

April 24, 2017 Revised: June 26, 2017

Stormwater Management Report

Submittal To:

Medway Zoning Board

Glen Brook Way

Definitive Site Plan "Glen Brook Way" #20 West Street Medway, Massachusetts

April 20, 2017 Revised: June 26, 2017

STORMWATER MANAGEMENT REPORT AND HYDROLOGIC-HYDRAULIC ANALYSIS

Project Summary

The subject property is located on the southwesterly side of West Street approximately $\frac{1}{2}$ mile from the intersection of Hartford Avenue (Rte 126). The property is located within the Agricultural-Residential II (AR-II) district as depicted on the Town of Medway Zoning Map. According to the Medway Assessor's Maps, the Site is comprised of 3 parcels with frontage along Glen Brook Way which is within the Site Locus. A portion of the rear property line of Lot 3 is defined by the Hopping Brook. The roadway was never constructed and the Applicant plans to eliminate the existing interior lot lines and easements as part of this project. The property consists of a total of $3.16\pm$ acres of which $0.54\pm$ acres ($23,411\pm$ s.f.) are wetlands.

The majority of the work associated with this proposal takes place within the front or northeasterly portion of the property with a small amount of alteration $(6,590 \pm \text{ s.f.})$ within the Riverfront Area associated with Hopping Brook towards the rear of the property. Access to the site is currently provided from West Street.

The existing Site includes a residential dwelling which according to Assessor's records was constructed in about 1935 along with an attached garage, shed, bituminous concrete driveway and other associated site amenities. The proposed project includes the demolition of the existing residential structure and shed, etc and the construction of 6 new multi-family residential structures with a total of 48 rental units. Also included in this proposal are the construction of access driveways, children's play areas, parking areas, landscape features and other site amenities.

Methodology

Drainage computations were performed using the Natural Resources Conservation Services (NRCS) TR-20 method and HydroCAD[®] Drainage Calculation Software. The HydroCAD[®] Report, and copies of the calculation sheets are included as appendices to this report.

Existing Conditions

Under existing conditions, stormwater runoff from the proposed project area flows from the higher areas of the Lot along West Street towards both Hopping Brook to the southwest and to the adjacent parcel, #31 West Street to the south. No treatment for water quality presently exists for any stormwater on the existing site, it simply flows overland towards one of the two tributary areas. Soil types were obtained from NRCS mapping and were found to be HSG A soils in the front or northeasterly portion of the lot and HSG B/D soils as you drop in elevation and get further into the site towards the river. In order to confirm the soil class and groundwater depth characteristics of these soils, test pits were performed by Merrill Engineers and Land Surveyors in December of 2016. The area where all of the structures and proposed construction will occur is completely located within areas mapped as HSG A soils so this is where all of the soils testing was performed. Based on soil textures encountered at the time of testing, these areas were found to be consistent with an A soil (coarse sand). To be conservative, an exfiltration rate of 2.41in/hr was used in the stormwater calculations for the subsurface infiltration systems.

Proposed Conditions/Stormwater Management

Under the post development condition, a high point will be constructed at the propertyline for both access driveways and runoff from the new driveways and parking areas will follow the existing topography and slope towards the front of buildings 5 and 6 where there are two deep sump hooded catch basin's set at two low points to collect all of the runoff from the impervious driveway and parking areas along with landscaped areas between buildings 1-4. From here, the runoff will be directed into a 49.83' wide x 157.50' long subsurface infiltration system #2 comprised of Cultec R-330XLHD chambers (see attached calculations and plans for more details). Runoff from the roof areas of buildings 1-3 would be considered "clean" runoff and therefore does not require pretreatment. This runoff would be routed directly into a smaller 40.17' long x 31.50' wide subsurface infiltration system #1 using the same chambers. Both of these systems have been designed to infiltrate up to and including the 100 year design storm. An emergency overflow has been designed for the larger infiltration system #2.

Compliance with Stormwater Management Standards

Standard 1 – No New Untreated Discharges

No new stormwater conveyances will discharge untreated pavement runoff into, or cause erosion to downgradient areas. Under existing conditions, a large portion of the site allows untreated stormwater to flow off the property without any treatment whatsoever. As mentioned above, the proposed site design will direct stormwater from all impervious areas on site to the stormwater management system where it will be treated and infiltrated for all design storm events.

Standard 2 - Peak Rate Attenuation

Peak rates of runoff were calculated using the TR-20 methodology developed by the NRCS (refer to Appendices). Since the impervious area on site will be increased from the existing conditions, there will be an increase in runoff rates under the proposed conditions. In order to meet the requirements of Standards #3 for recharge and water quality requirements, two subsurface infiltration systems will provide treatment, infiltration and storage volume controls. These measures will both detain and infiltrate runoff, mitigating increased rates and volumes of runoff for the 2, 10, 25 and 100 year storms events.

	EXISTING (CONDITIONS	PROPOSED CONDITIONS		
RETURN	TRIB TO #31	TRIB TO HOPPING	TRIB TO #31	TRIB TO HOPPING	
PERIOD	WEST ST	BROOK	WEST ST	BROOK	
	RATE (cfs),	RATE (cfs),	RATE (cfs),	RATE (cfs),	
	VOLUME (cf)	VOLUME (cf)	VOLUME (cf)	VOLUME (cf)	
2YR	0.00	0.09	0.00	0.09	
	14	1,093	2	925	
10YR	0.05	0.84	0.01	0.69	
	910	4,556	154	3,445	
25YR	0.30	1.95	0.05	1.46	
	2,424	8,406	410	6,157	
100YR 1.64 7,170		1.64 4.81 7,170 18,351		3.41 13,022	

The following is a summary of pre- and post-construction rates of runoff:

Standard 3 – Groundwater Recharge

Runoff will be infiltrated by the subsurface infiltration systems which have both been designed a minimum of two feet above seasonal high groundwater. The hydraulic conductivity was based on soil conditions found on the site via soil testing and DEP SMR Table 2.3.3 1982 Rawls Rates - values developed from Rawls, Brakensiek and Saxton, 1982. The total required groundwater recharge volume was calculated to be 1,854 cubic feet. The proposed subsurface infiltration systems will provide 20,766± cubic feet of recharge below the outlets, well above the requisite recharge volume for this project. Refer to Appendix B for infiltration system calculations and Appendix C for recharge volume calculations and soil testing results.

Standard 4 – Water Quality

A Long Term Source Control/Pollution Prevention Plan will incorporated into the Operation and Maintenance Plan once the project is funded by HDCD. The water quality

volume was calculated using the $\frac{1}{2}$ inch rule as the site is not within a critical area as defined by the Massachusetts Stormwater Handbook. The total required water quality treatment volume was calculated to be 2,317 cubic feet. The volume below the outlet in the large infiltration system, which will handle all of the runoff from the parking areas, is $17,900\pm$ c.f.. well above the requisite water quality volume for the proposed site design. Refer to Appendix C for water quality calculations.

In accordance with the guidelines of the Stormwater Management Policy, the Total Suspended Solids (TSS) Removal was calculated to be 89% for the new treatment train which will handle the stormwater runoff from the proposed project area. The treatment trains consist of deep sump hooded catch basins which capture runoff and direct it towards a subsurface infiltration system with a separator row. The separator row essentially functions as a sediment forebay and has been sized to treat 400 c.f. of runoff per impervious acre proposed to achieve the required minimum removal rate of 80% total suspended soils. TSS removal calculations are included in Appendix C.

Standard 5 – Land Use with Higher Potential Pollutants Loads (LUHPPL)

The proposed project does not include land uses with higher potential pollutant loads. Not Applicable.

Standard 6 – Critical Areas

The proposed project does not discharge to any critical areas. Not Applicable.

<u>Standard 7 – Redevelopment and Other Projects Subject to the Standards only to the</u> <u>maximum extent practicable</u>

The project site is currently developed and the proposed project consists of the razing of the existing building and the reconstruction of six new buildings with new driveways, parking areas, landscaping, drainage improvements and other associated site improvements. The proposed development could be considered redevelopment as much of the site is altered and has been cleared for the construction of a 3-lot subdivision roadway. In order to provide additional stormwater controls due to the projects proximity to wetland resource area, the project has been designed as if it were new construction and has met the all of the Stormwater Management Standards.

<u>Standard 8 – Construction Period Pollutions Prevention and Erosion and Sedimentation</u> <u>Control</u>

Erosion controls barriers will be placed at the limit of work prior to commencement of any construction activity. A Construction Operation and Maintenance Plan and Construction Pollution Prevention Plan have will be provided once the project is funded by DHCD.

Standard 9 – Operation and Maintenance Plan

A Long Term Source Control/Pollution Prevention Plan and Operation and Maintenance Plan will also be provided once the project is funded by DHCD.

Standard 10 – Prohibition of Illicit Discharges

No illicit discharges are anticipated on site. Measures to prevent illicit discharges will be included in the Long-Term Source Control/Pollution Prevention Plan.

APPENDIX A

Existing Conditions

2, 10, 25 and 100 year return storm Summaries



16064 PRE-DEVELOPMENT

Prepared by Microsoft HydroCAD® 10.00-19 s/n 02159 © 2016 HydroCAD Software Solutions LLC

Area Listing (selected nodes)

	Area (sq-ft)	CN	Description (subcatchment-numbers)
	37,457	49	50-75% Grass cover, Fair, HSG A (2E)
	40,652	39	>75% Grass cover, Good, HSG A (1E)
	311	96	Gravel surface, HSG A (1E)
	1,888	98	Paved parking, HSG A (1E)
	12,624	77	Wetlands (1E, 2E)
	21,019	30	Woods, Good, HSG A (1E, 2E)
	12,952	55	Woods, Good, HSG B (1E, 2E)
980 1	126,903	47	TOTAL AREA

16064 PRE-DEVELOPMENT	Type III 24-hr	2-Year Rainfall=3.22"
Prepared by Microsoft		Printed 4/21/2017
HydroCAD® 10.00-19 s/n 02159 © 2016 HydroCAD Software Solutions	LLC	Page 3

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: TRIB. TO #31 WEST S	F Runoff Area=53,197 sf 3.55% Impervious Runoff Depth=0.00" Flow Length=432' Tc=7.6 min CN=40 Runoff=0.00 cfs 14 cf
Subcatchment 2E: TRIB. TO HOPPING	Runoff Area=73,706 sf 0.00% Impervious Runoff Depth=0.18" Flow Length=415' Tc=10.5 min CN=52 Runoff=0.09 cfs 1,093 cf

Total Runoff Area = 126,903 sf Runoff Volume = 1,107 cf Average Runoff Depth = 0.10" 98.51% Pervious = 125,015 sf 1.49% Impervious = 1,888 sf

Page 4

Runoff = 0.00 cfs @ 23.90 hrs, Volume=	14 cf,	Depth=	0.00"
--	--------	--------	-------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.22"

	A	rea (sf)	CN	Description	ř.		
×		1,888	98	Paved park	king, HSG A		
		40,652	39	>75% Gras	s cover, Go	bod, HSG A	
		311	96	Gravel surf	ace, HSG A	A	
		9,303	30	Woods, Go	od, HSG A		
		584	55	Woods, Go	od, HSG B		
*		459	77	Wetlands			
0		53,197	40	Weighted A	verage		
		51,309		96.45% Pe	rvious Area		
		1,888		3.55% Imp	ervious Are	a	
	Тс	Length	Slope	e Velocity	Capacity	Description	
_	(min)	(teet)	(π/π) (ft/sec)	(CTS)		
	5.5	50	0.0500	0.15		Sheet Flow,	
	723 B.	12/12/13		20 - 120 Marine		Grass: Dense n= 0.240 P2= 3.40"	
	2.1	382	0.0340	0 2.97		Shallow Concentrated Flow,	
				-		Unpaved Kv= 16.1 fps	
	7.6	432	Total				

Subcatchment 1E: TRIB. TO #31 WEST ST



Summary for Subcatchment 2E: TRIB. TO HOPPING BROOK

Page 5

Runoff	=	0.09 cfs @	12.48 hrs, Volume=	1,093 cf, Depth= 0.18"
--------	---	------------	--------------------	------------------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.22"

	Area (sf)	CN	Description		
	37,457	49	50-75% Gra	ass cover, l	Fair, HSG A
	11,716	30	Woods, Go	od, HSG A	100 Metri Madeur Materia Astania (2010)
	12,368	55	Woods, Go	od, HSG B	
*	12,165	77	Wetlands		
	73,706 73,706	52	Weighted A 100.00% Pe	verage ervious Are	a
۲ miı)	c Length n) (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description
4	.5 20	0.0360	0.07		Sheet Flow,
4.	.2 30	0.0360	0 0.12		Woods: Light underbrush n= 0.400 P2= 3.40" Sheet Flow, Grass: Dense n= 0.240 P2= 3.40"
1.	.8 365	0.0420	3.30		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
10	5 415	Total			

Subcatchment 2E: TRIB. TO HOPPING BROOK



Hydrograph

16064 PRE-DEVELOPMENTType III 24-hr10-Year Rainfall=4.86"Prepared by MicrosoftPrinted 4/21/2017HydroCAD® 10.00-19 s/n 02159 © 2016 HydroCAD Software Solutions LLCPage 6

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: TRIB. TO #31 WEST ST Flow Length=432' Tc=7.6 min CN=40 Runoff Depth=0.21"

Subcatchment 2E: TRIB. TO HOPPING

Runoff Area=73,706 sf 0.00% Impervious Runoff Depth=0.74" Flow Length=415' Tc=10.5 min CN=52 Runoff=0.84 cfs 4,556 cf

Total Runoff Area = 126,903 sf Runoff Volume = 5,466 cf Average Runoff Depth = 0.52" 98.51% Pervious = 125,015 sf 1.49% Impervious = 1,888 sf

Printed 4/21/2017 Page 7

Summary for Subcatchment 1E: TRIB. TO #31 WEST ST

Runoff	=	0.05 cfs @	12.49 hrs,	Volume=	910 cf,	Depth= 0.21"	
--------	---	------------	------------	---------	---------	--------------	--

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	A	rea (sf)	CN	Description			
		1,888	98	Paved park	ing, HSG A		
		40,652	39	>75% Gras	s cover, Go	bod, HSG A	
		311	96	Gravel surf	ace, HSG A		
		9,303	30	Woods, Go	od, HSG A		
		584	55	Woods, Go	od, HSG B		
*		459	77	Wetlands			
		53,197	40	Weighted A	verage		
		51,309		96.45% Pe	rvious Area		
		1,888		3.55% Impe	ervious Are	a	
	Тс	Length	Slope	e Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)		
	5.5	50	0.0500	0.15		Sheet Flow,	
						Grass: Dense n= 0.240 P2= 3.40"	
	2.1	382	0.0340) 2.97		Shallow Concentrated Flow,	
			1		-	Unpaved Kv= 16.1 fps	
4.32	76	132	Total				

1.6 lotal

Subcatchment 1E: TRIB. TO #31 WEST ST



Summary for Subcatchment 2E: TRIB. TO HOPPING BROOK

Runoff	=	0.84 cfs @	12.20 hrs,	Volume=	4,556 cf,	Depth= 0.74"	
--------	---	------------	------------	---------	-----------	--------------	--

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	Area (sf)	CN	Description		
	37,457	49	50-75% Gra	ass cover, l	Fair, HSG A
	11,716	30	Woods, Go	od, HSG A	
	12,368	55	Woods, Go	od, HSG B	
*	12,165	77	Wetlands		
	73,706 52 73,706		Weighted A 100.00% Pe	verage ervious Are	a
- (mi	Гс Length n) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description
4	.5 20	0.036	0 0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.40"
4	.2 30	0.036	0 0.12		Sheet Flow, Grass: Dense, n= 0.240, P2= 3.40"
1	.8 365	0.042	0 3.30		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
10	.5 415	Total			

Subcatchment 2E: TRIB. TO HOPPING BROOK



Hydrograph

Type III 24-hr 25-Year Rainfall=6.15" **16064 PRE-DEVELOPMENT** Prepared by Microsoft HydroCAD® 10.00-19 s/n 02159 © 2016 HydroCAD Software Solutions LLC

Printed 4/21/2017 Page 9

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: TRIB. TO #31 WEST ST Runoff Area=53,197 sf 3.55% Impervious Runoff Depth=0.55" Flow Length=432' Tc=7.6 min CN=40 Runoff=0.30 cfs 2,424 cf

Subcatchment 2E: TRIB. TO HOPPING

Runoff Area=73,706 sf 0.00% Impervious Runoff Depth=1.37" Flow Length=415' Tc=10.5 min CN=52 Runoff=1.95 cfs 8,406 cf

Total Runoff Area = 126,903 sf Runoff Volume = 10,830 cf Average Runoff Depth = 1.02" 98.51% Pervious = 125,015 sf 1.49% Impervious = 1,888 sf

Summary for Subcatchment 1E: TRIB. TO #31 WEST ST

Runoff = 0.30 cfs @ 12.33 hrs, Volume=	2,424 cf, Depth= 0.55"
--	------------------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.15"

	A	rea (sf)	CN	Description	8		
		1,888	98	Paved park	ing, HSG A		
		40,652	39	>75% Gras	s cover, Go	bod, HSG A	
		311	96	Gravel surf	ace, HSG A		
		9,303	30	Woods, Go	od, HSG A		
		584	55	Woods, Go	od, HSG B		
*		459	77	Wetlands	ADDRESS IN MARKET CONTRACT		
0		53,197	40	Weighted A	verage		
51,309 96.45% Pervious Area							
		1,888		3.55% Impe	ervious Are	a	
	Тс	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	5.5	50	0.0500	0.15		Sheet Flow,	
						Grass: Dense n= 0.240 P2= 3.40"	
	2.1	382	0.0340	2.97		Shallow Concentrated Flow,	
_	an officer					Unpaved Kv= 16.1 fps	
	7.6	432	Total				

Subcatchment 1E: TRIB. TO #31 WEST ST



Summary for Subcatchment 2E: TRIB. TO HOPPING BROOK

Runoff	=	1.95 cfs @	12.17 hrs,	Volume=	8,406 cf, D)epth= 1.37"
--------	---	------------	------------	---------	-------------	--------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.15"

	Area (sf)	CN	Description							
	37,457	49	50-75% Grass cover, Fair, HSG A							
	11,716	30	Woods, Good, HSG A							
	12,368	55	Woods, Good, HSG B							
*	12,165	77	Wetlands							
	73,706 73,706	52	Weighted A 100.00% Pe	verage ervious Are	a					
٦ mi)	rc Length n) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description					
4	.5 20	0.036	0 0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.40"					
4	.2 30	0.036	0 0.12		Sheet Flow, Grass: Dense, n= 0.240, P2= 3.40"					
1	.8 365	0.042	0 3.30		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps					
10	.5 415	Total	6							

Subcatchment 2E: TRIB. TO HOPPING BROOK



Hydrograph

16064 PRE-DEVELOPMENTType III 24-hr100-Year Rainfall=8.80"Prepared by MicrosoftPrinted 4/21/2017HydroCAD® 10.00-19 s/n 02159© 2016 HydroCAD Software Solutions LLCPage 12

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1E: TRIB. TO #31 WEST ST Runoff Area=53,197 sf 3.55% Impervious Runoff Depth=1.62" Flow Length=432' Tc=7.6 min CN=40 Runoff=1.64 cfs 7,170 cf

Subcatchment 2E: TRIB. TO HOPPING

Runoff Area=73,706 sf 0.00% Impervious Runoff Depth=2.99" Flow Length=415' Tc=10.5 min CN=52 Runoff=4.81 cfs 18,351 cf

Total Runoff Area = 126,903 sf Runoff Volume = 25,521 cf Average Runoff Depth = 2.41" 98.51% Pervious = 125,015 sf 1.49% Impervious = 1,888 sf

Summary for Subcatchment 1E: TRIB. TO #31 WEST ST

Runoff	=	1.64 cfs @	12.14 hrs, Volume=	7,170 cf, Depth= 1.62"
--------	---	------------	--------------------	------------------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.80"

_	A	rea (sf)	CN	Description				
		1,888	98	Paved park	ing, HSG A	N		
		40,652	39	>75% Gras	s cover, Go	bod, HSG A		
		311	96	Gravel surf	ace, HSG A	\mathbf{A}		
		9,303	30	Woods, Go	od, HSG A			
		584	55	Woods, Go	od, HSG B			
*		459	77	Wetlands				
-		53,197	40	Weighted A	verage			
		51,309		96.45% Pervious Area				
		1,888		3.55% Impe	ervious Are	a		
	Тс	Length	Slope	e Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
	5.5	50	0.0500	0.15		Sheet Flow,		
						Grass: Dense n= 0.240 P2= 3.40"		
	2.1	382	0.0340	2.97		Shallow Concentrated Flow,		
			0		3	Unpaved Kv= 16.1 fps		
	76	432	Total				1	

432 Total

Subcatchment 1E: TRIB. TO #31 WEST ST



Summary for Subcatchment 2E: TRIB. TO HOPPING BROOK

Runoff =	4.81 cfs @	12.16 hrs,	Volume=	18,351 cf,	Depth= 2.99"	
----------	------------	------------	---------	------------	--------------	--

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.80"

	Ar	rea (sf)	CN	Description							
17	4	37,457	49	50-75% Grass cover, Fair, HSG A							
		11,716	30	Woods, Good, HSG A							
		12,368	55	Woods, Good, HSG B							
*		12,165	77	Wetlands							
		73,706 73,706	52	Weighted A 100.00% Pe	verage ervious Are	a					
(m	Tc nin)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description					
	4.5	20	0.0360	0.07		Sheet Flow,					
ļ	4.2	30	0.0360	0.12		Woods: Light underbrush n= 0.400 P2= 3.40" Sheet Flow,					
1	1.8	365	0.0420	3.30		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps					
1	0.5	415	Total		1,						

Subcatchment 2E: TRIB. TO HOPPING BROOK



Hydrograph

APPENDIX B

Proposed Conditions

2, 10, 25 and 100 year return storm Summaries



16064 POST-DEVELOPMENT

Prepared by Microsoft HydroCAD® 10.00-19 s/n 02159 © 2016 HydroCAD Software Solutions LLC

Area Listing (selected nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
14,662	49	50-75% Grass cover, Fair, HSG A (6S)
19,228	39	>75% Grass cover, Good, HSG A (2P, 6S, 7S)
188	72	Dirt roads, HSG A (7S)
46,983	98	Paved parking, HSG A (2P)
8,622	98	Roofs, HSG A (1P)
12,624	77	Wetlands (6S, 7S)
11,644	30	Woods, Good, HSG A (2P, 6S, 7S)
12,952	55	Woods, Good, HSG B (6S, 7S)
126,903	71	TOTAL AREA

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1P: ROOFS (BLD 1-3)	Runoff Area=8,622 sf 100.00% Impervious Runoff Depth=2.99" Tc=10.0 min CN=98 Runoff=0.54 cfs 2,146 cf
Subcatchment 2P: PARKING & BLD 4	Runoff Area=60,825 sf 77.24% Impervious Runoff Depth=1.70" Tc=10.0 min CN=84 Runoff=2.40 cfs 8,612 cf
Subcatchment 6S: TRIB. TO HOPPING	Runoff Area=48,453 sf 0.00% Impervious Runoff Depth=0.23" Flow Length=192' Tc=11.0 min CN=54 Runoff=0.09 cfs 925 cf
Subcatchment 7S: TRIB TO #31 WEST ST	Runoff Area=9,003 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=158' Tc=10.0 min CN=40 Runoff=0.00 cfs 2 cf
Pond 4P: LARGE INFILTRATION SYSTEM	Peak Elev=203.14' Storage=2,548 cf Inflow=2.40 cfs 8,612 cf Outflow=0.45 cfs 8,612 cf
Pond 5P: ROOF INFILTRATION SYSTEM	Peak Elev=203.39' Storage=666 cf Inflow=0.54 cfs 2,146 cf Outflow=0.08 cfs 2,146 cf
	C. D

Total Runoff Area = 126,903 sf Runoff Volume = 11,686 cf Average Runoff Depth = 1.11" 56.18% Pervious = 71,298 sf 43.82% Impervious = 55,605 sf

Summary for Subcatchment 1P: ROOFS (BLD 1-3)



Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.22"



Summary for Subcatchment 2P: PARKING & BLD 4 ROOF

Runoff = 2.40 cfs @ 12.15 hrs, Volume= 8,612 cf, De	pth= 1.70"
---	------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.22"

A	rea (sf)	CN	Description			
	46,983	98	Paved park	ing, HSG A		
	12,866	39	>75% Gras	s cover, Go	ood, HSG A	
	976	30	Woods, Go	od, HSG A		
	60,825	84	Weighted A	verage		
	13,842 22.76% Pervious Area					
	46,983 77.24% Impervious Area				ea	
Tc (min)	Length (feet)	Slope (ft/ft	Velocity (ft/sec)	Capacity (cfs)	Description	
10.0					Direct Entry,	

Subcatchment 2P: PARKING & BLD 4 ROOF



Summary for Subcatchment 6S: TRIB. TO HOPPING BROOK

		이번 아이에 가지 않는 것이 같아.	037231 - 2022324 - 23	1999 - 20	1	NEN 107 (24 (24 2019)
Runoff	=	0.09 cfs @	12.43 hrs,	Volume=	925 cf,	Depth= 0.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.22"

<i></i>	A	rea (sf)	CN	Description			
		14,662	49	50-75% Gra	ass cover, l	Fair, HSG A	
		8,056	30	Woods, Go	od, HSG A		
		12,496	55	Woods, Go	od, HSG B		
*		12,239	77	Wetlands	and and the set		
		1,000	39	>75% Grass cover, Good, HSG A			
		48,453 48,453	54 Weighted Average 100.00% Pervious Are		verage ervious Are	a	
	Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description	_
	10.5	50	0.0100	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.40"	
	0.5	142	0.0900	4.83		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
	11.0	192	Total				

Subcatchment 6S: TRIB. TO HOPPING BROOK



Hydrograph

Summary for Subcatchment 7S: TRIB TO #31 WEST ST

Runoff	=	0.00 cfs @	23.92 hrs,	Volume=	2 cf,	Depth=	0.00"
						1	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.22"

	A	rea (sf)	CN	Description					
		5,362	39	>75% Gras	5% Grass cover, Good, HSG A				
		188	72	Dirt roads, I	HSG A				
		2,612	30	Woods, Go	od, HSG A				
		456	55	Woods, Go	od, HSG B				
*		385	77	Wetlands					
		9,003	40	Weighted A	verage				
		9,003		100.00% Pe	ervious Are	а			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cts)		_		
	5.5	50	0.0500	0.15		Sheet Flow,			
						Grass: Dense n= 0.240 P2= 3.40"			
	0.6	108	0.0370	3.10		Shallow Concentrated Flow,			
						Unpaved Kv= 16.1 fps			
_	3.9					Direct Entry,	_		
	10.0	158	Total						

Subcatchment 7S: TRIB TO #31 WEST ST



Summary for Pond 4P: LARGE INFILTRATION SYSTEM

Inflow Area	a =	60,825 sf,	77.24% Imperviou	s, Inflow Depth = 1.70" for 2-Year event
Inflow	=	2.40 cfs @	12.15 hrs, Volume	= 8,612 cf
Outflow	=	0.45 cfs @	12.68 hrs, Volume	= 8,612 cf, Atten= 81%, Lag= 32.0 min
Discarded	=	0.45 cfs @	12.68 hrs, Volume	= 8,612 cf

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 203.14' @ 12.68 hrs Surf.Area= 7,849 sf Storage= 2,548 cf

Plug-Flow detention time= 39.4 min calculated for 8,603 cf (100% of inflow) Center-of-Mass det. time= 39.4 min (872.4 - 833.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	202.50'	6,485 cf	49.83'W x 157.50'L x 3.54'H Field A
			27,798 cf Overall - 11,586 cf Embedded = 16,211 cf x 40.0% Voids
#2A	203.00'	11,586 cf	Cultec R-330XLHD x 220 Inside #1
1121 \			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 10 rows
		18,071 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	

Discarded OutFlow Max=0.45 cfs @ 12.68 hrs HW=203.14' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.45 cfs)

Pond 4P: LARGE INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= $+1.50' \times 7.45$ sf x 10 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

22 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 155.50' Row Length +12.0" End Stone x 2 = 157.50' Base Length 10 Rows x 52.0" Wide + 6.0" Spacing x 9 + 12.0" Side Stone x 2 = 49.83' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

220 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 11,586.3 cf Chamber Storage

27,797.7 cf Field - 11,586.3 cf Chambers = 16,211.4 cf Stone x 40.0% Voids = 6,484.5 cf Stone Storage

Chamber Storage + Stone Storage = 18,070.8 cf = 0.415 af Overall Storage Efficiency = 65.0% Overall System Size = 157.50' x 49.83' x 3.54'

220 Chambers 1,029.5 cy Field 600.4 cy Stone



Pond 4P: LARGE INFILTRATION SYSTEM



1

Summary for Pond 5P: ROOF INFILTRATION SYSTEM

Inflow Area	a =	8,622 sf	,100.00% Impervious,	Inflow Depth = 2.99" for 2-Year event
Inflow	=	0.54 cfs @	12.14 hrs, Volume=	2,146 cf
Outflow	=	0.08 cfs @	12.72 hrs, Volume=	2,146 cf, Atten= 85%, Lag= 35.1 min
Discarded	=	0.08 cfs @	12.72 hrs, Volume=	2,146 cf

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 203.39' @ 12.72 hrs Surf.Area= 1,265 sf Storage= 666 cf

Plug-Flow detention time= 55.8 min calculated for 2,144 cf (100% of inflow) Center-of-Mass det. time= 55.8 min (815.7 - 760.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	202.50'	1,089 cf	40.17'W x 31.50'L x 3.54'H Field A 4,481 cf Overall - 1,758 cf Embedded = 2,723 cf x 40.0% Voids
#2A	203.00'	1,758 cf	Cultec R-330XLHD x 32 Inside #1 Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 8 rows
		2.847 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.08 cf	s @ 12.72 hrs HW=203.39' (Free Discharge)	

-1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond 5P: ROOF INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= $+1.50' \times 7.45$ sf x 8 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 8 Rows x 52.0" Wide + 6.0" Spacing x 7 + 12.0" Side Stone x 2 = 40.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

32 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 8 Rows = 1,758.4 cf Chamber Storage

4,481.1 cf Field - 1,758.4 cf Chambers = 2,722.7 cf Stone x 40.0% Voids = 1,089.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,847.5 cf = 0.065 afOverall Storage Efficiency = 63.5%Overall System Size = $31.50' \times 40.17' \times 3.54'$

32 Chambers 166.0 cy Field 100.8 cy Stone





Pond 5P: ROOF INFILTRATION SYSTEM



Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1P: ROOFS (BLD 1-3)	Runoff Area=8,622 sf 100.00% Impervious Runoff Depth=4.62" Tc=10.0 min CN=98 Runoff=0.81 cfs 3,322 cf
Subcatchment 2P: PARKING & BLD 4	Runoff Area=60,825 sf 77.24% Impervious Runoff Depth=3.14" Tc=10.0 min CN=84 Runoff=4.42 cfs 15,929 cf
Subcatchment 6S: TRIB. TO HOPPING	Runoff Area=48,453 sf 0.00% Impervious Runoff Depth=0.85" Flow Length=192' Tc=11.0 min CN=54 Runoff=0.69 cfs 3,445 cf
Subcatchment 7S: TRIB TO #31 WEST S	T Runoff Area=9,003 sf 0.00% Impervious Runoff Depth=0.21" Flow Length=158' Tc=10.0 min CN=40 Runoff=0.01 cfs 154 cf
Pond 4P: LARGE INFILTRATION SYSTEM	VI Peak Elev=203.68' Storage=6,145 cf Inflow=4.42 cfs 15,929 cf Outflow=0.47 cfs 15,929 cf
Pond 5P: ROOF INFILTRATION SYSTEM	Peak Elev=203.90' Storage=1,198 cf Inflow=0.81 cfs 3,322 cf Outflow=0.08 cfs 3,322 cf
Total Runoff Area = 126.903	sf Runoff Volume = 22,850 cf Average Runoff Depth = 2,16"

Total Runoff Area = 126,903 sf Runoff Volume = 22,850 cf Average Runoff Depth = 2.16" 56.18% Pervious = 71,298 sf 43.82% Impervious = 55,605 sf


Summary for Subcatchment 2P: PARKING & BLD 4 ROOF

Runoff	=	4.42 cfs @	12.14 hrs,	Volume=	15,929 cf,	Depth= 3.14"	
--------	---	------------	------------	---------	------------	--------------	--

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

Area	a (sf)	CN I	Description			
46	6,983	98	Paved park	ing, HSG A		
12	2,866	39 :	>75% Gras	s cover, Go	ood, HSG A	
	976	30	Noods, Go	od, HSG A		
60),825	84 \	Neighted A	verage		
13	3,842	:	22.76% Per	vious Area		
46	5,983		77.24% lmp	pervious Are	ea	
Tc L (min)	ength. (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
10.0					Direct Entry,	

Subcatchment 2P: PARKING & BLD 4 ROOF



Summary for Subcatchment 6S: TRIB. TO HOPPING BROOK

Runoff	=	0.69 cfs @	12.20 hrs,	Volume=	3,445 cf,	Depth= 0.85"	
--------	---	------------	------------	---------	-----------	--------------	--

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	A	rea (sf)	CN	Description		
-		14,662	49	50-75% Gra	ass cover, I	Fair, HSG A
		8,056	30	Woods, Go	od, HSG A	
		12,496	55	Woods, Go	od, HSG B	
*		12,239	77	Wetlands		
		1,000	39	>75% Gras	s cover, Go	bod, HSG A
_		48,453	54	Weighted A	verage	
		48,453		100.00% P	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description
	10.5	50	0.0100	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.40"
	0.5	142	0.0900	4.83		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1	11.0	192	Total			

Subcatchment 6S: TRIB. TO HOPPING BROOK



Summary for Subcatchment 7S: TRIB TO #31 WEST ST

Runoff	=	0.01 cfs @	12.53 hrs,	Volume=	154 cf, E)epth= 0.21"	
--------	---	------------	------------	---------	-----------	--------------	--

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.86"

	A	rea (sf)	CN	Description		
8. <u> </u>		5,362	39	>75% Gras	s cover, Go	bod, HSG A
		188	72	Dirt roads, I	HSG A	
		2,612	30	Woods, Go	od, HSG A	
		456	55	Woods, Go	od, HSG B	
*		385	77	Wetlands		
		9.003	40	Weighted A	verage	
		9,003		100.00% Pe	ervious Are	a
	Tc (min)	Length	Slope	e Velocity	Capacity	Description
-	((((((((((((((((((((((((((((((((((((((((leet)	(1010) (IUSEC)	(015)	Object Flow
	5.5	50	0.0500	0.15		Grass: Dense n= 0.240 P2= 3.40"
	0.6	108	0.0370	3.10		Shallow Concentrated Flow,
_	3.9					Direct Entry,
	10.0	158	Total			

Subcatchment 7S: TRIB TO #31 WEST ST



Summary for Pond 4P: LARGE INFILTRATION SYSTEM

Inflow Area	a =	60,825 sf	, 77.24% Impervious	Inflow Depth = 3.14"	for 10-Year event
Inflow	=	4.42 cfs @	12.14 hrs, Volume=	15,929 cf	
Outflow	=	0.47 cfs @	13.10 hrs, Volume=	15,929 cf, Atte	en= 89%, Lag= 57.4 min
Discarded	=	0.47 cfs @	13.10 hrs, Volume=	15,929 cf	

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 203.68' @ 13.10 hrs Surf.Area= 7,849 sf Storage= 6,145 cf

Plug-Flow detention time= 110.6 min calculated for 15,913 cf (100% of inflow) Center-of-Mass det. time= 110.5 min (925.9 - 815.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	202.50'	6,485 cf	49.83'W x 157.50'L x 3.54'H Field A
		2	27,798 cf Overall - 11,586 cf Embedded = 16,211 cf x 40.0% Voids
#2A	203.00'	11,586 cf	Cultec R-330XLHD x 220 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 10 rows
111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 111 - 11		18,071 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.47 cf	s @ 13.10 hrs HW=203.68' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.47 cfs)

Pond 4P: LARGE INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 10 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

22 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 155.50' Row Length +12.0" End Stone x 2 = 157.50' Base Length 10 Rows x 52.0" Wide + 6.0" Spacing x 9 + 12.0" Side Stone x 2 = 49.83' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

220 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 11,586.3 cf Chamber Storage

27,797.7 cf Field - 11,586.3 cf Chambers = 16,211.4 cf Stone x 40.0% Voids = 6,484.5 cf Stone Storage

Chamber Storage + Stone Storage = 18,070.8 cf = 0.415 af Overall Storage Efficiency = 65.0% Overall System Size = 157.50' x 49.83' x 3.54'

220 Chambers 1,029.5 cy Field 600.4 cy Stone



Pond 4P: LARGE INFILTRATION SYSTEM



Summary for Pond 5P: ROOF INFILTRATION SYSTEM

Inflow Area	a =	8,622 sf.	100.00% Impervious,	Inflow Depth = 4.6	62" for 10-Year event
Inflow	-	0.81 cfs @	12.14 hrs, Volume=	3,322 cf	
Outflow		0.08 cfs @	13.03 hrs, Volume=	3,322 cf, A	Atten= 90%, Lag= 53.6 min
Discarded	=	0.08 cfs @	13.03 hrs, Volume=	3,322 cf	

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 203.90' @ 13.03 hrs Surf.Area= 1,265 sf Storage= 1,198 cf

Plug-Flow detention time= 107.6 min calculated for 3,318 cf (100% of inflow) Center-of-Mass det. time= 107.4 min (859.6 - 752.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	202.50'	1,089 cf	40.17'W x 31.50'L x 3.54'H Field A 4,481 cf Overall - 1,758 cf Embedded = 2,723 cf x 40.0% Voids
#2A	203.00'	1,758 cf	Cultec R-330XLHD x 32 Inside #1 Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 8 rows
		2,847 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow M	Max=0.08 cf	s @ 13.03 hrs HW=203.90' (Free Discharge)	

-1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond 5P: ROOF INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= $+1.50' \times 7.45$ sf x 8 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 8 Rows x 52.0" Wide + 6.0" Spacing x 7 + 12.0" Side Stone x 2 = 40.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

32 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 8 Rows = 1,758.4 cf Chamber Storage

4,481.1 cf Field - 1,758.4 cf Chambers = 2,722.7 cf Stone x 40.0% Voids = 1,089.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,847.5 cf = 0.065 afOverall Storage Efficiency = 63.5%Overall System Size = $31.50' \times 40.17' \times 3.54'$

32 Chambers 166.0 cy Field 100.8 cy Stone





Pond 5P: ROOF INFILTRATION SYSTEM



Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1P: ROOFS (BLD 1-3)	Runoff Area=8,622 sf 100.00% Impervious Runoff Depth=5.91" Tc=10.0 min CN=98 Runoff=1.03 cfs 4,248 cf
Subcatchment 2P: PARKING & BLD 4	Runoff Area=60,825 sf 77.24% Impervious Runoff Depth=4.34" Tc=10.0 min CN=84 Runoff=6.03 cfs 21,984 cf
Subcatchment 6S: TRIB. TO HOPPING	Runoff Area=48,453 sf 0.00% Impervious Runoff Depth=1.52" Flow Length=192' Tc=11.0 min CN=54 Runoff=1.46 cfs 6,157 cf
Subcatchment 7S: TRIB TO #31 WEST S	T Runoff Area=9,003 sf 0.00% Impervious Runoff Depth=0.55" Flow Length=158' Tc=10.0 min CN=40 Runoff=0.05 cfs 410 cf
Pond 4P: LARGE INFILTRATION SYSTEM	Peak Elev=204.19' Storage=9,476 cf Inflow=6.03 cfs 21,984 cf Outflow=0.48 cfs 21,984 cf
Pond 5P: ROOF INFILTRATION SYSTEM	Peak Elev=204.37' Storage=1,667 cf Inflow=1.03 cfs 4,248 cf Outflow=0.09 cfs 4,248 cf
Total Dun off Area = 126 002	of Bunoff Volume = 22 798 of Average Bunoff Depth = 3 10"

Total Runoff Area = 126,903 sf Runoff Volume = 32,798 cf Average Runoff Depth = 3.10" 56.18% Pervious = 71,298 sf 43.82% Impervious = 55,605 sf



Summary for Subcatchment 2P: PARKING & BLD 4 ROOF

Runoff = 6.03 cfs @ 12.14 hrs, Volume= 21,984 cf, Depth= 4.3	Depth= 4.34"
--	--------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.15"

A	rea (sf)	CN	Description				
	46,983	98	Paved park	Paved parking, HSG A			
	12,866	39	>75% Gras	>75% Grass cover, Good, HSG A			
	976	30	Woods, Go	od, HSG A			
	60,825	84	Weighted A	verage			
	13,842	2 22.76% Pervious Area					
	46,983		77.24% Imp	pervious Are	ea		
Те	Longth	Clane	Volocity	Consoitu	Description		
(min)	Length	Siope		Capacity	Description		
(min)	(reet)	(IVIL) (IUSec)	(CIS)			
10.0					Direct Entry,		

Subcatchment 2P: PARKING & BLD 4 ROOF



Summary for Subcatchment 6S: TRIB. TO HOPPING BROOK

Runoff = 1.46 cfs @ 12.17 hrs, Volume= 6,157 cf, Dep	= 1.5	52"
--	-------	-----

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.15"

	A	rea (sf)	CN	Description						
_		14,662	49	50-75% Gra)-75% Grass cover, Fair, HSG A					
		8,056	30	Woods, Go	oods, Good, HSG A					
		12,496	55	Woods, Good, HSG B						
*		12,239	77	Wetlands						
		1,000	39	>75% Gras	s cover, Go	bod, HSG A				
48,45354Weighted Average48,453100.00% Pervious Area				а						
	Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description				
	10.5	50	0.0100	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.40"				
	0.5	142	0.0900	0 4.83		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
_	11.0	192	Total							

Subcatchment 6S: TRIB. TO HOPPING BROOK



Summary for Subcatchment 7S: TRIB TO #31 WEST ST

Dumoff		O OF of a	10 27 hrs	Volumon	410 of Donth- 0 55"
Runon	-	0.05 crs @	12.37 hrs,	volume-	410 cl, Deptil- 0.55

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.15"

	A	rea (sf)	CN	Description			_			
2		5,362	39	>75% Grass cover, Good, HSG A						
		188	72	Dirt roads, I	rt roads, HSG A					
		2,612	30	Woods, Good, HSG A						
		456	55	Woods, Go	od, HSG B					
*		385	77	Wetlands						
		9.003 40 Weighted Average								
		9,003		100.00% Pe	a					
	Tc (min)	Length	Slope	e Velocity	Capacity (cfs)	Description				
-	55	50	0.0500	0 15	(010)	Sheet Flow	_			
	5.5	50	0.0000	0.15		Grass: Dense $n=0.240$ P2= 3.40"				
	0.6	108	0.0370	3.10		Shallow Concentrated Flow, Unpaved Ky= 16.1 fps				
	3.9					Direct Entry,				
	10.0	158	Total		-					

Subcatchment 7S: TRIB TO #31 WEST ST



Hydrograph

Summary for Pond 4P: LARGE INFILTRATION SYSTEM

Inflow Area	a =	60,825 sf,	77.24% Impervious,	Inflow Depth = 4.34" for 25-Year event
Inflow	=	6.03 cfs @	12.14 hrs, Volume=	21,984 cf
Outflow	=	0.48 cfs @	13.67 hrs, Volume=	21,984 cf, Atten= 92%, Lag= 92.0 min
Discarded	=	0.48 cfs @	13.67 hrs, Volume=	21,984 cf

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 204.19' @ 13.67 hrs Surf.Area= 7,849 sf Storage= 9,476 cf

Plug-Flow detention time= 177.6 min calculated for 21,961 cf (100% of inflow) Center-of-Mass det. time= 177.4 min (983.7 - 806.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	202.50'	6,485 cf	49.83'W x 157.50'L x 3.54'H Field A
			27,798 cf Overall - 11,586 cf Embedded = 16,211 cf x 40.0% Voids
#2A	203.00'	11,586 cf	Cultec R-330XLHD x 220 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
v			Row Length Adjustment= +1.50' x 7.45 sf x 10 rows
		18,071 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	
Discaro		Max=0.48 cf	e @ 13.67 brs. HW=204.19' (Free Discharge)	

Discarded OutFlow Max=0.48 cfs @ 13.67 hrs HW=204.19' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.48 cfs)

Pond 4P: LARGE INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= $+1.50' \times 7.45$ sf x 10 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

22 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 155.50' Row Length +12.0" End Stone x 2 = 157.50' Base Length 10 Rows x 52.0" Wide + 6.0" Spacing x 9 + 12.0" Side Stone x 2 = 49.83' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

220 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 11,586.3 cf Chamber Storage

27,797.7 cf Field - 11,586.3 cf Chambers = 16,211.4 cf Stone x 40.0% Voids = 6,484.5 cf Stone Storage

Chamber Storage + Stone Storage = 18,070.8 cf = 0.415 af Overall Storage Efficiency = 65.0% Overall System Size = 157.50' x 49.83' x 3.54'

220 Chambers 1,029.5 cy Field 600.4 cy Stone



Pond 4P: LARGE INFILTRATION SYSTEM



Summary for Pond 5P: ROOF INFILTRATION SYSTEM

Inflow Area	a =	8,622 sf	,100.00% Impervious,	Inflow Depth = 5.91"	for 25-Year event
Inflow	=	1.03 cfs @	12.14 hrs, Volume=	4,248 cf	
Outflow	=	0.09 cfs @	13.30 hrs, Volume=	4,248 cf, Atte	n= 92%, Lag= 69.7 min
Discarded	=	0.09 cfs @	13.30 hrs, Volume=	4,248 cf	

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 204.37' @ 13.30 hrs Surf.Area= 1,265 sf Storage= 1,667 cf

Plug-Flow detention time= 153.5 min calculated for 4,243 cf (100% of inflow) Center-of-Mass det. time= 153.3 min (901.8 - 748.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	202.50'	1,089 cf	40.17'W x 31.50'L x 3.54'H Field A 4,481 cf Overall - 1,758 cf Embedded = 2,723 cf x 40.0% Voids
#2A	203.00'	1,758 cf	Cultec R-330XLHD x 32 Inside #1 Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 8 rows
		2,847 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	
Discard		Max=0.09 cf	@ 13 30 brs HW=204 37' (Free Discharge)	

Discarded OutFlow Max=0.09 cfs @ 13.30 hrs HW=204.37 (Free Discharge)

Pond 5P: ROOF INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= $47.8''W \times 30.0''H \Rightarrow 7.45 \text{ sf } \times 7.00'L = 52.2 \text{ cf}$ Overall Size= $52.0''W \times 30.5''H \times 8.50'L$ with 1.50' Overlap Row Length Adjustment= $+1.50' \times 7.45 \text{ sf } \times 8 \text{ rows}$

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 8 Rows x 52.0" Wide + 6.0" Spacing x 7 + 12.0" Side Stone x 2 = 40.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

32 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 8 Rows = 1,758.4 cf Chamber Storage

4,481.1 cf Field - 1,758.4 cf Chambers = 2,722.7 cf Stone x 40.0% Voids = 1,089.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,847.5 cf = 0.065 afOverall Storage Efficiency = 63.5%Overall System Size = $31.50' \times 40.17' \times 3.54'$

32 Chambers 166.0 cy Field 100.8 cy Stone





Pond 5P: ROOF INFILTRATION SYSTEM



Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1P: ROOFS (BLD 1-3)	Runoff Area=8,622 sf 100.00% Impervious Runoff Depth=8.56" Tc=10.0 min CN=98 Runoff=1.48 cfs 6,150 cf
Subcatchment 2P: PARKING & BLD 4	Runoff Area=60,825 sf 77.24% Impervious Runoff Depth=6.87" Tc=10.0 min CN=84 Runoff=9.36 cfs 34,801 cf
Subcatchment 6S: TRIB. TO HOPPING	Runoff Area=48,453 sf 0.00% Impervious Runoff Depth=3.22" Flow Length=192' Tc=11.0 min CN=54 Runoff=3.41 cfs 13,022 cf
Subcatchment 7S: TRIB TO #31 WEST S	ST Runoff Area=9,003 sf 0.00% Impervious Runoff Depth=1.62" Flow Length=158' Tc=10.0 min CN=40 Runoff=0.26 cfs 1,213 cf
Pond 4P: LARGE INFILTRATION SYSTE	M Peak Elev=205.84' Storage=17,432 cf Inflow=9.36 cfs 34,801 cf Outflow=0.52 cfs 34,801 cf
Pond 5P: ROOF INFILTRATION SYSTEM	Peak Elev=205.83' Storage=2,743 cf Inflow=1.48 cfs 6,150 cf Outflow=0.10 cfs 6,150 cf

Total Runoff Area = 126,903 sf Runoff Volume = 55,186 cf Average Runoff Depth = 5.22" 56.18% Pervious = 71,298 sf 43.82% Impervious = 55,605 sf

Summary for Subcatchment 1P: ROOFS (BLD 1-3)

Runoff = 1.48 cfs @ 12.14 hrs, Volume= 6,150 cf, Depth= 8.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.80"



Summary for Subcatchment 2P: PARKING & BLD 4 ROOF

Runoff =	9.36 cfs @	12.14 hrs.	Volume=	34,801 cf.	Depth= 6.87"	
----------	------------	------------	---------	------------	--------------	--

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.80"

A	rea (sf)	CN	Description			
	46,983	98	Paved park	ing, HSG A		
	12,866	39	>75% Gras	s cover, Go	ood, HSG A	
	976	30	Woods, Go	od, HSG A		
	60,825	84	Weighted A	verage		
	13,842 22.76% Pervious Area					
46,983 77.24% Impervious Are				pervious Ar	ea	
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description	
10.0			ia di Kalendari di K		Direct Entry,	

Subcatchment 2P: PARKING & BLD 4 ROOF



Summary for Subcatchment 6S: TRIB. TO HOPPING BROOK

Runoff = 3.41 cfs @ 12.16 hrs, Volume=	13,022 cf, Depth= 3.22"
--	-------------------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.80"

	A	rea (sf)	CN	Description			
		14,662	49	50-75% Gra	ass cover, F	Fair, HSG A	
		8,056	30	Woods, Go	od, HSG A		
		12,496	55	Woods, Go	od, HSG B		
* 12.239 77 Wetlands							
		1,000	39	>75% Gras	s cover, Go	bod, HSG A	_
		48,453 48,453	54	Weighted A 100.00% Pe	verage ervious Are	а	
	Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description	
	10.5	50	0.0100	0.08		Sheet Flow, Grass: Dense n= 0.240 P2= 3.40"	
	0.5	142	0.0900	4.83		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
2	11.0	192	Total	_			

Subcatchment 6S: TRIB. TO HOPPING BROOK



Hydrograph

16064 POST-DEVELOPMENT

Prepared by Microsoft HydroCAD® 10.00-19 s/n 02159 © 2016 HydroCAD Software Solutions LLC

Summary for Subcatchment 7S: TRIB TO #31 WEST ST

Runoff = 0.26 cfs @ 12.17 hrs, Volume=	1,213 cf, Depth= 1.62"
--	------------------------

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.80"

	A	rea (sf)	CN	Description		
		5,362	39	>75% Gras	s cover, Go	bod, HSG A
		188	72	Dirt roads, I	HSG A	
		2,612	30	Woods, Go	od, HSG A	
		456	55	Woods, Go	od, HSG B	
*		385	77	Wetlands	<i>17</i>	
		9,003	40	Weighted A	verage	
		9,003		100.00% Pe	ervious Are	a
	Tc (min)	Length	Slope	e Velocity	Capacity	Description
-	(min)	(leet)			(015)	Sheet Flow
	5.5	50	0.0500	0.15		Grass: Dense $n= 0.240$ P2= 3.40"
	0.6	108	0.0370	3.10		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	3.9					Direct Entry,
	10.0	158	Total			

Subcatchment 7S: TRIB TO #31 WEST ST



Hydrograph

Summary for Pond 4P: LARGE INFILTRATION SYSTEM

Page 41

Inflow Area	a =	60,825 sf,	77.24% Impervious,	Inflow Depth = 6	6.87" foi	r 100-Year event
Inflow	=	9.36 cfs @	12.14 hrs, Volume=	34,801 cf		
Outflow	=	0.52 cfs @	14.62 hrs, Volume=	34,801 cf,	Atten= 9	4%, Lag= 149.2 min
Discarded	=	0.52 cfs @	14.62 hrs, Volume=	34,801 cf		

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 205.84' @ 14.62 hrs Surf.Area= 7,849 sf Storage= 17,432 cf

Plug-Flow detention time= 322.8 min calculated for 34,764 cf (100% of inflow) Center-of-Mass det. time= 322.8 min (1,116.3 - 793.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	202.50'	6,485 cf	49.83'W x 157.50'L x 3.54'H Field A
#2A	203.00'	11,586 cf	Cultec R-330XLHD x 220 Inside #1 Effective Size= 47.8 ''W x 30.0''H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0''W x 30.5''H x 8.50'L with 1.50' Overlap Bow Length Adjustment= ± 1.50 ' x 7.45 sf x 10 rows
		18,071 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	
Discard		Max-0 52 of	@ 14.62 hrs HW-205.84' (Free Discharge)	

Discarded OutFlow Max=0.52 cfs @ 14.62 hrs HW=205.84' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.52 cfs)

Pond 4P: LARGE INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= $+1.50' \times 7.45$ sf x 10 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

22 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 155.50' Row Length +12.0" End Stone x 2 = 157.50' Base Length 10 Rows x 52.0" Wide + 6.0" Spacing x 9 + 12.0" Side Stone x 2 = 49.83' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

220 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 11,586.3 cf Chamber Storage

27,797.7 cf Field - 11,586.3 cf Chambers = 16,211.4 cf Stone x 40.0% Voids = 6,484.5 cf Stone Storage

Chamber Storage + Stone Storage = 18,070.8 cf = 0.415 af Overall Storage Efficiency = 65.0% Overall System Size = 157.50' x 49.83' x 3.54'

220 Chambers 1,029.5 cy Field 600.4 cy Stone



00000000000

Pond 4P: LARGE INFILTRATION SYSTEM



Summary for Pond 5P: ROOF INFILTRATION SYSTEM

Inflow Area	a =	8,622 sf	,100.00% Impervious,	Inflow Depth =	8.56"	for	100-Year event
Inflow	=	1.48 cfs @	12.14 hrs, Volume=	6,150 c	f		
Outflow	=	0.10 cfs @	13.89 hrs, Volume=	6,150 c	f, Atte	en= 93	%, Lag= 105.1 min
Discarded	=	0.10 cfs @	13.89 hrs, Volume=	6,150 c	f		NUM SANTA DUBUCH PROVIN

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs Peak Elev= 205.83' @ 13.89 hrs Surf.Area= 1,265 sf Storage= 2,743 cf

Plug-Flow detention time= 249.3 min calculated for 6,144 cf (100% of inflow) Center-of-Mass det. time= 249.3 min (993.0 - 743.8)

Volume	Invert	Avail.Storage	Storage Description			
#1A	202.50'	1,089 cf	40.17'W x 31.50'L x 3.54'H Field A			
			4,481 cf Overall - 1,758 cf Embedded = 2,723 cf x 40.0% Voids			
#2A	203.00'	1,758 cf	Cultec R-330XLHD x 32 Inside #1			
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf			
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap			
			Row Length Adjustment= +1.50' x 7.45 sf x 8 rows			
		2,847 cf	Total Available Storage			

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	202.50'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.10 cfs	s @ 13.89 hrs HW=205.83' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.10 cfs)

Pond 5P: ROOF INFILTRATION SYSTEM - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= $+1.50' \times 7.45$ sf x 8 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 8 Rows x 52.0" Wide + 6.0" Spacing x 7 + 12.0" Side Stone x 2 = 40.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

32 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 8 Rows = 1,758.4 cf Chamber Storage

4,481.1 cf Field - 1,758.4 cf Chambers = 2,722.7 cf Stone x 40.0% Voids = 1,089.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,847.5 cf = 0.065 afOverall Storage Efficiency = 63.5%Overall System Size = $31.50' \times 40.17' \times 3.54'$

32 Chambers 166.0 cy Field 100.8 cy Stone





16064 POST-DEVELOPMENT

Prepared by Microsoft HydroCAD® 10.00-19 s/n 02159 © 2016 HydroCAD Software Solutions LLC

Pond 5P: ROOF INFILTRATION SYSTEM



APPENDIX C

Additional Calculations:

- **1.** Soils Information (under separate cover)
- 2. Recharge Volumes Calculation
- 3. Water Quality Volume
- 4. TSS Removal Calculations
- 5. Separator Row sizing calculation
- 6. 72 Hour Drawdown Calculations for Infiltration Systems
- 7. Groundwater Mounding Calculation



Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — Norfolk and Suffolk Counties, Massachusetts (MA616)						
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI		
5	Saco silt loam, 0 to 3 percent slopes	B/D	1.3	34.4%		
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	A	2.5	65.6%		
Totals for Area of Inter	rest	3.8	100.0%			

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.


Hydrologic Soil Group—Norfolk and Suffolk Counties, Massachusetts (Glen Brook Way)



USDA

Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey 10/28/2016 Page 2 of 4

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
5	Saco silt loam, 0 to 3 percent slopes	B/D	1.1	32.5%
254B Merrimac fine sandy Ioam, 3 to 8 percent slopes		A	2.2	67.5%
Totals for Area of Inte	rest	3.3	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

ON-S	ITE	RE/	/IEW
------	-----	-----	------

ON-SITE	REVIEW		2020					
DEEP HOLE	E #: 16-01	DATE: 12/1	/16	TIME: 8:00am	1 WEATHER: Sunny 45*			
SITE ADDR	ESS or MAI	P/LOT #: Map 66,	Lot 1, West Str	eet, Medway MA	D NO - 46.064			
OWNER:	Summit Ho	me Builders Inc			B NU.: 16-064			
LOCATION	(identity on	Plan): See Attached Pla	an GRO	JUND ELEVATION	AT SURFACE OF HOLE: To be determined			
LAND USE:	Reside	ntial SURF	ACE STONES:	Yes: X No:	SLOPE (%): 2-4%			
VEGETATIC	N: Gravell	v- Field		LANDFORM:	Kame			
DISTANCES	FROM:	•	1000					
OPEN WAT	ER BODY:	300'+ ft PROPERTY	Y LINE: 40'	ft POSSIBLE WE	T AREA: 200 ft DRAINAGEWAY: 300 ft			
DRINKING V	WATER WE	ELL: - ft OTHE	ER:					
DEEP OBSE	RVATION	HOLE LOG						
Depth (inches)	Soil Hor./ Layer	Soil Texture (USDA)	Soil Color (Munsell)	Redoximorphic Features	Other (Structure, Consistency,% Gravels, Stones, Boulders			
0-12"	А	Loamy Sand (LS)	10yr3/3		Friable Roots (FR)			
12"-22"	в	Loamy Sand (LS)	10yr5/8	-	Friable Roots (FR)			
32"-84"	C1	Sand (S)	10yr5/4	64"	Med-Coarse Sand, Gravel 10% Stone			
84"-96"	C2	Sand (S)	10yr5/3	Ox. 10yr5/8	Very Fine to Fine Sand, Ledge 96"			
				Depl. 10yr6/2				
				Damp 84"+				
PARENT M	TERIAL:	Loamy Glacio Depostits(LGD)	Unsuitable Material	Present? Yes: X No: If Yes:			
Disturb	ed Soil:	Fill Mat'l:	mpervious Laye	r(s): We	eathered/Fractured Rock: Bedrock: X			
GROUNDW	ATER OBS	ERVED: Yes: X	No:	If Yes: What is the	e depth of Groundwater:			
Standing i	in Hole:	Weeping from	n Face:	Saturating the	he Face: 84" Mottling: 64"			
Estimated D	Pepth to Se	asonal High Ground Wat	er: 64"					
PERCOL	ATION TE	EST						
Percolation I	Hole #:			Percolation Hol	e #:			
Test Date:				Test Date:				
Depth of Per	rc:	<u></u>		Depth of Perc:				
Start of Pres	oak:			- Start of Presoal	k:			
End of Press	oak:			End of Presoak				
Time @ 12":				Time @ 12":	· · · · · · · · · · · · · · · · · · ·			
Time @ 9":				. Time @ 9":				
Time Elapse	::(12"-9")			Time Elapse:(1	2"-9")			
Time AT 6":				Time AT 6":	7			
Time Elapse	: (9"-6"):	<u>.</u>		Time Elapse: (9	9"-6"):			
Rate: (min/ir	n.):			Rate: (min/in.):				
Test Passed	/ Failed/	4		Test Passed/ F	ailed/ Discon/			
Discon/ Add	. rest ked t	.		Add. Testing Ri	ey u.			
Performed B Comments:	y: Thoma Drainag	s A Pozerski Witness ge Test Pits TH 16-01-05	sed By: <u>N/A</u>		Mach./Oper.: Trufant			

An indication that the "site passed" indicates only that the basic criteria for a soil evaluation and percolation test under Title 5 have been met in the area tested. Further soil evaluations and design work are necessary to determine whether a septic system for a particular use, meeting the requirements of Title5 and applicable local bylaws, will in fact be feasible on this site.

DN-SITE REVIEW	
-----------------------	--

ON-SITE	REVIEW				
DEEP HOLE	E #: 16-02	DATE: 12/1	/16	TIME: 9:00am	WEATHER: Sunny 45*
SITE ADDR	ESS or MAP	P/LOT #: Map 66,	Lot 1, West Str	eet, Medway MA	
OWNER:	Summit Hor	me Builders Inc		JOI	B NO.: 16-064
LOCATION	(Identify on I	Plan): See Attached Pla	n GRO	OUND ELEVATION A	AT SURFACE OF HOLE: To be determined
LAND USE:	Resider	ntial SURF	ACE STONES:	Yes: X No:	SLOPE (%): 2-4%
	ON: Gravelly	/-Field		LANDFORM:	Kame
OPEN WAT	ER BODY:	300' ft PROPERTY	LINE: 60'	ft POSSIBLE WET	TAREA: 145' ft DRAINAGEWAY: 300' ft
DRINKING V	WATER WE	LL: - ft OTHE	ER:		
DEEP OBSI	ERVATION I	HOLELOG	-		
Depth (inches)	Soil Hor./ Layer	Soil Texture (USDA)	Soil Color (Munsell)	Redoximorphic Features	Other (Structure, Consistency,% Gravels, Stones, Boulders
0-32"		Clean Fill			Fine to Coarse Sand and Gravel
32"-42"	A	Loamy Sand (LS)	10yr3/3		Friable Roots
42"-60"	42"-60" B Loamy Sand (LS) 10yr5/8 Friable Roots				
60"-72"	C1	Sand	10yr5/4	60"	M-C Sand, Gravel 10% Stones
72"-96"	C2	Sand	10yr 5/3	Oxid. 10yr5/8 Depl. 10yr6/2 Damp 72"+	Slightly Firm, Very Fine- Fine Sand Ledge 96"
PARENT M	TERIAL:	Loamy Glacio Deposits (L	.GD)	Unsuitable Material	Present? Yes: X No: If Yes:
Disturb	ed Soil:	Fill Mat'l: X	npervious Laye	r(s): We	eathered/Fractured Rock: Bedrock: X
GROUNDW	ATER OBSE	RVED: Yes: X	No:	If Yes: What is the	depth of Groundwater:
Standing i	n Hole:	Weeping from	n Face:	Saturating th	ne Face: 72"+ Mottling: 60"
Estimated D PERCOL	epth to Sea	asonal High Ground Wat	er: <u>60"</u>		
Percolation I	Hole #:			Percolation Hole	e #:
Test Date:				Test Date:	
Depth of Per	rc:			Depth of Perc:	
Start of Pres	oak:			Start of Presoak	«
End of Press	oak:			End of Presoak:	
Time @ 12":				Time @ 12":	
Time @ 9":				Time @ 9":	
Time Elapse:(12"-9") Time Elapse:(12"-9")					
Time AT 6":				Time AT 6":	
Time Elapse	: (9"-6"):		_	Time Elapse: (9	"-6"):
Rate: (min/in	n.):			Rate: (min/in.):	
Test Passed Discon/ Add	l/ Failed/ . Test Req'd	:		Test Passed/ Fa Add. Testing Re	ailed/ Discon/ eq'd:
Performed B Comments:	y: Thomas	A Pozerski Witness	sed By: <u>N/A</u>	N	Mach./Oper.: Trufant

An indication that the "site passed" indicates only that the basic criteria for a soil evaluation and percolation test under Title 5 have been met in the area tested. Further soil evaluations and design work are necessary to determine whether a septic system for a particular use, meeting the requirements of Title5 and applicable local bylaws, will in fact be feasible on this site.

JN-SITE REVIEW	EVIEW	-SITE	NC
----------------	-------	-------	----

ON-SITE	REVIEW				
DEEP HOLI	E #: 16-03	DATE: 12/1	/16	TIME: 10:00a	m WEATHER: Sunny 50*
SITE ADDR	ESS or MAF	P/LOT #: Map 65, L	ot 26, West Stre	eet, Medway MA	
OWNER:	Summit Hor	me Builders Inc		lo	B NO.: 16-064
LOCATION	(Identify on I	Plan): See Attached Pla	in GRC	OUND ELEVATION	AT SURFACE OF HOLE: To be determined
LAND USE:	Resider	ntial SURF	ACE STONES:	Yes: X No:	SLOPE (%): 2-4%
VEGETATIO	ON: Gravelly	/- Field		LANDFORM:	Kame
DISTANCES	S FROM:				
OPEN WAT	ER BODY:	280' ft PROPERTY	/ LINE:20'	ft POSSIBLE WE	T AREA: 150 ft DRAINAGEWAY: 280 ft
DRINKING	WATER WE	LL: - ft OTHE	ER:		
DEEP OBS	ERVATION	HOLE LOG	Coll Color	Dedevineembie	
(inches)	Layer	Soil Texture (USDA)	(Munsell)	Features	Other (Structure, Consistency,% Gravels, Stones, Boulders
0-60"		Fill			_
60"-96"	с	Loamy Sand (LS)	10yr6/4	60"	Fine to Med Sand with Silt, 10% Stones, Large Boulder at 96".
				Oxid. 10yr6/8	
				Depl. 10yr 6/4	
				Damp 74"+	
		Loamy Glacio Depostits((GD)	Linsuitable Material	Present? Yes: X No: If Yes:
Disturb	ed Soil	Fill Mat'l:	mpervious Laver	(s): We	athered/Fractured Rock: Bedrock:
CROUNDW				If Ves: 10/bat is the	depth of Groundwater:
Standing	in Hole:	Weeping from	Face:	Saturating th	be Face: 74" Mottling: 60"
Estimated I	Depth to Sea	asonal High Ground Wat	er: 60"	Gaturating ti	Notang. 00
PERCOL	ATION TE	ST	70 N X 4747 -		
Percolation	Hole #:			Percolation Hol	e #:
Test Date:				Test Date:	
Depth of Pe	rc:			Depth of Perc:	
Start of Pres	soak:			Start of Presoal	K:
End of Pres	oak:			End of Presoak	
Time @ 12"	;			Time @ 12":	
Time @ 9":				Time @ 9":	
Time Elapse	e:(12"-9")			Time Elapse:(1)	2"-9")
Time AT 6":		· · · · · · · · · · · · · · · · · · ·		Time AT 6":	
Time Elapse	e: (9"-6"):			Time Elapse: (9)"-6"):
Rate: (min/ir	n.):			Rate: (min/in.):	
Test Passed	d/ Failed/	A		Test Passed/ Factor	ailed/ Discon/
Discon/ Add	I. Test Req'd			Add. Testing Re	eq'd:
Performed E Comments:	By: Thomas	A Pozerski Witnes:	sed By: <u>N/A</u>		Mach./Oper.: Trufant

An indication that the "site passed" indicates only that the basic criteria for a soil evaluation and percolation test under Title 5 have been met in the area tested. Further soil evaluations and design work are necessary to determine whether a septic system for a particular use, meeting the requirements of Title5 and applicable local bylaws, will in fact be feasible on this site.

0	N	-S	IT	Е	R	E١	/I	E	N	

DEEP HOLI	E #: 16-04	DATE: 12/1	/16	TIME: 11:00a	m WEATHER: Sunny 51*
SITE ADDR	ESS or MAR	P/LOT #: Map 65, L	ot 26, West Str	eet, Medway MA	
OWNER:	Summit Ho	me Builders Inc		JO	B NO.: 16-064
LOCATION	(Identify on	Plan): See Attached Pla	in GR	OUND ELEVATION	AT SURFACE OF HOLE: To be determined
LAND USE:	Resider	ntial SURF	ACE STONES:	Yes: X No:	SLOPE (%): 2-4%
VEGETATIC	ON: Gravell	y- Field		LANDFORM:	Kame
OPEN WAT	ER BODY:	300 ft PROPERTY	(LINE: 30	ft POSSIBLE WE	T AREA: 185 ft DRAINAGEWAY: 300 ft
DRINKING \	WATER WE	LL: <u> </u>	IR:		
DEEP OBS	ERVATION	HOLE LOG			
Depth (inches)	Soil Hor./ Layer	Soil Texture (USDA)	Soil Color (Munsell)	Redoximorphic Features	Other (Structure, Consistency,% Gravels, Stones, Boulders
0-24"		Fill			Clean Fill M-C Sand and Gravel
24"-132"	24"-132" C Sand 10yr6/4				Fine-Coarse Sand and Gravel
				Ox. 10yr5/8	5
				Depl. 10yr 6/4	
	Test sections.	n and a part of the	UMANEN.	New and and and at the set	
PARENT M	ATERIAL:	Loamy Glacio Depostits(LGD)	Unsuitable Material	Present? Yes: X No: If Yes:
Disturb	ed Soil:	Fill Mat'l: X	npervious Laye	r(s): We	eathered/Fractured Rock: Bedrock:
GROUNDW	ATER OBSI	ERVED: Yes: X	No:	If Yes: What is the	depth of Groundwater:
Standing i	in Hole:	Weeping from	n Face:	Saturating th	he Face: 74" Mottling: 72"
PERCOL	ATION TE	asonal High Ground Wat	er: <u>72</u> "		· · ·
Percolation I	Hole #:			Percolation Hol	e #:
Test Date:				Test Date:	
Depth of Per	rc:			Depth of Perc:	
Start of Pres	oak:			Start of Presoal	k:
End of Prese	oak:			End of Presoak	
Time @ 12":			_	Time @ 12":	
Time @ 9":		· · · · · · · · · · · · · · · · · · ·		Time @ 9":	/
Time Elapse	e:(12"-9")			Time Elapse:(1)	2"-9")
Time AT 6":		1		Time AT 6":	
Time Elapse	e: (9"-6"):			Time Elapse: (9	9"-6"):
Rate: (min/ir	n.):	2000 - 100 -		Rate: (min/in.):	
Test Passed Discon/ Add	l/ Failed/ . Test Req'd	ж <u></u>		Test Passed/ Fa Add. Testing Re	ailed/ Discon/ eq'd:
Performed B Comments:	By: Thomas	s A Pozerski Witness	sed By: <u>N/A</u>	· · · · · ·	Mach./Oper.: Trufant

An indication that the "site passed" indicates only that the basic criteria for a soil evaluation and percolation test under Title 5 have been met in the area tested. Further soil evaluations and design work are necessary to determine whether a septic system for a particular use, meeting the requirements of Title5 and applicable local bylaws, will in fact be feasible on this site.

	ON-S	ITE	REVI	EW
--	------	-----	------	----

DEED HOL	- #: 16.05	DATE: 12/1	/16	TIME: 12:00p	m MEATHER: Suppy 51			
SITE ADDR	ESS or MAI	DATE: 12/1 P/LOT # Map 65 L	ot 25 West Str	eet Medway MA	WEATHER. Sunny 51			
OW/NER	Summit Ho	me Builders Inc	or 20, West Su	.IO	B NO 16-064			
LOCATION	(Identify on	Plan): See Attached Pla	in GR	OUND ELEVATION	AT SURFACE OF HOLE: To be determined			
LOOAHON	(identity off	Flang. Obe Attached Fle						
LAND USE:	Reside	ntial SURF	ACE STONES:	Yes: X No:	SLOPE (%): 2-4%			
VEGETATIO	DN: Gravell	y- Field		LANDFORM:	Kame			
DISTANCES	S FROM:							
OPEN WAT	ER BODY:	350 ft PROPERTY	LINE: 55	ft POSSIBLE WE	T AREA: 230 ft DRAINAGEWAY: 350 ft			
DRINKING	WATER WE	ELL: ft OTHE	R:	5) <u> </u>				
DEEP OBS	ERVATION	HOLE LOG						
Depth (inches)	Soil Hor./ Layer	Soil Texture (USDA)	Soil Color (Munsell)	Redoximorphic Features	Other (Structure, Consistency,% Gravels, Stones, Boulders			
0-42"		Fill						
42"-72"	C1	Loamy Sand	10yr6/4	72"	Fine-Coarse Sand, Gravel and 10% Stones			
72"-108" C2 Sand			10yr 5/4	Ox. 10yr5/8	Fine Sand, Ledge 108"			
				Depl, 10yr 6/2				
	And Market							
PARENT M	ATERIAL:	Loamy Glacio Depostits(LGD)	Unsuitable Material	Present? Yes: X No: If Yes:			
Disturb	ed Soil:	Fill Mat'l: X	npervious Laye	r(s): We	eathered/Fractured Rock: Bedrock: X			
GROUNDW	ATER OBS	ERVED: Yes:	No:	If Yes: What is the	e depth of Groundwater:			
Standing	in Hole:	Weeping from	Face:	Saturating t	he Face: Mottling: 72"			
Estimated I	Depth to Se	asonal High Ground Wat	er: <u>72</u> "					
PERCOL	ATION TE	EST						
Percolation	Hole #:			Percolation Hol	e #:			
Test Date:				Test Date:	(<u></u>			
Depth of Pe	rc:	· · · · · · · · · · · · · · · · · · ·		Depth of Perc:				
Start of Pres	soak:			Start of Presoak:				
End of Pres	oak:			End of Presoak				
Time @ 12"				Time @ 12":				
Time @ 9":				- Time @ 9":	New York			
Time Elapse	e:(12"-9")			Time Elapse:(1	2"-9")			
Time AT 6":				Time AT 6":				
Time Elapse	e: (9"-6"):	······································		Time Elapse: (9	9"-6"):			
Rate: (min/ii	า.):			Rate: (min/in.):				
Test Passed	/ Failed/			Test Passed/ F	ailed/ Discon/			
Discon/ Add	. Test Req'd	J.		Adu, Testing Ri	ey u.			
Performed E Comments:	By: Thoma	s A Pozerski Witnes:	sed By: N/A		Mach./Oper.: Trufant			

An indication that the "site passed" indicates only that the basic criteria for a soil evaluation and percolation test under Title 5 have been met in the area tested. Further soil evaluations and design work are necessary to determine whether a septic system for a particular use, meeting the requirements of Title5 and applicable local bylaws, will in fact be feasible on this site.

MERRILL ENGINEERS & LAND SURVEYOR REGISTERED PROFESSIONAL ENGINEERS 427 COLUMBIA ROAD, HANOVER, MA. 0233 TEL. (781) 826-9200	JOB SHEET NO. CALCULATED B CHECKED BY	16-064 1 Y <u>DA</u> <u>PGP</u>	of D	1 ATE: 6/12/17	
Location:	GLEN BROOF	K WAY			
	Recharge Vol	umes (Standard	<u>#3)</u>		
Total Area (Ac.)=	3.155				
Total Impervious Area A Soil (Ac.)=	1.277				
Total Impervious Area B Soil (Ac.)=	0				
Total Impervious Area C Soil (Ac.)=	0				
	Vol. To				
	Recharge	Volume (Imp.			
	(inches per	Area x inches			
	Imp. Acre)	per Acre)			
Recharge Volume (A soil)	0.4	0.51			
Recharge Volume (B soil)	0.25	0.00			
Recharge Volume (C soil)	0.1	0.00			
		0.51	AC-IN		
Total Required Recharge Volume:		0.04	AC-FT		
		1854	C.F.		

Recharge volume provided by Infiltration		
System:		
Volume Provided (below outlet, 4P Lg Syst):	17,940	C.F.
Volume Provided (below outlet, 5P, Roof Syst.):	2,826	C.F.
Total Volume	20,766	

Water Quality Volume			
Required Volume =	400 CF/AC x Impervious Area		
New Impervious Area onsite	55,605 SF 1.28 AC	7.48 Gal/CF	
Required Volume for Separator Row Volume Provided	510.61 CF 535 CF (below 12" o	= 3819 Gal verflow pipe invert)	

MERRILL ENGI REGISTERED P 427 COLUMBIA TEL. (781) 826-9 Location:	NEERS & LAND SURVEYORS PROFESSIONAL ENGINEERS ROAD, HANOVER, MA. 02339 2200 <u>WATER QUALITY VOLUME (STAI</u> GLEN BROOK WAY	JOB 16-064 SHEET N0. 1 of CALCULATED BY <u>DA</u> CHECKED BY <u>PGP</u>	1 DATE: 4/15/2017 REV'D:
Total New Imper	vious Area Parking area	46,983 S.F.	
	Roof	8,622 S.F.	
		00,000 0.1 .	
Water Quality Volume using:	0.5 or 1.0 inch x Imp. Area (per S.W. Mgmt 0.5 inch x Imp. Area	Policy) 2,317 cubic feet	
Provided by large	Infiltration System #2 (see calcs in Appdx B)	17,900+ c.f. (Below	outlet)

INSTRUCTIONS:

In BMP Column, click on Blue Cell to Activate Drop Down Menu
Select BMP from Drop Down Menu
After BMP is selected, TSS Removal and other Columns are automatically completed.

			Ī								
	ш	Remaining	Load (D-E)	0.75	0.56	0.56	0.56	0.56	Separate Form Needs to be Completed for Each Outlet or BMP Train	a	n previous BMP (E)
	ш	Amount	Removed (C*D)	0.25	0.19	0.00	0.00	0.00	44%		*Equals remaining load fron
ent	Ω	Starting TSS	Load*	1.00	0.75	0.56	0.56	0.56	SS Removal =	L	
Glen Brook Way - Pretreatm	U	TSS Removal	Rate ¹	0.25	0.25	0.00	0.00	0.00	Total T	16-064	DA
Location:	Ш		BMP ¹	Deep Sump and Hooded Catch Basin	Sediment Forebay					Project:	Prepared By:
				ູງອອເ	orkst oval	mэЯ W no	itelu:	OlbJ	-		
					())						

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1

Date: 6/27/2017

Mass. Dept. of Environmental Protection

which enters the BMP

Version 1, Automated: Mar. 4, 2008

INSTRUCTIONS:

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

After BMP is selected, TSS Removal and other Columns are automatically completed.



must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1 Non-automated TSS Calculation Sheet

Date: |6/15/2017

*Equals remaining load from previous BMP (E)

which enters the BMP

Version 1, Automated: Mar. 4, 2008

Stage-Area-Storage for Pond 7P: SEPARATOR ROW (Stone not included)

	Elevation	Storage	Elevation	Storage	Elevation	Storage
		(CUDIC-IEEL)				
	203.00	0	204.08	030	205.10	1,114
	203.02	12	204.10	647	205.18	1,119
	203.04	25	204.12	658	205.20	1,124
	203.06	37	204.14	669	205.22	1,128
	203.08	49	204.16	680	205.24	1,132
	203.10	62	204.18	691	205.26	1,136
	203.12	74	204.20	702	205.28	1,140
	203.14	86	204.22	713	205.30	1,143
	203.16	98	204.24	723	205.32	1,146
	203.18	111	204.26	734	205.34	1,149
	203.20	123	204.28	745	205.36	1,151
	203.22	135	204.30	755	205.38	1,153
	203.24	147	204.32	766	205.40	1,154
	203.26	159	204.34	776	205.42	1,156
	203.28	171	204.36	787	205.44	1,157
	203.30	183	204.38	797	205.46	1,158
	203.32	195	204.40	807	205.48	1,158
	203.34	207	204.42	817	205.50	1,159
	203.36	219	204.44	827		
	203.38	232	204.46	837		
	203.40	244	204.48	846		
	203.42	256	204.50	856		
	203.44	268	204.52	866		
	203.46	280	204.54	875		
	203.48	292	204.56	885		
	203.50	304	204.58	894		
	203.52	316	204.60	903		
	203.54	328	204.62	912		
	203.56	339	204.64	922		
	203.58	351	204.66	931		
	203.60	363	204.68	939		
	203.62	3/5	204.70	948		
	203.64	387	204.72	957		
	203.66	398	204.74	905		
	203.68	410	204.76	974		
	203.70	421	204.78	982		
	203.72	433	204.80	991		
	203.74	444	204.82	999		
	203.76	400	204.84	1,007		
	203.10	40/	204.00	1,010		
	203.60	4/0	204.00	1,022		
	203.02	490	204.90	1,030		
	203.04	501	204.92	1,037	ъ	
	203.00	502	204.94	1,040		
al a st	203.00	535	204.90	1,052		
W.Q. V	203.90	5/6	204.30	1,000		
= 211 GU	203.32	557	205.00	1 072		
	203.04	569	205.02	1 079		
	203.00	580	205.04	1 085		
	200.00	591	205.08	1 091		
	204.00	602	205 10	1 097		
	204.02	613	205.12	1,103		
	204.04	624	205.14	1.109		
	201100			.,		

- = 511

Hydrograph for Pond 4P: LARGE INFILTRATION SYSTEM

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Discarded (cfs)	Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Discarded (cfs)	
0.00	0.00	0	202.50	0.00	27.00	0.00	2,929	203.20	0.45	
0.50	0.00	0	202.50	0.00	27.50	0.00	2,114	203.08	0.45	
1.00	0.00	0	202.50	0.00	28.00	0.00	1,305	202.92	0.45	
1.50	0.00	0	202.50	0.00	28.50	0.00	505	202.66	0.44	
2.00	0.00	0	202.50	0.00	29.00	0.00	3	202.50	0.01	RECHARGE SYSTEM
2.50	0.00	0	202,50	0.00	29.50	0.00	0	202.50	0.00	DRAIN TIME
3.00	0.00	0	202.50	0.00	30.00	0.00	0	202.50	0.00	< 22 Ha
3.50	0.00	0	202.50	0.00	30.50	0.00	0	202.50	0.00	TE IKS
4.00	0.00	0	202.50	0.00	31.00	0.00	0	202.50	0.00	
4.50	0.01	1	202.50	0.01	31.50	0.00	0	202.50	0.00	
5.00	0.02	4	202.50	0.02	32.00	0.00	0	202.50	0.00	
5.50	0.03	7	202.50	0.03	32.50	0.00	0	202.50	0.00	
6.00	0.04	10	202.50	0.04	33.00	0.00	0	202.50	0.00	
6.50	0.06	14	202.50	0.05	33.50	0.00	0	202.50	0.00	
7.00	0.08	19	202.51	0.07	34.00	0.00	0	202.50	0.00	
7.50	0.10	25	202.51	0.10	34.50	0.00	0	202.50	0.00	
8.00	0.13	32	202.51	0.13	35.00	0.00	0	202.50	0.00	
8.50	0.17	42	202.51	0.17	35.50	0.00	0	202.50	0.00	
9.00	0.23	56	202.52	0.22	36.00	0.00	0	202.50	0.00	
9.50	0.30	73	202.52	0.29	36.50	0.00	0	202.50	0.00	
10.00	0.37	90	202.53	0.36	37.00	0.00	0	202.50	0.00	
10.50	0.48	121	202.54	0.44	37.50	0.00	0	202.50	0.00	
11.00	0.62	320	202.60	0.44	38.00	0.00	0	202.50	0.00	
11.50	1.00	927	202.80	0.44	38.50	0.00	0	202.50	0.00	
12.00	4.93	4,308	203.40	0.46	39.00	0.00	0	202.50	0.00	
12.50	2.98	14,493	205.05	0.50	39.50	0.00	0	202.50	0.00	
13.00	1.02	16,394	205.51	0.51	40.00	0.00	0	202.50	0.00	
13.50	0.76	17,011	205.70	0.51	40.50	0.00	0	202.50	0.00	
14.00	0.62	17,330	205.81	0.51	41.00	0.00	0	202.50	0.00	
14.50	0.53	17,428	203.84	0.52	41.50	0.00	0	202.50	0.00	
15.00	0.40	17,390	203.03	0.51	42.00	0.00	0	202.00	0.00	
15.50	0.40	17,240	200.70	0.51	42.00	0.00	0	202.50	0.00	
16.00	0.33	10,900	200.09	0.51	43.00	0.00	0	202.50	0.00	
17.00	0.29	16,011	200.00	0.51	43.30	0.00	0	202.50	0.00	
17.00	0.20	15,190	200.40	0.51	44.00	0.00	0	202.50	0.00	
18.00	0.23	15,721	205.52	0.50	45.00	0.00	0	202.00	0.00	
18.50	0.20	14 649	205.20	0.50	45.50	0.00	ő	202.50	0.00	
19.00	0.10	14,045	200.00	0.00	46.00	0.00	õ	202.50	0.00	
19.50	0.10	13 499	204.86	0.49	46.50	0.00	õ	202.50	0.00	
20.00	0.16	12 907	204.00	0.49	47.00	0.00	õ	202.50	0.00	
20.50	0.15	12,304	204 65	0.49	47.50	0.00	õ	202.50	0.00	
21.00	0.14	11,694	204.55	0.49	48.00	0.00	0	202.50	0.00	
21.50	0.14	11,076	204 44	0.48	10.00	0100	-			
22.00	0.13	10.450	204.34	0.48						
22.50	0.12	9.816	204.24	0.48						
23.00	0.12	9,174	204.14	0.48						
23.50	0.11	8,525	204.04	0.47						
24.00	0.10	7,868	203.94	0.47						
24.50	0.00	7,079	203.82	0.47						
25.00	0.00	6,239	203.69	0.47						
25.50	0.00	5,404	203.57	0.46						
26.00	0.00	4,574	203.44	0.46	1					
26.50	0.00	3,749	203.32	0.46						
					1					

Hydrograph for Pond 5P: ROOF INFILTRATION SYSTEM

Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Discarded (cfs)	Time (hours)	Inflow (cfs)	Storage (cubic-feet)	Elevation (feet)	Discarded (cfs)		
0.00	0.00	0	202.50	0.00	27.00	0.00	7	202.51	0.03		
0.50	0.00	Ő	202.50	0.00	27.50	0.00	0	202.50	0.00	RECHARGE	SYSTEM
1.00	0.00	1	202.50	0.00	28.00	0.00	0	202.50	0.00	DRALLE	A AL A STREET
1.50	0.01	2	202.50	0.01	28.50	0.00	0	202.50	0.00	VICTIN I	IME
2.00	0.01	3	202.51	0.01	29.00	0.00	Õ	202.50	0.00	<72 Hi	25
2.50	0.01	3	202.51	0.01	29.50	0.00	Ō	202.50	0.00		
3.00	0.02	4	202.51	0.01	30.00	0.00	Õ	202.50	0.00		
3.50	0.02	4	202.51	0.02	30.50	0.00	Ō	202.50	0.00		
4.00	0.02	5	202.51	0.02	31.00	0.00	0	202.50	0.00		
4.50	0.02	5	202.51	0.02	31.50	0.00	Õ	202.50	0.00		
5.00	0.02	6	202.51	0.02	32.00	0.00	0	202.50	0.00		
5.50	0.02	6	202.51	0.02	32.50	0.00	Ō	202.50	0.00		
6.00	0.03	6	202.51	0.03	33.00	0.00	0	202.50	0.00		
6.50	0.03	7	202.51	0.03	33.50	0.00	Ō	202.50	0.00		
7.00	0.03	8	202.52	0.03	34.00	0.00	0	202.50	0.00		
7.50	0.04	10	202.52	0.04	34.50	0.00	0	202.50	0.00		
8.00	0.04	11	202.52	0.04	35.00	0.00	Ō	202.50	0.00		
8.50	0.05	13	202.52	0.05	35.50	0.00	0	202.50	0.00		
9.00	0.06	15	202.53	0.06	36.00	0.00	Ō	202.50	0.00		
9.50	0.07	18	202.54	0.07	36.50	0.00	0	202.50	0.00		
10.00	0.08	28	202.56	0.07	37.00	0.00	0	202.50	0.00		
10.50	0.10	61	202.62	0.07	37.50	0.00	0	202.50	0.00		
11.00	0.12	130	202.76	0.07	38.00	0.00	0	202.50	0.00		
11.50	0.18	261	203.01	0.07	38.50	0.00	0	202.50	0.00		
12.00	0.81	845	203.56	0.08	39.00	0.00	0	202.50	0.00		
12.50	0.45	2,423	205.25	0.09	39.50	0.00	0	202.50	0.00		
13.00	0.15	2,676	205.70	0.10	40.00	0.00	0	202.50	0.00		
13.50	0.11	2,731	205.81	0.10	40.50	0.00	0	202.50	0.00		
14.00	0.09	2,742	205.83	0.10	41.00	0.00	0	202.50	0.00		
14.50	0.08	2,720	205.79	0.10	41.50	0.00	0	202.50	0.00		
15.00	0.07	2,679	205.71	0.10	42.00	0.00	0	202.50	0.00		
15.50	0.06	2,621	205.59	0.10	42.50	0.00	0	202.50	0.00		
16.00	0.05	2,548	205.45	0.09	43.00	0.00	0	202.50	0.00		
16.50	0.04	2,460	205.30	0.09	43.50	0.00	0	202.50	0.00		
17.00	0.04	2,367	205.17	0.09	44.00	0.00	0	202.50	0.00		
17.50	0.03	2,267	205.04	0.09	44.50	0.00	0	202.50	0.00		
18.00	0.03	2,161	204.91	0.09	45.00	0.00	0	202.50	0.00		
18.50	0.03	2,051	204.78	0.09	45.50	0.00	0	202.50	0.00		
19.00	0.03	1,940	204.66	0.09	46.00	0.00	0	202.50	0.00		
19.50	0.02	1,828	204.54	0.09	46.50	0.00	0	202.50	0.00		
20.00	0.02	1,715	204.42	0.09	47.00	0.00	0	202.50	0.00		
20.50	0.02	1,602	204.30	0.09	47.50	0.00	0	202.50	0.00		
21.00	0.02	1,489	204.19	0.08	48.00	0.00	0	202.50	0.00		
21.50	0.02	1,376	204.08	0.08							
22.00	0.02	1,262	203.97	0.08							
22.50	0.02	1,148	203.85	0.08							
23.00	0.02	1,034	203.74	0.08							
23.50	0.02	920	203.63	0.08							
24.00	0.02	806	203.52	0.08							
24.50	0.00	674	203.40	0.08							
25.00	0.00	535	203.26	0.08							
25,50	0.00	398	203.14	0.08							
26.00	0.00	262	203.01	0.07							
26.50	0.00	130	202.76	0.07	1						

Groundwater Mound Beneath Rectangular Recharge Area 폐

by Glenn M. Duffield, President, HydroSOLVE, Inc. 🛅

in Share

<u>Hantush (1967)</u> presented the following equations for predicting the maximum height of the <u>water table</u> beneath a rectangular recharge area:

4

$$\begin{split} h_m^2 - h_i^2 &= Z_m(t) = (2w/K)vtS^*(0.5A/(4vt)^{1/2}, 0.5B/(4vt)^{1/2}) \dots \dots (1) \\ v &= K\overline{b}/\epsilon \dots \dots (2) \\ \overline{b} &= 0.5[h_i(0) + h(t)] \dots \dots (3) \end{split}$$

where h_m is maximum height of mound above aquifer base (i.e., maximum saturated thickness of aquifer beneath recharge area); h_i is initial height of water table above aquifer base (i.e., initial saturated thickness of aquifer); K and ϵ are <u>hydraulic conductivity</u> and <u>storativity</u> (<u>specific yield</u>) of aquifer, respectively; w is constant rate of percolation from rectangular recharge area of length A and width B; \overline{b} is a constant of linearization; and the function S* is an integral expression (see <u>Hantush 1967</u>). The aquifer is unconfined and assumed to have infinite extent.

If infiltration ends at time $t=t_0$, Hantush (1967) applied the principle of superposition to compute the decay of the mound as follows:

$$h_m^2 - h_i^2 = Z_m(t) - Z_m(t-t_0) \dots (4)$$

Equation (1) is nonlinear owing to the definition of \overline{b} in Equation (3); however, the solution is readily obtained by successive approximation.

Results of Groundwater Mounding Calculation									
Solution by Successive Approximation									
Itera	ation		b		h _m *		% Change		
1	1	6	95	696.08	818571472	68 0.15	5662898887554		
2	2	695.5409	285736	34696.08	820605149	99 ^{2.92}	160653891926E- 05		
K [L/T]	з	h _i [L]	A [L]	B [L]	w [L/T]	t [T]	հ _m [L]		
15.0468	.3	695	157.5	49.83	4.43425	1	696.082060514999		
maximum water-table rise (h _m - h _i) at time t = 1 is 1.08206051499894									

Return to Groundwater Mounding Calculator

MERRILL ENGINEERS AND LAND SURVEYORS

REGISTERED PROFESSIONAL ENGINEERS 427 COLUMBIA ROAD, HANOVER, MA. 02339 TEL. (781) 826-9200 JOB 16-064 SHEET N0. 1 of 1 CALCULATED BY <u>DA</u> CHECKED BY <u>PGP</u> <u>DATE:</u> 6/12/2017 REV'D:

Hantush (1967) Groundwater Mounding Calculator Data

Location: Glen Brook Way, Medway

Infiltration System:

1 Perc Rate P.R.):	2	MPI
2 Hydraulic Conductivity (K)		
Rate (ft/day): ((60mph/P.R.)x(24hr/1 day))/(12in./ft)	60	ft/day
K=R/6.03)^1.18=	15.0468	ft/day
3 Specific Yield: Gravelly Sand =	0.30	
4 T= (per Brett Rowe & Kermit Studley, MA DEP):	1	days
5 Initial Sat'd Thickness (h_i): (assumed from nearby irrigation well)	695	ft
6 Length of basin:	157.5	ft
7 Width of basin:	49.83	ft
8 Recharge Rate:		
A=L x W =	7848.225	sf
Q= (DDF)		
Flow	34801	C.F. per day (Hydrocad)
Recharge Rate:	4.43425	ft/day

APPENDIX D

Existing and Proposed Watersheds Plan (Insert)



PRE-DEVELOPMENT WATERSHEDS

SUBCATCHME	INT 1E	
DESCRIPTION	AREA (S.	F.)
GRASS HSG A WOODS HSG A WOODS HSG B WETLANDS GRAVEL IMPERVIOUS AREA SUBTOTAL	40,652 9,303 584 459 311 1,888 53,197	S.F. S.F. S.F. S.F. S.F. S.F.
SUBCATCHM	ENT 2F	
SUBCATCHME DESCRIPTION	<u>ENT 2E</u> area (s.	F.)
SUBCATCHME DESCRIPTION GRASS HSG A WOODS HSG A WOODS HSG B WETLANDS	AREA (S. 37,457 11,716 12,368 12,165	F.) S.F. S.F. S.F. S.F.
SUBCATCHME DESCRIPTION GRASS HSG A WOODS HSG A WOODS HSG B WETLANDS SUBTOTAL	AREA (S. 37,457 11,716 12,368 12,165 73,706	F.) S.F. S.F. S.F. S.F. S.F.

REVISIONS DRAWN BY: VC DESIGNED BY: PGP CHECKED BY: PGP Чŝ Å Ā Ā An \mathbb{H} ัธิอี 26 427 E WEST STREET MEDWAY, MASSACHUSETTS Der: Metro Mest collaborative development Newton, Ma 02458 P L A N SITE Ê APRIL 24, 2017 SCALE: AS-NOTED JOB No. 16-064 LATEST REVISION: EXISTING WATERSHED PLAN SHEET 1 OF 1



DEVELOPMENT	WATERSHEDS

SUBTOTAL 9,003

S.F.

SUBCATCHMENT	7S	
DESCRIPTION	AREA (S.F.)	
GRASS COVER, HSG A DIRT ROADS, HSG A WOODS, GOOD, HSG A WOODS, GOOD, HSG B WETLANDS	5,362 188 2,612 456 385	S.F. S.F. S.F. S.F. S.F.

SUBCATCHMENT 6S

SCRIPTION	AREA (S.F.)	
ASS COVER, HSG A ODS, GOOD, HSG A ODS, GOOD, HSG B TLANDS ASS COVER, GOOD, HSG A	14,662 8,056 12,496 12,239 1,000	S.F. S.F. S.F. S.F. S.F.
SUBTOTAL	48,453	S.F.
SUBCATCHMENT 1	Р	

DESCRIPTION AREA (S.F.)

SUBCATCHMENT	2P	
SCRIPTION	AREA (S.F.)	
PERVIOUS, HSG A ASS COVER, GOOD, HSG A IODS, HSG A	46,983 12,866 976	S.F. S.F S.F
SUBTOTAL	60,825	S.F.
TOTAL AREA	126,903	S.F.



