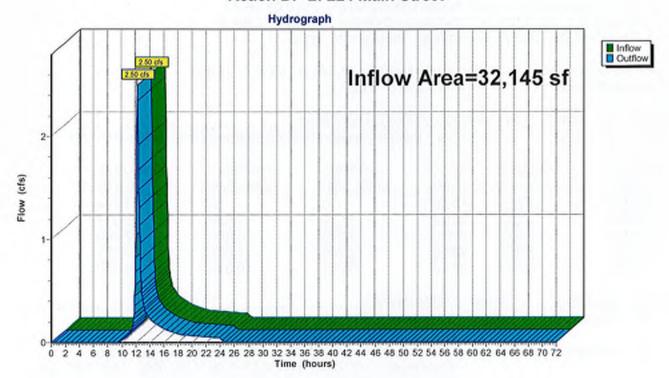
2.50 cfs @ 12.18 hrs, Volume= 9,762 cf

Outflow

2.50 cfs @ 12.18 hrs, Volume= 9,762 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach DP-2: 224 Main Street



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Summary for Pond DB-1: Prop Detention Basin

42,486 sf, 21.55% Impervious, Inflow Depth = 4.54" for 100-Year Design Storm event Inflow Area = 4.37 cfs @ 12.14 hrs, Volume= Inflow = 16.085 cf Outflow = 0.88 cfs @ 12.66 hrs, Volume= 16,084 cf, Atten= 80%, Lag= 31.5 min 0.17 cfs @ 12.66 hrs, Volume= Discarded = 13,314 cf 0.71 cfs @ 12.66 hrs, Volume= 2,770 cf Primary 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs / 2 Peak Elev= 231.11' @ 12.66 hrs Surf.Area= 3,065 sf Storage= 7,394 cf Flood Elev= 232.00' Surf.Area= 3,494 sf Storage= 10,313 cf

Plug-Flow detention time= 401.6 min calculated for 16,073 cf (100% of inflow) Center-of-Mass det. time= 401.8 min (1,230.5 - 828.7)

Volume	Invert	Avail.St	torage	Storage Description	n		
#1	228.00'	10,	313 cf	Main Infiltration B	a s in (Irregular) List	ed below (Recalc)	
Elevatio		ırf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
228.0 229.0 230.0 231.0 232.0	00 00 00	1,744 2,135 2,558 3,014 3,494	183.8 201.4 218.0 233.8 246.4	0 1,936 2,343 2,783 3,251	0 1,936 4,280 7,062 10,313	1,744 2,317 2,909 3,521 4,059	
Device	Routing	lnver	t Outle	et Devices			
#1	Discarded	228.00		0 in/hr Exfiltration (
#2	Primary	231.00	9' 8.0' Head 2.50	3.00 3.50 4.00 4.	Broad-Crested Re 0.60 0.80 1.00 1.2 50 5.00 5.50		
#3	Secondary	231.20	24.0	2.65 2.65 2.66 2. x 48.0" Horiz. Orif ted to weir flow at lo	ice/Grate C= 0.60		

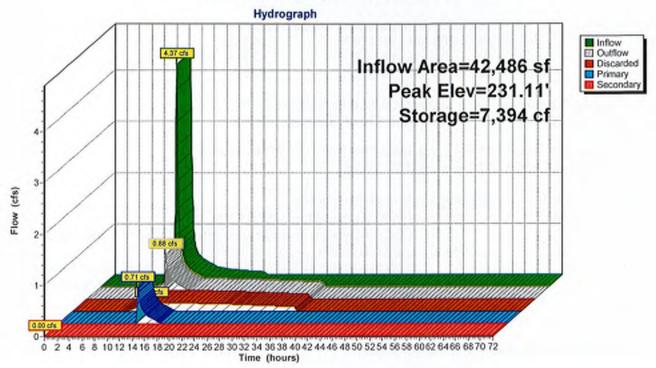
Discarded OutFlow Max=0.17 cfs @ 12.66 hrs HW=231.11' (Free Discharge)
1=Exfiltration (Controls 0.17 cfs)

Primary OutFlow Max=0.69 cfs @ 12.66 hrs HW=231.11' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 0.69 cfs @ 0.80 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=228.00' (Free Discharge) 3=Orifice/Grate (Controls 0.00 cfs)

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Pond DB-1: Prop Detention Basin



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Summary for Pond DW-1: Chamber drywell

Inflow Area = 2,174 sf,100.00% Impervious, Inflow Depth = 8.02" for 100-Year Design Storm event

Inflow = 0.40 cfs @ 12.09 hrs, Volume= 1,453 cf

Outflow = 0.02 cfs @ 10.60 hrs, Volume= 1,453 cf, Atten= 94%, Lag= 0.0 min

Discarded = 0.02 cfs @ 10.60 hrs, Volume= 1,453 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 231.13' @ 13.73 hrs Surf.Area= 430 sf Storage= 593 cf

Plug-Flow detention time= 191.2 min calculated for 1,452 cf (100% of inflow)

Center-of-Mass det. time= 191.1 min (931.9 - 740.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	229.10'	391 cf	11.17'W x 38.50'L x 3.54'H Field A
			1,523 cf Overall - 544 cf Embedded = 979 cf x 40.0% Voids
#2A	229.60'	544 cf	Cultec R-330XL x 10 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		935 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	_
#1	Discarded	229.10'	2.410 in/hr Exfiltration over Surface area	

Discarded OutFlow Max=0.02 cfs @ 10.60 hrs HW=229.14' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.02 cfs)

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Pond DW-1: Chamber drywell - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length

2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

10 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 543.9 cf Chamber Storage

1,522.6 cf Field - 543.9 cf Chambers = 978.7 cf Stone x 40.0% Voids = 391.5 cf Stone Storage

Stone + Chamber Storage = 935.4 cf = 0.021 af Overall Storage Efficiency = 61.4%

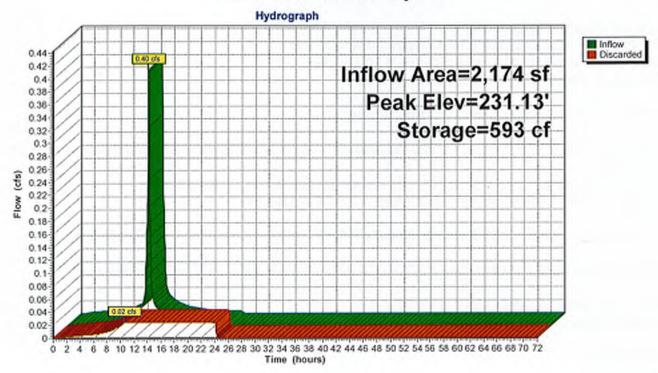
10 Chambers 56.4 cy Field 36.2 cy Stone





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Pond DW-1: Chamber drywell



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Summary for Pond DW-2: Chamber drywell Quad

Inflow Area = 6,891 sf,100.00% Impervious, Inflow Depth = 8.02" for 100-Year Design Storm event

Inflow = 1.25 cfs @ 12.09 hrs, Volume= 4,606 cf

Outflow = 0.09 cfs @ 10.95 hrs, Volume= 4,606 cf, Atten= 93%, Lag= 0.0 min

Discarded = 0.09 cfs @ 10.95 hrs, Volume= 4,606 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 236.69' @ 13.31 hrs Surf.Area= 1,600 sf Storage= 1,739 cf

Plug-Flow detention time= 142.9 min calculated for 4,602 cf (100% of inflow)

Center-of-Mass det. time= 142.8 min (883.6 - 740.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	234.70	995 cf	40.00'W x 40.00'L x 2.04'H Field A
			3,267 cf Overall - 778 cf Embedded = 2,489 cf x 40.0% Voids
#2A	235.20	778 cf	Cultec C-100 x 55 Inside #1
			Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf
			Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap
			Row Length Adjustment= +0.50' x 1.86 sf x 11 rows
		1 774 of	Total Available Storage

1,774 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	234 70'	2 410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.09 cfs @ 10.95 hrs HW=234.72' (Free Discharge)
1=Exfiltration (Exfiltration Controls 0.09 cfs)

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Pond DW-2: Chamber drywell Quad - Chamber Wizard Field A

Chamber Model = Cultec C-100

Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap Row Length Adjustment= +0.50' x 1.86 sf x 11 rows

36.0" Wide + 6.0" Spacing = 42.0" C-C Row Spacing

5 Chambers/Row x 7.50' Long +0.50' Row Adjustment = 38.00' Row Length +12.0" End Stone x 2 = 40.00' Base Length

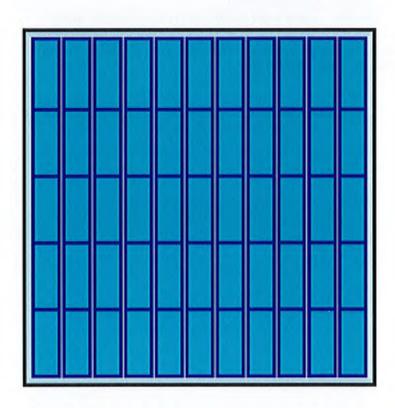
11 Rows x 36.0" Wide + 6.0" Spacing x 10 + 12.0" Side Stone x 2 = 40.00' Base Width 6.0" Base + 12.5" Chamber Height + 6.0" Cover = 2.04' Field Height

55 Chambers x 14.0 cf +0.50' Row Adjustment x 1.86 sf x 11 Rows = 778.1 cf Chamber Storage

3,266.7 cf Field - 778.1 cf Chambers = 2,488.6 cf Stone x 40.0% Voids = 995.4 cf Stone Storage

Stone + Chamber Storage = 1,773.5 cf = 0.041 af Overall Storage Efficiency = 54.3%

55 Chambers 121.0 cy Field 92.2 cy Stone

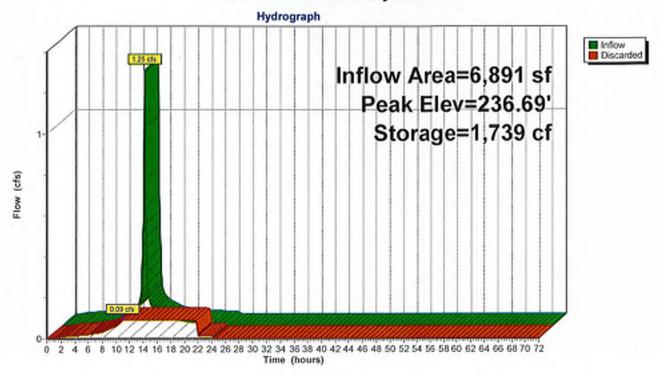




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Pond DW-2: Chamber drywell Quad



-						
-						



MASSACHUSETTS STORMWATER MANAGEMENT STANDARDS

Standard #1: Na New Untreated Discharges

Developmental Measures:

The proposed development on this site includes the construction of four new housing units in the form of one new building. A driveway will also be constructed to serve the new building. The two existing single-family homes on the property will remain, however the existing driveway will be reconstructed as part of the proposed driveway. The existing pool and shed will be removed.

To account for increased impervious from the new development, several stormwater management devices are proposed. Two subsurface infiltration systems are proposed to serve all three buildings (two existing and one proposed) on the site. These chambers will serve as drywells and are sized to infiltrate storms up to and including the 100-year storm event. Downspouts on all structures shall be fitted with overflows for larger storm events. Runoff from the remainder of the developed site shall be routed to a detention basin via deep sump catch basins and CDS treatment unit. The detention basin is sized to contain the 100-year storm, however the rim elevation of the upstream catchbasins have been set such that additional flow can backwater into the catchbasins and flow overland to the municipal system on Main Street.

Standard #2: Peak Rate Attenuation

SUMMARY OF COMPUTATIONS

DEP Stormwater Management Regulations as well as Medway's Stormwater and Land Disturbance Bylaw both stipulate that no increase in the rate nor volume of stormwater runoff is allowed between existing and proposed conditions on a site. The following table shows peak flow rates and runoff volumes for this site and demonstrate that no increase for either parameter is seen.

Design Point]					
Peak Flow (cfs)	2	Yr.	10	Yr.	100	Yr.
DP-1	0.47	0.11	1.28	0.35	2.78	0.88
OP-2	0.24	0.24	0.97	0.97	2.53	2.50

Design Point]					
Runoff Volume (cf)	2	Yr.	10	Yr.	100	Yr.
DP-1	2,529	509	6,196	1,328	13,201	5,709
DP-2	1,890	1,381	5,772	4,093	13,996	9,762

Existing
Proposed

Standard #3: Recharge Calculations

Based on the DEP Stormwater Handbook, a "Rawls" infiltration rate has been utilized for and Subsurface Infiltration Chamber Design. The NRCS Hydrologic Soil Group rating for site hydrology is "B" based on NRCS soil maps. On-site soil testing performed in April of 2020 revealed a layer of sandy loam underlain by loamy sand. As such, the chamber systems, which will be placed below existing grade in the loamy sand layer, were designed based on a Rawls Infiltration rate of 2.41 in/hr. This is consistent with HSG Type "A" soils. The detention basin, which will be constructed above existing grade and will therefore dewater into the sandy loam layer, was designed based on a Rawls Infiltration rate of 1.02 in/hr. This is consistent with Type "B" soils found at the surface across the site. Mounding and dewatering calculations were performed for each component consistent with the Rawls Rates noted above. NRCS data and test pit information supporting this can be found in the "Soils Information" section of this report.

The Required Recharge Volume (Rv):

This project is required to meet this Standard to the maximum extent practicable, but fully complies as designed. There are currently approximately 10,473 sf of impervious areas on the site. Under proposed conditions, the amount of impervious area would increase to 20,396 sf.

Total impervious on site = 20,396 sf

Rv = F * Impervious Area

F = Target Depth Factor associated with Hydrological Soll Group; HSG = 0.35 inches

 $Rv = {(0.35 in)(20,396 sf)}/{(12 in/ft)} = {594.9 ft}^{3}$

Recharge volume provided by DB-1: 10,313 ft3

Therefore, the total recharge volume provided is 10,313 ft³ > 594.95 ft³ required. OKAY

Drawdown Within 72 Hours

$$Time_{drawdown} = \frac{Rv}{(K)(Bottom\ Area)(n)}$$

Rv = Storage Volume (recharge volume provided)%

K = Saturated Hydraulic Conductivity (1.02 in/hr for PP-1, 2.41 in/hr for dry wells)

Bottom Area = Bottom Area of Recharge Structure

n = porosity of the stone; If applicable

DB-1

$$Tinne_{drivedown}$$
 SIS = 10,313 cu.ft / (2.41 in/hr * 1/12 ft/in * 3,494 sq.ft.) = 14.7 hrs <72 hrs

DW-1

$$Time_{drawdown}$$
 SIS = 593 cu.ft / (2.41 in/hr * 1/12 ft/in * 430 sq.ft.) = 6.9 hrs < 72 hrs

DW-2

 $Time_{drawdown}$ SIS = 1,739 cu.ft / (2.41 in/hr * 1/12 ft/in * 1,600 sq.ft.) = 5.4 hrs < 72 hrs

Standard #4: Woter Quality Valume Calculations

The Water Quality Treatment Volume (Vwq):

 $V_{WQ} = (D_{WQ}/12 \text{ inches/foot})^* (A_{IMP})$

 $D_{WQ} = 1$ inch (required water quality volume)

A_{IMP} = 11,331 sf (does not include building roofs)

Vwq (Proposed) = (1 inch/12 inches/foot)* (11,331 sf) = 944 ft?

→ 7,062 ft³ provided by detention basin DB-1 (below 231.0)

TSS Removal Rate

Using deep sump catch basins, a CDS treatment unit, and a detention basin, a TSS removal efficiency of 95% is achieved. See attached TSS calculation worksheet.

Stondord #5: Lond Uses with Higher Potential Pollutont Laads

This project does not have a land use with a higher potential pollutant loads.

Stondord #6: Critical Areos

This project does not discharge to a Zone II, Interim Wellhead Protection Areas or directly to a Cold-Water Fisheries.

Standord #7: Redevelopment

While part of the Project could qualify as "redevelopment," the calculations for Standards 2-6 demonstrate full compliance with Massachusetts Stormwater Regulations and Medway's Stormwater Management and Land Disturbance Bylaw.

Standard #8: Construction Periad Controls

Upon completion of the project, the site will have disturbed approximately 1.15 acres, therefore a NPDES Construction General Permit is required and will be completed prior to construction.

Stondord #9: Operation And Maintenance Plan

A Long-Term Operation and Maintenance (O&M) Plan has be developed and is attached to this report.

Stondord #10: Illicit Dischorges To Droinoge System

An Illicit Discharge Compliance Statement has not been incorporated into the Operation and Maintenance (O&M) plan, however one will be completed prior to construction.

INSTRUCTIONS:

- 1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table
- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D

E1	O	Starting TSS Amount	Load* Removed (B*C)	1.00	0.75	0.26	
		moval					
Location:	В	TSS Re	Rate	looded 0.25	0.65	tem 0.80	
Locs	A		BMP1	Deep Sump and Hooded Catch Basin	CDS Unit	Infiltration System	

Total TSS Removal =

95%

Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: 218-222 Main Street, Medway
Prepared By: Meridian Associates, Inc.

*Equals remaining load from previous BMP (E)

This spreadsheet will calculate the height of a groundwater mound beneath a stormwater infiltration basin. More information can be found in the U.S. Geological Survey Scientific Investigations Report 2010-5102 "Simulation of groundwater mounding beneath hypothetical stormwater infiltration basins".

The user must specify infiltration rate (it), specific yield (5y), horizontal hydraulic conductivity (Xh), basin dimensions (x, y), duration of infiltration period (it), and the initial thickness of the saturated zone (hij(i), height of the water table if the bottom of the aquifer is the datum). For a square basin the half width equals the half length (x = y). For a rectangular basin, if the user wants the water-table changes perpendicular to the long side, specify x as the short dimension and y as the long dimension. Conversely, if the user wants the values perpendicular to the short side, specify y as the short dimension, x as the long dimension. All distances are from the center of the basin. Users can change the distances from the center of the basin at which water-table aquifer thickness are calculated.

Cells highlighted in yellow are values that can be changed by the user. Cells highlighted in red are output values based on user-specified inputs. The user MUST click the blue "Re-Calculate Now" button each time ANY of the user-specified inputs are changed otherwise necessary iterations to converge on the correct solution will not be done and values shown will be incorrect. Use consistent units for all input values (for example, feet and days)

put Values		use consistent unit	is (e.g. feet & days or inches & hours)	Conversion inch/hou	n Table feet/d	ay
4.8200	R	Recharge (infiltra	ation) rate (feet/day)	0	67	1.33
0.150	Sy	Specific yield, Sy	(dimensionless, between 0 and 1)			
48.20	K	Horizontal hydra	ulic conductivity, Kh (feet/day)*	2	.00	4.00 in the report accompanying this spreadsheet
27.500	×	1/2 length of bas	in (x direction, in feet)			(USGS SIR 2000-5102), vertical soil permeability
14.750	y	1/2 width of basi	in (y direction, in feet)	hours	days	(ft/d) is assumed to be one-tenth horizontal
0.230	t	duration of infilt	ration period (days)		36	1.50 hydraulic conductivity (ft/d).
3.950	hi(0)	initial thickness of	of saturated zone (feet)			
7.663 3.713	h(max) Ah(max)		ess of saturated zone (beneath center dwater mounding (beneath center of			1.6. C
iter ce ounding in in	et 0	Do Colo	ulata Navu			
oter ce ounding in in et fe 3.713 2.667	enter of basin ex direction, in et 0 25	Re-Calc	ulate Now			
ter ce sunding, in in e fe 3.713 2.562 0.871 0.007	onter of basin x direction, in et 0 25 50 75	Re-Calc		unding in	fact	
ter ce bunding in in e fe 3.713 2.962 0.371 0.007 0.008	onter of basin x direction, in et 0 25 50 75	Re-Calc	ulate Now Groundwater Mo	unding, in	feet	
ster ce sunding, in in et fe 8,718 2,962 0,871 0,007 0,009 0,000	onter of basin x direction, in et 0 25 50 75 100 125	Re-Calc	Groundwater Mo	unding, in	feet	
ter ce sunding, in in et fer 3,713 2,562 0,371 0,007 0,007 0,000 0,000	onter of basin x direction, in et 0 25 50 75 100 125 150		Groundwater Mo	unding, in	feet	
ater ce ounding in in et fe 3,713 2,962 0,871 0,007 0,008 0,002	onter of basin x direction, in et 0 25 50 75 100 125	4.0	Groundwater Mo	unding, in	feet	
ater ce lounding, in in et fe 3.713 2.967 0.871 0.027 0.003 0.003	onter of basin x direction, in et 0 25 50 75 100 125 150	4.0	Groundwater Mo	unding, in	feet	

50

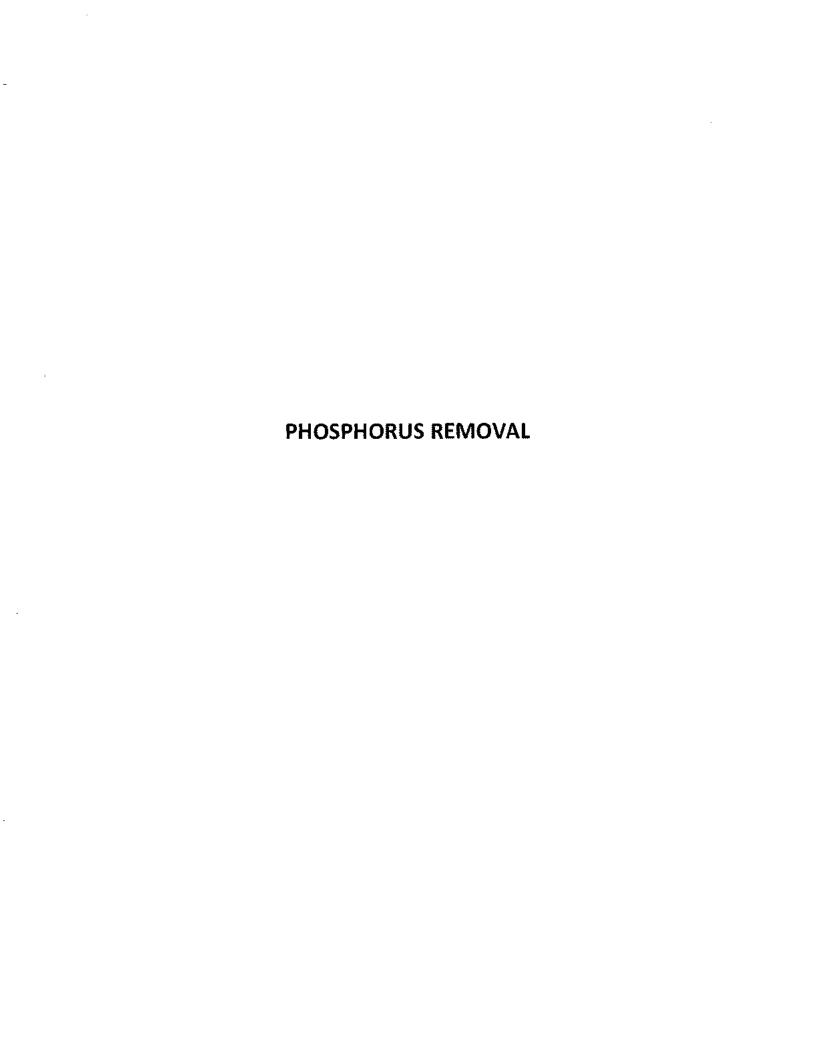
150

Disclaimer

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

0.500

-0.500



From MA MS4 General Permit Appendix F Attachment 3: Method to determine the phosphorus load reduction for a BMP with known storage volume when both pervious and impervious drainage areas are present.

For DB-1:

Impervious area (IA) = 11,331 SF = 0.26 Ac.
Pervious Area (PA) = 31,155 SF = 0.7115 Ac.
DB-1 Volume (below 231.0) = 7,062 CF
Depth of runoff treated from IA for 50% reduction = 0.2 in.

DB-1 Volume is converted to inches of runoff from the contributing IA: DB-1 Vol = $(7,062 \text{ SF}/0.26 \text{ Ac.}) \times (12 \text{ in/ft} / 43,560 \text{ SF/Ac}) = 7.48 \text{ in.}$

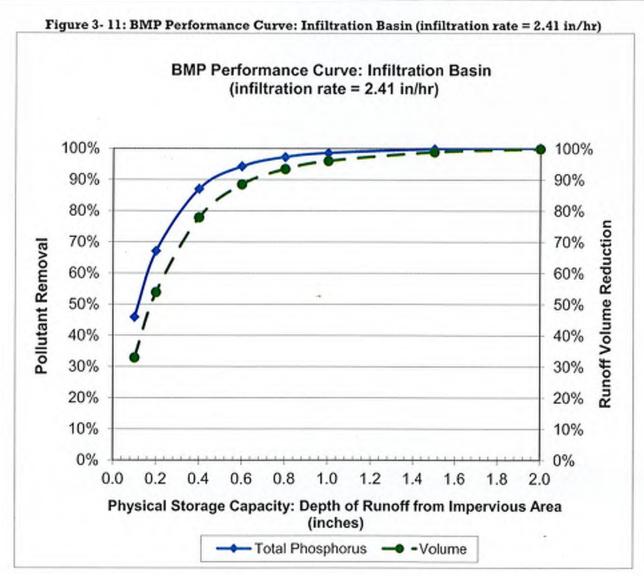
Volume of runoff from PA: (0.715 Ac. x 0.2 in.) x 3,630 cf/Ac-in. = 519 CF

Portion of DB-1 Vol available to treat runoff from IA: 7,062 CF - 519 CF = 6,543 CF $(6543 \text{ CF}/0.26 \text{ Ac.}) \times (12 \text{ in/ft} \times 1 \text{ Ac.}/43,560 \text{ SF}) = 6.93 \text{ in.}$

Per Table 3-14 (attached), any treatment depth of 2 inches or greater will yield 100% phosphorous removal.

Table 3-14: Infiltration Basin (2.41 in/hr) BMP Performance Table

Infiltration Basin (2.41 in/h		Perfori			Long-	Term F	Phosph	orus
BMP Capacity: Depth of Runoff Treated from Impervious Area (inches)	0.1	0.2	0.4	0.6	0.8	1.0	1.5	2.0
Runoff Volume Reduction	32.8%	53.8%	77.8%	88.4%	93.4%	96.0%	98.8%	99.8%
Cumulative Phosphorus Load Reduction	46%	67%	87%	94%	97%	98%	100%	100%





Stormwater Management Operation and Maintenance Plan Multifamily Development

218-220 Moin Street, Medwoy, Mossochusetts

June 10, 2020 Revised November 12, 2020

In accordance with Standard 9 of the Massachusetts Department of Environmental Protection (MassDEP) Stormwater Handbook, the attached on-site maintenance program for the proposed stormwater management system has been developed to ensure the Best Management Practices (BMP's) in place will remain functioning as designed. The Plan contains both construction period operations and maintenance as well as post construction responsibilities that shall "run" with the property if ownership is transferred.

All stormwater management-related records shall be retained for a minimum of three (3) years. These records shall be available for inspection during normal business hours upon request by City or MassDEP personnel.

Owner/Operator:

Harmony Village LLC 218 Main Street Medway, MA 02053

Construction Period Operation and Maintenance

Erosion Control Barrier:

Compost filter socks ("Filtrexx Soxx"), or approved equal, shall be installed where indicated on the plans and in other appropriate locations where warranted. These barriers shall be installed prior to the commencement of any work on site and in accordance with the construction plans. A supply of erosion control barrier materials shall be kept on site to replace and/or repair barriers that are damaged or degraded. The barriers shall be observed and maintained as necessary on a weekly basis and after every rainfall event of 0.25 inches or more during construction.

Deep Sump Catch Basin Protection:

Temporary catch basin protection barriers consisting of compost filter socks and a Silt Sack will be placed around and In all constructed inlets to prevent inflow of sediment into the constructed drainage systems. The barriers shall remain in place until a permanent cover is established or diversions away from the catch basin are constructed. The barrier shall be observed and maintained as necessary on a weekly basis and after every rainfall event of 0.25 inches or more. If inspection identifies the presence of hydrocarbons, these materials shall be immediately removed and disposed of in accordance with applicable local, state and federal guidelines and regulations.

Harmony Village: 218-220 Main Street

November 12, 2020

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Diversions:

Temporary diversion swales and mounds will be constructed to divert stormwater away from areas under construction to limit sediment transport. These diversions will be relocated as construction progresses. Compost filter socks shall be installed in the centerline of swales where necessary to reduce storm velocities and soil erosion.

Sediment Traps:

Temporary sediment traps shall be utilized to limit sediment transport off-site. These traps will be sized according to Massachusetts DEP and US EPA guidelines and will be relocated as construction progresses. No sediment shall be allowed to enter the infiltration components of the stormwater system.

Surface Stabilization:

The surface of all disturbed areas shall be stabilized during and after construction. Temporary measures shall be taken during construction to prevent erosion and siltation. All finished surfaces shall be stabilized with finish materials or permanent vegetative cover. Some or all of the following measures will be utilized on this project as conditions may warrant.

- Temporary Seeding
- Temporary Mulching
- Permanent Seeding
- Placement of Sod
- Hydroseeding
- Placement of Hay
- Placement of Jute Netting

Subsurface Storage Facilities:

Construction activity above and around the proposed location of the subsurface storage facilities shall be limited to prevent compaction of the existing soil. Care shall be taken to redirect stormwater runoff from this area to prevent ponding. Installation of this system shall occur under dry weather conditions and system shall be backfilled immediately to prohibit the introduction of fines or other material that would compromise the functionality of this system.

Spill Control:

A contingency plan to address the spillage/release of petroleum products and any hazardous materials will be implemented for the site during construction. The plan will include the following measures:

 Equipment necessary to quickly attend to inadvertent spills or leaks shall be maintained on-site in a secure but accessible location. Such equipment will include, but not be limited to, the following: urethane drain cover seals (mats), a spill containment kit which includes sand and shovels, suitable absorbent materials,

Harmony Village: 218-220 Main Street

November 12, 2020

Page 3

storage containers, safety goggles, chemically resistant gloves and overshoe boots, water and chemical fire extinguishers, and first aid equipment.

- Spills or leaks will be treated properly according to material type, volume of spillage and location of spill. Mitigation will include preventing further spillage, containing the spilled material in the smallest practical area, removing spilled material in a safe and environmentally friendly manner, and remediating any damage to the environment.
- The contractor shall be familiar with the reporting requirements of the Massachusetts
 Contingency Plan (310 CMR 40.00) as issued by the Massachusetts Department of
 Environmental Protection (DEP); specifically Subpart C Notification of Releases and
 Threats of Release of Oil and Hazardous Materials and Subpart D Preliminary Response
 Activities and Risk Reduction Measures.
- For any large spills, Massachusetts DEP Hazardous Waste Incident Response Group will be notified immediately at (617) 792-7653 and an emergency response contractor will be called in.

Long-Term Operation and Maintenance

General House Keeping:

The site should generally be kept clean and free of debris such as leaves, limbs, trash, construction materials, etc. Maintenance of lawns, gardens and other landscaped areas should be done regularly and any clippings composted or disposed of as appropriate and recommended by Medway DPW. Pet waste should be picked up and disposed of in trash.

Deep Sump Hooded Catch Basins:

Deep Sump Drain Basins shall be inspected at least four times per year. Accumulated sediment in drain basins shall be removed when sediment accumulates to 24 inches below the invert of the outlet pipe of the drain basins; but should be removed during late winter / early spring at a minimum. Sediment shall be transported off site and disposed of in accordance with applicable local, state and federal guidelines and regulations. Care shall be taken to not dislodge the hood/tees on the outlet pipes. If dislodged, the hood/tee shall be immediately reinstalled and secured.

CDS® Treatment Units:

CDS treatment units shall be inspected a minimum of four times per year until the site reaches "equilibrium"; after which time annual inspections are typically sufficient. Accumulated sediment shall be removed via a vacuum truck when it reaches a depth of 1.5 feet. Any accumulated hydrocarbons shall be removed via the inspection / cleanout port. Refer to spill control section below in the event of any hazardous material spill. Transport and dispose of sediment and hydrocarbons off site in accordance with applicable local, state and federal guidelines and regulations. See the attached CDS Inspection and Maintenance Guide/Log as provided by Contech Construction Products, Inc.

Harmony Village: 218-220 Main Street

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Subsurface Storage Facilities:

The subsurface storage system inspections should include inspections following the first several rainfall events or first few months after construction, after all major storms (2-year), and on regular bi-annual scheduled dates, to ascertain whether captured runoff dissipates within 72 hours following the event. Ponded water inside the system (as visible from the observation port) after several days often indicates that the bottom of the system is clogged. If the water does not drain, then a qualified professional should be retained to determine the cause of apparent infiltration failure and recommend corrective action. Such corrective action should be immediately implemented by the owner. The system should receive little or no sediment. If any significant sediment is observed in the observation ports or drain manhole, then the system can be cleaned based on manufacturer recommendations and the source of the sediment eliminated.

Storage/Recharge Basin, Weir/Spillway, Flared End Inlets:

The open storage/recharge basin and flared end inlet shall be inspected annually to ensure basin is operating properly. Inlet and outlets shall be examined for clogging. Sediment accumulation shall be removed from inlets and rip-rap areas as required to maintain free flow. Sediment accumulation shall be removed from the basin at least once every five (5) years or when it accumulates over twelve (12) inches above bottom.

Vegetation on the side slopes and basin bottom shall be mowed and any woody growth shall be removed on a regular basis so that trees and large scrub brush does not grow in the basin.

Storing Materials and Waste Products:

General storage of materials and waste products should be kept inside and/or under cover (garage, basement, carport, etc.).

Vehicle Washing:

Vehicle washing should be done sparing as allowed by Medway water regulations. Washing products used should be safe for the environment.

Snow Removal:

Snow that is removed from paved surfaces shall not be stored over catch basins or in the recharge basin. In the event that snow storage areas are depleted, snow is to be transported off-site.

De-icing:

The use of Sodium Chloride ("rock salt") for de-icing of paved surfaces is not permitted. The use of Calcium Chloride is allowed but will be limited. Sand will be the primary icing control agent.

Harmony Village: 218-220 Main Street

November 12, 2020

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Fertilizer:

Slow release organic fertilizers will be used in landscape areas to limit nutrient transport to groundwater and any offsite wetland areas. Application will be limited to 3 lbs. per 1000 square feet of lawn area.

Waste Management:

Solid waste will be contained within dumpsters for pick up by a privately contracted waste hauler. Waste deposition in these dumpsters will be consistent with state and local permits. The covers of the dumpster and doors of the dumpster enclosure will be kept closed to limit rainwater and pest intrusion.

Spill Control:

A contingency plan to address the spillage/release of petroleum products and any hazardous materials will be implemented for the facility. The plan will include the following measures:

- Spills or leaks will be treated properly according to material type, volume of spillage and location of spill. Mitigation will include preventing further spillage, containing the spilled material in the smallest practical area, removing spilled material in a safe and environmentally friendly manner, and remediating any damage to the environment.
- The catch basins have a specific internal storage capacity that will be available in the event of any hazardous material spill. However, for added security, urethane drain cover seals ("mats") will be kept on-site to be placed over the grate of the catch basin to assist with the prevention of flow from entering the drainage system in the event of a spill. These should be kept in an easily accessible on-site location.
- The owner shall be familiar with the reporting requirements of the Massachusetts Contingency Plan (310 CMR 40.00) as issued by the Massachusetts Department of Environmental Protection (DEP); specifically Subpart C Notification of Releases and Threats of Release of Oil and Hazardous Materials and Subpart D Preliminary Response Activities and Risk Reduction Measures.
- For any large spills, Massachusetts DEP Hazardous Waste Incident Response Group will be notified immediately at (617) 792-7653 and an emergency response contractor will be called in.

Prohibition of Illicit Discharges

All illicit discharges to the stormwater management system are prohibited. Illicit discharges to the stormwater management system are discharges that are not entirely comprised of stormwater.

An Illicit discharge does not include allowable non-stormwater discharges from the following activities or facilities: firefighting, water line flushing, landscape irrigation, uncontaminated groundwater, potable water sources, foundation drains, air conditioning condensation, footing drains, individual resident car washing, flows from riparian habitats and wetlands,

Stormwater Management Operation and Maintenance Plan Harmony Village: 218-220 Main Street November 12, 2020 Page 6

dechlorinated water from swimming pools, water used for street washing and water used to clean residential building without detergents.

Long-Term Operation and Maintenance Budget

Consistent with Standard 9 of the Massachusetts Department of Environmental Protection Stormwater Handbook (February 2008) the approximate cost of inspections and maintenance based on the abovementioned post-construction activities and frequencies is as follows;

- Deep Sump Catch Basins & Trench Drain/Manhole inspection/cleaning \$2,000 per year based on quarterly inspections and sediment removal from the three (3) deep sump catch basins/inlets and one drain/manhole.
- Stormwater Quality Units (CDS) inspection/cleaning \$500.00 per year based on quarterly inspections (or per manufacturer's guidelines) and sediment removal for one unit
- Subsurface Storage Chambers \$1,000 per year based on bi-annual inspections. Any necessary maintenance costs to be determined based on observations.
- Storage/Recharge Basin inspection/cleaning \$500 per year/cleaning \$500 (as required based upon yearly inspection).

Additional costs may be incurred if it is determined during routine inspections of the BMP's that further corrective actions are necessary.

G:\^\8521 Medway\Engineering\Stormwater Report\Rev 20201110\8521_O&M.doc

Stormwater Management Operation and Maintenance Plan Harmony Village: 218-220 Main Street November 12, 2020 Page 7

Inspection Report

Operation and Maintenance Log

General Information					
Project Name	Harmony Village				
MAI Project No.	8521	Location	218-220 Main Street		
			Medway, MA 02053		
Date of Inspection		Start/End Time			
Inspector's Name(s)					
Inspector's Title(s)					
Inspector's Contact Information					
Inspector's Qualifications					
Describe present phase of					
construction					
Type of Inspection: ☐ Regular ☐ Pre-storm event	☐ During storm event	☐ Post-storm e	vent		
The storm events	Weather Info				
Has there been a storm event since					
If yes, provide:					
	orm Duration (hrs):	Approximate :	Amount of Precipitation (in):		
Weather at time of this inspection?					
☐ Clear ☐ Cloudy ☐ Rain ☐		ng 🔲 High Winds			
Other:	Temperature:				
Have any discharges occurred since	the last increation? These	TNO			
If yes, describe:	the last inspections. Laves	⊒ ₩0			
Are there any discharges at the tim	e of inspection? 🗆 Yes 🗆 N	lo			
If yes, describe:					

Harmony Village: 218-220 Main Street

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Site-specific BMPs

Number the structural and non-structural BMPs identified in your O&M Plan on your site map and list
them below (add as many BMPs as necessary). Carry a copy of the numbered site map with you during
your inspections. This list will ensure that you are inspecting all required BMPs at your site.

Describe corrective actions initiated, date completed, and note the person that completed the work in

the Corrective Action Log.

	ВМР	BMP Installed?	BMP Maintenance Required?	Corrective Action Needed and Notes
1		□Yes □No	□Yes □No	
2		□Yes □No	□Yes □No	
3		□Yes □No	□Yes □No	
4		□Yes □No	□Yes □No	
5		□Yes □No	∐Yes ∐No	
6		□Yes □No	□Yes □No	
7		□Yes □No	□Yes □No	
8		□Yes □No	□Yes □No	***************************************
9		□Yes □No	□Yes □No	
10		□Yes □No	□Yes □No	

Overall Site Issues

Below are some general site issues that should be assessed during inspections. Customize this list as needed for conditions at your site.

	BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes
1	Are all slopes and disturbed areas not actively being worked properly stabilized?	□Yes □No	□Yes □No	
2	Are natural resource areas (e.g., streams, wetlands, mature trees, etc.) protected with barriers or similar BMPs?	□Yes □No	∐Yes QNo	
3	Are perimeter controls and sediment barriers adequately installed (keyed into substrate) and maintained?	□Yes □No	□Yes □No	
4	Are discharge points and receiving waters free of any sediment deposits?	□Yes □No	□Yes □No	
5	Are storm drain inlets properly protected?	□Yes □No	□Yes □No	
6	Is the construction exit preventing sediment from being tracked into	□Yes □No	□Yes □No	

Harmony Village: 218-220 Main Street

November 12, 2020

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	BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes	·
:	the street?		-		
7	is trash/litter from work areas collected and placed in covered dumpsters?	□Yes □No	□Yes □No		
8	Are washout facilities (e.g., paint, stucco, concrete) available, clearly marked, and maintained?	□Yes □No	□Yes □No		
9	Are vehicle and equipment fueling, cleaning, and maintenance areas free of spills, leaks, or any other deleterious material?	□Yes □No	UYes □No		
10	Are materials that are potential stormwater contaminants stored inside or under cover?	□Yes □No	□Yes □No		
11	Are non-stormwater discharges (e.g., wash water, dewatering) properly controlled?	□Yes □No	□Yes □No		
12	(Other)	∐Yes □No	□Yes □No		
			Non-Complia	ince	
Des	cribe any incidents of non-co	ompliance not des	scribed above:		

MADEP STORMWATER MANAGEMENT CHECKLIST



Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



Checklist for Stormwater Report

B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

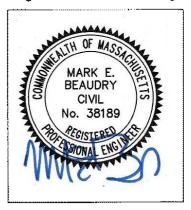
Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



Please See Stamp to Left - 11/12/2020

Signature and Date

Checklist

	ject Type : Is the application for new development, redevelopment, or a mix of new and evelopment?
	New development
	Redevelopment
X	Mix of New Development and Redevelopment



Checklist for Stormwater Report

Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

X	No disturbance to any Wetland Resource Areas
	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	☐ Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):
Sta	ndard 1: No New Untreated Discharges
X	No new untreated discharges
	Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
X	Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Checklist for Stormwater Report

Checklist (continued) Standard 2: Peak Rate Attenuation Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding. Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm. Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm. Standard 3: Recharge Soil Analysis provided. Required Recharge Volume calculation provided. Required Recharge volume reduced through use of the LiD site Design Credits. Sizing the infiltration, BMPs is based on the following method: Check the method used. Dynamic Field¹ X Static ☐ Simple Dynamic Runoff from all impervious areas at the site discharging to the infiltration BMP. Runoff from all impervious areas at the site is not discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum extent practicable for the following reason: Site is comprised solely of C and D soils and/or bedrock at the land surface M.G.L. c. 21E sites pursuant to 310 CMR 40.0000 Solid Waste Landfill pursuant to 310 CMR 19.000 Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable. Calculations showing that the infiltration BMPs will drain in 72 hours are provided. Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

^{1 80%} TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Checklist for Stormwater Report

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Checklist (continued)

Standard 3: Recharge (continued)

The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.

Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.

applicable, the 44% TSS removal pretreatment requirement, are provided.

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	A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
	Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
	is within the Zone II or Interim Wellhead Protection Area
	is near or to other critical areas
	is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
	involves runoff from land uses with higher potential pollutant loads.
	The Required Water Quality Volume is reduced through use of the LID site Design Credits.
X	Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if



Checklist for Stormwater Report

Cl	necklist (continued)
Sta	indard 4: Water Quality (continued)
X	The BMP is sized (and calculations provided) based on:
	☐ The ½" or 1" Water Quality Volume or
	The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
	The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
	A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Sta	indard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
	The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior</i> to the discharge of stormwater to the post-construction stormwater BMPs.
	The NPDES Multi-Sector General Permit does not cover the land use.
	LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
	All exposure has been eliminated.
	All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
	The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Sta	ndard 6: Critical Areas
	The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
	Critical areas and BMPs are identified in the Stormwater Report.



Checklist for Stormwater Report

Checklist (continued)

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

X		e project is subject to the Stormwater Management Standards only to the maximum Extent cticable as a:
		Limited Project
		Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area. Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
		Bike Path and/or Foot Path
		Redevelopment Project
	X	Redevelopment portion of mix of new and redevelopment.
	The implied the and	tain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an clanation of why these standards are not met is contained in the Stormwater Report. It project involves redevelopment and a description of all measures that have been taken to prove existing conditions is provided in the Stormwater Report. The redevelopment checklist found foliume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment I structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) proves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- · Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Checklist for Stormwater Report

Checklist (continued) Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued) The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application, A Construction Period Pollution Prevention and Erosion and Sedimentation Control has not been included in the Stormwater Report but will be submitted before land disturbance begins. The project is **not** covered by a NPDES Construction General Permit. ☐ The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report. The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins. Standard 9: Operation and Maintenance Plan The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information: Name of the stormwater management system owners; Party responsible for operation and maintenance; Schedule for implementation of routine and non-routine maintenance tasks; Plan showing the location of all stormwater BMPs maintenance access areas; Description and delineation of public safety features; X Estimated operation and maintenance budget; and X Operation and Maintenance Log Form. The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions: A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs; A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions. Standard 10: Prohibition of Illicit Discharges The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges; An Illicit Discharge Compliance Statement is attached; NO Illicit Discharge Compliance Statement is attached but will be submitted prior to the discharge of any stormwater to post-construction BMPs.